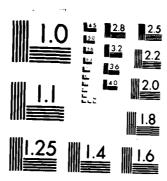
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VANDENBERG AIR FORCE BASE, CALIFORNIA

RANGE REFERENCE ATMOSPHERE
0-70 KM ALTITUDE

APRIL 1983

METEOROLOGY GROUP
RANGE COMMANDERS COUNCIL

WHITE SANDS MISSILE RANGE KWAJALEIN MISSILE RANGE YUMA PROVING GROUND

PACIFIC MISSILE TEST CENTER
NAVAL WEAPONS CENTER
ATLANTIC FLEET WEAPONS TRAINING FACILITY
NAVAL AIR TEST CENTER

EASTERN SPACE AND MISSILE CENTER
ARMAMENT DIVISION
WESTERN SPACE AND MISSILE CENTER
AIR FORCE SATELLITE CONTROL FACILITY
AIR FORCE FLIGHT TEST CENTER
AIR FORCE TACTICAL FIGHTER WEAPONS CENTER



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FOREWORD

Atmospheric parameters are essential to the research and development of missiles and aerospace vehicles. In the early 1960's, the need was recognized for realistic atmospheric models derived in a consistent manner for each of the several major test ranges. An atmospheric model derived from statistical data for a particular geographical location is referred to as a reference atmosphere.

The first Range Reference Atmosphere (RRA) was issued in 1963 by the Inter-Range Instrumentation Group (IRIG) for Cape Kennedy, Florida, and was followed by additional publications for several ranges up to 1974. Since that time, improved upper air data bases have become available from which to develop the RRA. These resulted from the extended period of records and from improvement in the upper air measuring program by rocketsondes for altitudes above the rawinsonde ceiling of 30 km. Revised and improved RRAs are justified for the following reasons:

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For these reasons, the Range Reference Atmosphere Committee (RRAC) was tasked by the Range Commanders Council Meteorology Group (RCC MG) to establish new and improved RRAs. The purpose, scope, and objectives of this task are outlined in the following paragraphs.

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In keeping with the RCC's objective of standardization, the modeling techniques, basic text, and tabulation format are to be the same for all RRAs. These new and revised RRAs present not only the mean values of the thermodynamic quantities (pressure, temperature, virtual temperature, and density), but also include statistical measures for the dispersion (i.e., standard deviations and skewness coefficients). New quantities presented are water vapor pressure and dewpoint temperature. The statistical modeling for the wind is entirely new. The new approach uses the properties of the bivariate normal probability distribution function.

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The text was prepared jointly by USAFETAC and the NASA/George C. Marshall Space Flight Center's Space Sciences Laboratory, Atmospheric Sciences Division. The editing and preparation of the draft manuscript were performed by the NASA/MSFC organization.

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The RRAC consists of representatives from the U.S. Air Force, U.S. Army, National Aeronautics and Space Administration, U.S. Navy, and National Oceanic and Atmospheric Administration. The committee members for the RRA for the first publication are:

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- S. F. Kubinski, WSMR
- F. J. Schmidlin, NASA/WFC
- O. E. Smith Cochairman, NASA/MSFC

Maj. B. W. Galusha Cochairman, USAF/ETAC

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VANDENBERG AIR FORCE BASE, CALIFORNIA

RANGE REFERENCE ATMOSPHERE 0-70 KM ALTITUDE

April 1983

Prepared by

Range Reference Atmosphere Committee Meteorology Group Range Commanders Council

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White Sands Missile Range, New Mexico 88002



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LIST OF ORGANIZATION ACRONYMS

AD

Armament Division

AFFTC

Air Force Flight Test Center

AFSC

Air Force Systems Command

AFSC/AFGL

AFSC/Air Force Geophysics Laboratory

AFSC/SD

AFSC/Space Division

AFSCF

Air Force Satellite Control Facility

AFTFWC

Air Force Tactical Fighter Weapons Center

AWS

Air Weather Service

BMD

Ballistic Missile Division

DOD

Department of Defense

DOE

Department of Energy

DOE/NTS

DOE/Nevada Test Site

DPG

Dugway Proving Ground

ESMC

Eastern Space and Missile Center

ETR

Eastern Test Range

KMR

Kwajalein Missile Range

NASA

National Aeronautics and Space Administration

NASA/MSFC

NASA/Marshall Space Flight Center

NASA/WFC

NASA/Wallops Flight Center

NOAA

National Oceanic and Atmospheric Administration

NWC

Naval Weapons Center

PMTC

Pacific Missile Test Center

USA/DTC

U.S. Army/Deseret Test Center

USAECOM

U.S. Army Electronics Command

USAFETAC

United States Air Force Environmental Technical

Applications Center

UTTR Utah Test and Training Range

WSMC Western Space and Missile Center

WSMR White Sands Missile Range

WTR Western Test Range

YPG Yuma Proving Ground

6585TG 6585th Test Group

TSCF Targeting Systems Characterization Facility

FOREWORD

Atmospheric parameters are essential to the research and development of missiles and aerospace vehicles. In the early 1960's, the need was recognized for realistic atmospheric models derived in a consistent manner for each of the several major test ranges. An atmospheric model derived from statistical data for a particular geographical location is referred to as a reference atmosphere.

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Maj. B. W. Galusha Cochairman, USAF/ETAC

CHAPTER I. INTRODUCTION

A. Definition and Purpose of the Range Reference Atmosphere

A.1 Definition

A reference atmosphere is a statistical model of the Earth's atmosphere derived from upper air measurements over a particular geographical location. Hence, these Range Reference Atmospheres (RRAs) are atmospheric models developed by the Range Reference Atmosphere Committee (RRAC) in response to a task by the Range Commanders Council Meteorology Group (RCC MG) and published by the RCC Secretariat. The RCC MG, formerly called the Inter-Range Instrumentation Group/Meteorology Working Group (IRIG/MWG), published a series of RRAs during the period 1963 through 1974.

A.2 Purpose

A series of revised and expanded RRAs are to be published for locations of interest to the RCC. These publications are to serve as authoritative reference sources on certain upper air statistics and as atmospheric models for particular range sites. The technical usefulness of these documents for the ranges, range users, U.S. aerospace industries, and the scientific community is recognized because of the standardization of the development techniques and the presentation of the tabulations.

B. Scope of the Range Reference Atmosphere and Arrangement of Tables

B.1 Scope

The RRA contains tabulations for monthly and annual means, standard deviations, and skewness coefficients for windspeed, pressure, temperature, density, water vapor pressure, virtual temperature, and dewpoint temperature; the means and standard deviations for the zonal (U) and meridional (V) wind components; and the linear (product moment) correlation coefficient between the wind components. These statistical parameters are tabulated at the station elevation, at 1-km intervals from sea level to 30 km, and at 2-km intervals from 30 to 90 km. The wind statistics are given at approximately 10 m above the station elevations and at altitudes with respect to mean sea level thereafter. For those range sites without rocketsonde measurements, the RRAs terminate at 30 km altitude, or they are extended, if required, when rocketsonde data from a nearby launch site are available. There are four sets of tables for each of the 12 monthly reference periods and the annual reference period.

B.2 Arrangement of Tables

The statistical parameters for the RRA models are presented in four tables, as outlined in the following paragraphs.

Table I contains all the wind statistical parameters. This table gives the monthly and annual means and standard deviations of the U and V wind components and the linear (product moment) correlation coefficient between these

two components; the mean, standard deviation and skewness coefficient of the windspeed; and the number of wind observations (sample size).

Table II contains the monthly and annual means, standard deviations, and skewness values of pressure, temperature, and density, and the number of observations used for each of these thermodynamic quantities.

Table III contains the monthly and annual means, standard deviations and skewness values of the water vapor pressure, virtual temperature and dewpoint, and the number of observations for each of these moisture-related quantities. The statistical parameters for water vapor pressure and dewpoint terminate at 15 km altitude. Above 15 km the statistical parameters for virtual temperature are considered to be the same as those for temperature.

Table IV contains the monthly and annual mean atmospheric models for the thermodynamic variables: pressure, virtual temperature, and density. This table is derived from the monthly and annual mean virtual temperature versus altitude (geometric) using the hydrostatic equation and the equation of state. Also presented is the geopotential height corresponding to the tabulated geometric altitudes.

The physical unit for all wind parameters is meters per second. The physical unit for pressure is millibars; for temperature and virtual temperature, degrees Kelvin; for density, grams per cubic meter; and for water vapor pressure, millibars. In all cases the skewness coefficient and the correlation coefficient between wind components are unitless. All reference to altitude is geometric altitude and is expressed in kilometers. All reference to height is geopotential height and has the unit geopotential meters or kilometers. All geometric altitudes and geopotential heights are with respect to mean sea level.

C. Data Quality Control Procedures

A small portion (less than 10 percent) of the soundings in the data base used to calculate the RRA tables contained erroneous data values. The soundings which contained these erroneous values were eliminated from the data base using the following procedures:

- 1) Soundings containing gaps in their height data greater than 200 mb were rejected. This step was taken because some soundings only contained height values at their "mandatory" pressure levels, which were occasionally missing, resulting in soundings with no height information at all.
- 2) An initial set of RRA statistics was computed using all the remaining soundings. This initial set of statistics was used to determine data limits for the temperature, pressure, U and V components of the wind, and the dewpoint (for the 0- to 30-km portion of the RRA) or the density (for the 30- to 90-km portion of the RRA). The lower (upper) data limits were set at the mean value for a specific parameter, minus (plus) six standard deviations of that quantity. One pair of data limits was computed for each of these parameters: month of the year and data level.

- 3) This initial set of data limits was then used to screen the data base. All the soundings that contained values outside these data limits were rejected. A new RRA was then computed using the screened data base. This second RRA was used to generate a second set of data limits.
- 4) The second set of data limits was then used to screen the data base further. A new RRA was again generated. The skewness values in this RRA were then evaluated, according to empirical criteria specified in section III.A.3 of this document for the winds, and according to criteria in section III.A.3 for the thermodynamic quantities. If these criteria were satisfied, the new RRA was then used to generate a final set of data limits, which were used to control the quality of the data base for the final version of the RRA.
- 5) Occasionally, the third RRA that was generated did not satisfy all of the skewness criteria. This indicated that some incorrect values were still present in the data base. To complete quality control, steps 3 and 4 were repeated for additional iterations (usually one or two) until the resulting RRA satisfied the skewness criteria. At that point, a final set of data limits was generated. This final set of data limits was then used to control the quality of the data base and generate the final RRA.

D. Organization of the Chapters

Because there are plans to publish a series of RRAs, comments on the special organization of the document are in order. The RRA document is arranged in four chapters. Chapter I is the introduction. Chapter II, Wind Statistics and Models, contains the techniques used to arrive at the wind statistical parameters, table I, and the probability functions that are to be used as wind models to derive several wind statistics. Chapter III, Statistics of Thermodynamic Quantities and Models, contains the techniques used to arrive at the thermodynamic and moisture-related statistical parameters given in tables II and III and the atmospheric thermodynamic model presented in table IV. This chapter also contains sets of equations to calculate several atmospheric properties. Chapter IV contains the general conclusions and recommendations. These four chapters are reprinted without change for each documented RRA to assure consistency and for expediency in preparing the documentation. To account for variations particular to a specific RRA, two appendixes have been included. Appendix A, Examples of Wind Statistics, is designed to give a few illustrative examples of wind statistics for the specific RRA and cursory observations, comparisons, or comments on wind statistics. Appendix B, Range Specific Information, is designed to present specific information particular to the range, such as geographical location, data base, etc., and any cursory observations or comments on the thermodynamic quantities.

Read these appendixes! They are located as the last two units in the document because they may vary in length depending on the circumstances. Appendixes A and B and tables I, II, III, and IV are the only differences among the RRA documents published in this new RRA series.

CHAPTER II. WIND STATISTICS AND MODELS

A. General Considerations

A.1. Objectives

An objective of the RRA is to furnish minimum tabulation for the wind statistics. To meet this objective, the bivariate normal probability distribution was adopted as a statistical model for the wind treated as a vector quantity at the RRA data levels. Only five statistical parameters are required to completely describe this probability function. In Cartesian coordinates these parameters are the means and standard deviations of the two orthogonal components and the correlation coefficient between the two components. These five statistical parameters for the U and V (meteorological coordinates) components are given in table I. The statistical properties of the bivariate normal probability distribution are used to derive many wind statistics that are of interest to the ranges and range users. This procedure produces consistent wind statistics that are connected through rigorous mathematical probability functions. By using these functions, extensive tabulations of wind statistics are avoided.

The statistical properties of the bivariate normal probability distribution presented for the vector wind statistical model are:

- 1) The wind components are univariate normally distributed.
- 2) The conditional distribution of one component given a value of the other component is univariate normally distributed.
 - 3) The windspeed is of the form of a generalized Rayleigh distribution.
 - 4) The frequency distribution of wind direction can be derived.
- 5) The conditional distribution of windspeed given a value of wind direction (wind rose) can be derived.
- 6) The five tabulated wind statistical parameters with respect to the meteorological U and V coordinate system can be derived for any arbitrary rotation of the orthogonal axes.

The probability distribution functions and sets of equations to derive wind statistics for the previously stated properties of the vector wind model are presented in this chapter. Symbols used are summarized in table A. Illustrative examples are presented in appendix A. No attempt is made to give the derivation of the probability functions. The reader is referred to Smith (1976) for some derivations and several applications of the probability distribution properties for wind statistics.

A.2. Data Quality Control

The U and V components of the wind were used to generate data limits set at plus and minus six standard deviations from the mean for each of the

TABLE A. LIST OF SYMBOLS USED IN CHAPTER II

- N The number of wind measurements in table I
- r A general variable for the bivariate normal probability distribution in polar coordinates
- R A generalized Rayleigh variable used for derived windspeed probability distribution
- R (U, V) The linear (product moment) correlation coefficient between the zonal and meridional wind components in table I
- SK (W) Skewness parameter for windspeed in table I
- S (U) The standard deviation of the zonal wind component in table I
- $S\ (V)$ The standard deviation of the meridional wind component in table I
- S (W) The standard deviation of windspeed in table I
- t A standardized normal variate used in text table B
- U The zonal wind component
- UBAR The mean value of the zonal wind component in table I
- V The meridional wind component
- $\ensuremath{\mathsf{VBAR}}$ The mean value of the meridional wind component in table I
- W Windspeed or modulus of wind vector, a scalar quantity
- WBAR The mean value of windspeed in table I
- X A general component variable or coordinate axis
- Y A general component variable or coordinate axis
- \bar{X} A general component mean value in the [x,y] coordinate system
- \overline{Y} A general component mean value in the [x,y] coordinate system
- a (alpha) Rotation angle for the [x,y] coordinate system

TABLE A. (concluded)

- θ (theta) Wind direction in the polar coordinate system
- $^{\lambda}(\)$ (Lambda) A parameter in the bivariate normal probability distribution in text table C
- $\boldsymbol{\xi}$ (Xi) The mean value in the standardized normal probability distribution used in text table \boldsymbol{B}
- π (Pi) Constant = 3.14159 ...
- ρ (Rho) The general linear correlation coefficient between the two component variables in the [x,y] coordinate system
- $\sigma_{\mathbf{x}},\sigma_{\mathbf{y}}$ The general standard deviations of the x and y component variables in the [x,y] coordinate system.

quantities. These data limits were used to screen the wind data base, as described in section I.C. The data base was considered to be free from errors under the following conditions:

- 1) The skewness of the windspeed was below 4.0 at data levels where the mean windspeed was less than 15 m/s, and
- 2) The skewness of the windspeed was below 2.5 at data levels where the mean windspeed was greater than 15 m/s.

A.3 Limitations

For the wind statistics, the correlation coefficients for like wind components and unlike wind components between altitude levels were not computed. Therefore, wind statistics with respect to altitude (profile) cannot be derived from the RRA statistics. For wind profile modeling techniques the user is referred to Smith (1976). However, the wind statistics at discrete altitudes are valid; all of the probability distribution functions given in chapter II can be derived from the five wind component statistical parameters contained in table I, and the derived distributions can be considered as wind models at discrete altitudes.

By convention, in the statistical literature Greek letters are used for population or theoretically known parameters, and sample estimates are denoted by English alphabetical letters or with a "hat" (^) over the Greek letters. In chapter II Greek letters are used for the variances and the linear correlation coefficient, and the means are denoted by \overline{X} and \overline{Y} when dealing with the bivariate normal distribution. It will always be understood that table I contains sample estimates of the statistical parameters and they are with respect to the meteorological U and V coordinate system.

B. Coordinate System and Computation of Statistical Parameters

B.1. Coordinate System

Wind measurements are recorded in terms of magnitude and direction. The wind direction is measured in degrees clockwise from true north and is the direction from which the wind is blowing. The wind magnitude (the modulus of the vector) is the scalar quantity and is referred to as windspeed or scalar wind. A statistical description that accounts for the wind as a vector quantity is appropriate and requires a coordinate system.

For the RRA the standard meteorological coordinate system has been chosen for the wind statistics, all tables of statistical parameters, and related discussions because the coordinate system used in aerospace and related applied fields has not always been consistent.

Using figure 1, the polar and Cartesian forms for the meteorological coordinate system are defined:

- W = windspeed, scalar wind, or magnitude of the wind vector in meters per second.
- θ = wind direction. θ is measured in degrees clockwise from true north and is the direction from which the wind is blowing.
- $\ensuremath{\mathsf{U}}\xspace = \ensuremath{\mathsf{zonal}}\xspace$ wind component, positive west to east, in meters per second.
- V = meridional wind component, positive south to north, in meters per second.

The components $\boldsymbol{\theta}$ and W define the polar form, and the U-V components define the Cartesian forms:

$$U = -W \sin \theta \quad , \quad 0 < \theta \le 360^{\circ} \tag{1}$$

$$V = -W \cos\theta \qquad . \tag{2}$$

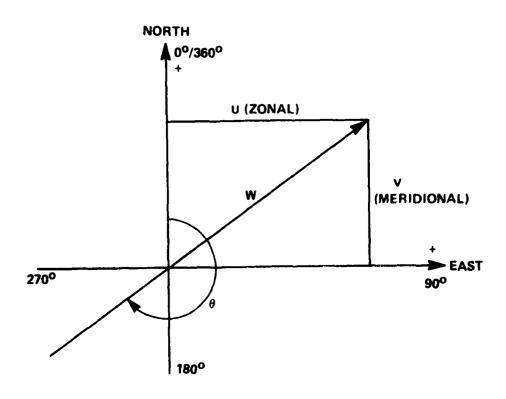


Figure 1. The meteorological coordinate system.

It is helpful to note the difference between the mathematical convention for a vector direction and the meteorological convention for wind direction:

$$\theta$$
 met = 270 - θ math (3)

when $0 \le \theta$ math $\le 270^{\circ}$

$$\theta$$
 met = 360 + (270 - θ math)

when $270 \le \theta$ math $\le 360^{\circ}$

B.2 Computation of Statistical Parameters

The wind statistical parameters in table I for the means and standard deviations of the U and V wind components and windspeed and the skewness parameter of windspeed were computed using the sums technique presented in chapter III.C.3. In addition, the linear (product moment) correlation coefficient between the U and V wind components, r (u,v) in table I, was computed. This correlation coefficient is defined as

$$\mathbf{r} (\mathbf{u}, \mathbf{v}) = \frac{\sum_{i=1}^{n} (\mathbf{U}_{i} - \overline{\mathbf{U}}) (\mathbf{V}_{i} - \overline{\mathbf{V}})}{\mathbf{N} \mathbf{s}(\mathbf{u}) \cdot \mathbf{s}(\mathbf{v})} . \tag{4}$$

These statistical parameters are with respect to the Standard Meteorological Coordinate System.

C. Statistical Wind Models

C.1. Wind Component Statistics

The univariate normal (Gaussian) probability distribution function is used to obtain wind component statistics. In generalized notations, this probability density function (pdf) is

$$f(t) = \frac{e^{-\frac{t^2}{2}}}{\sqrt{2\pi}}$$
, (5)

where t = X - ξ/σ_X is the standardized variate, with ξ defining the mean and σ_X the standard deviation. The probability distribution function (PDF) is

$$F(X) = \int_{-\infty}^{X} f(t) dt . \qquad (6)$$

Because this integral cannot be obtained in closed form, it is widely tabulated for zero mean and unit standard deviation. For a convenient reference for the RRA, selected values of F(X) are given in table B. To emphasize the connotation of probability, F(X) is shown in table B as $P\left\{X\right\}$.

The t values in table B are used as multiplier factors to the standard deviation to express the probability that a normally distributed variable, X, is less than or equal to a given value as

$$P\{X \leq \text{mean} + t \sigma_X\} = \text{probability}, p$$
 (7)

For example, when t=1.6449, the probability that X is less than or equal to the mean plus 1.6449 standard deviations is 0.95. That value of X that is less than or equal to the mean plus 1.6449 standard deviations is called the 95th percentile value of X. Also given in table B are the numerical values to express the probability that X falls in the interval X_1 and X_2 ; i.e.,

$$P\{X_1 \subseteq X \subseteq X_2\} = Interpercentile Range,$$
 (8)

where

$$X_1 = \widetilde{X} - t \circ_{\mathbf{X}}$$
$$X_2 = \widetilde{X} + t \circ_{\mathbf{X}} \qquad .$$

For t = 1.9602 the probability that X lies in the interval X_1 and X_2 is 0.95. The values of X_1 and X_2 in this example comprise the 95th interpercentile range.

For a normally distributed variable, the mode (most frequent value) and the median (50th percentile value) are the same as the mean value. The means and standard deviations of the U and V wind components from table 1 are used in equations (7) and (8) to compute the percentile values and interpercentile ranges of the U and V wind components. When equation (7) is illustrated on a normal probability graph, a straight line is formed.

C.2. The Vector Wind Model

Because wind is a vector quantity having direction and magnitude that can be expressed as two components in an orthogonal coordinate system, a probability model that describes the joint relationship is the bivariate normal probability distribution. In general component notation, the bivariate normal probability density function (BNpdf) is

TABLE B. VALUES OF t FOR STANDARDIZED NORMAL (UNIVARIATE) DISTRIBUTION FOR PERCENTILES AND INTERPERCENTILE RANGES

		AND INTERPERCEN	NTILE RANGES
t	P(X)	х	$P\{X_1 \leq X \leq X_2\} \ (^{C_{\epsilon}})$
-3.0000	0.00135	ε = 3.0000 σ	
-2.5758	0.00500	$\xi = 2.5758 \ \sigma$	
-2.3263	0.01000	ξ - 2.3263 σ	
-2.2365	0.01266	ξ - 2.2365 σ	
-2.0000	0.02275	ξ - 2.0000 σ	
-1.9602	0.02500	ξ - 1, 9602 σ	
-1.6449	0.05000	ξ - 1.6449 σ	
-1.2816	0.10000	ξ - 1.2816 σ	
-1.0000	0.15866	ξ - 1.0000 σ	
-0.8416	0.20000	ξ - 0.8416 σ	732) - (32) - (1)
-0.6745	0.25000	$\xi = 0.6745 \sigma$	(31, 732)
-0.2533	0.40000	$\xi = 0.2533 \sigma$	(80) ⁴ (40) 268 (31.7 (20) (10) (5) 45 (4.55) 468 (2.55 (2.00) (1.00) 73 (0.27)
0.0000	0.50000	ξ	
0,2533	0,60000	$\xi + 0.2533 \sigma$	20 20 10 10 10 10 10 10 10 10 10 10 10 10 10
0,6745	0,75000	$\xi + 0.6745 \sigma$	
0.8416	0,80000	$\xi + 0.8614 \sigma$	
1.0000	0,84134	ξ + 1.0000 σ	<u>+</u>
1.2816	0 . 9 0000	ξ +1.2816 σ	
1.6449	0.95000	ξ + 1.6449 σ	
1.9602	0.97502	ξ +1.9602 σ	
2.0000	0.97725	ξ + 2.0000 σ	
2.2365	0.98734	ξ +2.2365 σ	
2, 3263	0.99000	$\xi + 2.3263 \sigma$	
2.5758	0.99500	ξ + 2.5758 σ	
3,0000	0.99865	ξ 3.0000 σ	
			where $X_1 = \xi - t\sigma$ and $X_2 = \xi + t\sigma$

$$f(X,Y) = \frac{1}{2\pi\sigma_{X}\sigma_{y}} \sqrt{1-\rho^{2}} \left[\exp \frac{-1}{2(1-\rho^{2})} \left\{ \frac{(X-\overline{X})^{2}}{x^{2}} - \frac{2\rho(X-\overline{X})(Y-\overline{Y})}{\sigma_{X}\sigma_{y}} + \frac{(Y-\overline{Y})^{2}}{\sigma_{y}^{2}} \right\} \right] - \infty \leq X \leq \infty \text{ and}$$

$$-\infty \leq Y \leq \infty , \qquad (9)$$

where the five parameters are $\overline{x},\overline{y}$, the component means; σ_{x} , σ_{y} , the component standard deviations; and ρ , the correlation coefficient between the two component variables, X and Y.

For many applications the interest is in determining the probability that a point $\{X,Y\}$ will fall within a contour of equal probability density. The exponential terms of equation (9), when set equal to a constant, λ^2 , give a family of ellipses depending on the value of the constant. The ellipses have a common center at the point $\{\overline{X},\overline{Y}\}$. Integration of equation (9) over the region bounded by the contours of equal probability density gives

$$P(\lambda) = 1 - e^{\frac{-\lambda^2}{2(1 - \rho^2)}}$$
 (10)

Solving for λ^2 and replacing $P(\lambda)$ by p gives

$$\chi^2 = -2(1-y^2) \ln (1-p)$$
 (11)

Now define

$$\lambda_{e} = \sqrt{2} \sqrt{-\ln (1-p)}$$
 (12)

For ready reference and comparisons, $\lambda_{\rm e}$ is shown in table C for selected values of p.

TABLE C. VALUES OF λ FOR BIVARIATE NORMAL DISTRIBUTION ELLIPSES AND CIRCLES

	$\frac{\lambda}{\mathbf{e}}$	λ _c		λ _e	λ _c
P(')	(ellipse)	(circle)	P((ellispe)	(circle)
0.000	0.0000	0.0000	65,000	1.4490	1.0246
5,000	0.3203	0.2265	68.268	1.5151	1.0713
10.000	0.4590	0.3246	70.000	1.5518	1.0973
15,000	0.5701	0.4031	75.000	1.6651	1.1774
20.000	0.6680	0.4723	80,000	1.7941	1.2686
25,000	0.7585	0.5363	85.000	1.9479	1.3774
30.000	0.8446	0.5972	86.466	2.0000	1.4142
35,000	0.9282	0.6563	90.000	2.1460	1.5175
39.347	1.0000	0.7071	95.000	2.4477	1.7308
40.000	1.0108	0.7147	95.450	2.4860	1.7579
45,000	1.0935	0.7732	98.000	2.7971	1.9778
50,000	1.1774	0.8325	98.168	2.8284	2.0000
54.406	1.2533	0.8862	98.889	3.0000	2.1213
55,000	1.2637	0.8936	99.000	3.0348	2.1460
60.000	1.3537	0.9572	99. 730	3,4393	2.4320
63, 212	1.4142	1.0000	99.9877	4,2426	3,0000

 $\lambda_{c} = \sqrt{2} \times -\ln (1 - P)$ $\lambda_{c} = \sqrt{-\ln (1 - P)}$

The probability ellipse that contains p-percent of the wind vectors expressed in the most general form is the conic defined by

$$AX^2 + BXY + CY^2 + DX + EY + F = 0$$
, (13)

where

$$A = y_v^2$$

$$\mathbf{B} = -2 \mathbf{x} \mathbf{y}$$

$$c = x_x^2$$

$$D = 2c_{\mathbf{X}}c_{\mathbf{y}} \circ \overline{\mathbf{Y}} - 2c_{\mathbf{y}}^{2}\overline{\mathbf{X}} = -(B\overline{\mathbf{Y}} + 2A\overline{\mathbf{X}})$$

$$E = 2 \sqrt{x} \sqrt{y} + \overline{X} - 2 \sqrt{x} = - (B\overline{X} + 2C\overline{Y})$$

$$F = A\overline{X}^2 + C\overline{Y}^2 + B\overline{X}\overline{Y} - AC (1 - \rho^2) \lambda_e^2 ,$$

and

$$rac{1}{e} = \sqrt{2} \sqrt{-\ln (1-\rho)}$$
.

For graphical presentations, the range of the variable is important in order to arrange the scale. The largest and smallest values of X and Y for a given probability ellipse, p, are given by

$$X_{L,S} = \overline{X} \pm \sigma_{X} \lambda_{e}$$
 (14)

$$Y_{L,S} = \overline{Y} \pm \sigma_{V} \lambda_{e}$$
 (15)

where, as before,
$$\cdot_e = \sqrt{2} \sqrt{-\ln (1 - p)}$$
.

Although there are several approaches to graphing the probability ellipses, the following procedure is advantageous for electronic computer plotting. In establishing the computer plotting program, the sample estimates for $\overline{X}, \overline{Y}, \sigma_{\chi}, \sigma_{\chi}$, and p are constants in equation (13). The user makes the choice of probability ellipses desired. Thus, p in equation (12) is programmed as a parameter. The largest and smallest values for X and Y are computed by equations (14) and (15) for the largest probability ellipse selected. This sets the graphical scale. Values of X within the range of "X smallest" to "X largest" are obtained by incrementing X between these limits. Using the quadratic equation, a solution for Y of equation (13) is made and plotted for each value of X. The centroid (X,Y) for the family of probability ellipses is plotted as a point. Labeling and other identification complete the plotting program.

For a given probability, equation (13) defines an ellipse that contains p-percent of the points X,Y. Since the entire area under the bivariate normal density function [equation (9)] is unity, upon integration for a given probability ellipse, that given ellipse contains p-percent of the total area. In the wind statistics, p-percent of the wind vectors fall within the specified probability ellipse. From this point of view, a specified probability ellipse gives the joint probability that p-percent of the U-V components lie within the given ellipse.

When $\sigma_{\chi}^{2} = \sigma_{y}^{2} = \sigma^{2}$ and $\rho = 0$ in the bivariate normal distribution, the probability ellipses of equation (13) reduce to circles whose centers are at the means $\overline{X}, \overline{Y}$. The radii of the probability circles are $\sigma_{V1}^{\lambda}_{c}$, where

$$\sigma_{V1} = \sqrt{2\sigma^2} \tag{16}$$

and

$$\lambda_{C} = \sqrt{-\ln (1 - p)} \quad . \tag{17}$$

Values for $\lambda_{\rm C}$ for selected probabilities, p, are given in table C.

Because this function is simple, it can easily be graphed manually. However, the generalized plotting technique for electronic computer plotters, as represented by equation (13), can be advantageously used.

C.3. Derived Distributions for Wind Statistics

In this subsection the probability distribution functions and sets of equations are presented to derive certain probability distribution functions for wind statistics. These derived probability distributions are:

- 1) The conditional distribution of wind components
- 2) The generalized Rayleigh distribution for windspeed
- 3) The distribution for wind direction
- 4) The conditional distribution of windspeed given a wind direction (wind rose).

The required five statistical parameters for these derived distributions for wind statistics are given in table I.

C.3.1 The Conditional Distribution of Wind Components

Given that two random variables X and Y are bivariate normally distributed, the conditional distribution f(Y|X) is read as f(Y) given X, and likewise f(X|Y) is read as f(X) given Y. The conditional probability distribution function F(Y|X) has the mean E(Y|X) and variance $\sigma^2(x|y)$, where

$$E(Y|X^*) = \overline{Y} + \rho\left(\frac{\sigma_y}{\sigma_x}\right) (X^* - \overline{X})$$
 (18)

and

$$\sigma^2(y|x^*) = \sigma_y^2 (1 - \rho^2)$$
 (19)

The conditional standard deviation is

$$\sigma_{(\mathbf{y} \mid \mathbf{x}^*)} = \sigma_{\mathbf{y}} \sqrt{1 - \rho^2} \quad . \tag{20}$$

By interchanging the variables and parameters, the conditional distribution function for $F(X|Y^*)$ has the conditional mean

$$E(X|Y^*) = \overline{X} + \wp\left(\frac{\sigma_X}{\sigma_y}\right) (Y^* - \overline{Y}) , \qquad (21)$$

conditional variance

$$\sigma^{2}(\mathbf{x}|\mathbf{y}^{*}) = \sigma_{\mathbf{x}}^{2} (1 - \rho^{2}) \qquad (22)$$

and conditional standard deviation

$$\sigma_{(\mathbf{x}|\mathbf{y}^*)} = \sigma_{\mathbf{x}} \sqrt{1-\rho^2} \quad . \tag{23}$$

The preceding conditional probability distribution functions are univariate normal distributions for a (fixed) given value for one of the bivariate normal variables. Thus, the t-values given in table B are applicable for conditional probability statements. For example,

$$F(Y|X^*) = E(Y|X^*) + t\sigma_{(Y|X^*)}$$
 (24)

For t = 1.6449 there is a 95 percent chance that Y is less than or equal to \overline{Y} + 1.6449 $\sigma_{(y|x^*)}$ given that X = X*. In symbols this statement reads

$$P\left\{Y \leq E(Y|X^*) + 1.6449 \ \sigma_{(y|X^*)} \ | X = X^*\right\} = 0.9500$$
 (25)

Interval probability statements can also be made; namely,

$$P \left\{ Y_1 = E(Y | X^*) - to_{(y|X^*)} \le Y \le Y_2 = E(Y | X^*) + to_y | X = X^* \right\}$$

where X* can take on any fixed value of X, but a convenient arrangement is to let X* = $\overline{X} \pm t\sigma_v$.

The close connection of the regression function of Y on X to the conditional mean for the bivariate normal distribution is noted; namely,

$$Y = \vec{Y} + \rho \left(\frac{\sigma_{\mathbf{Y}}}{\sigma_{\mathbf{X}}} \right) (X - \vec{X}) \qquad (26)$$

Similarly, the regression function of X on Y is

$$X = \overline{X} + i \left(\frac{\sigma_{Y}}{\sigma_{X}}\right) (Y - \overline{Y}) \qquad (27)$$

These are linear functions and express the same results as would be obtained from a least-squares regression line.

C.3.2. The Generalized Rayleigh Distribution for Windspeed

If two random variables, X and Y, are bivariate normally distributed, then the probability distribution for the modulus, R, can be derived in terms of the five parameters that define the bivariate normal distribution.

$$R = \sqrt{X^2 + Y^2} \tag{28}$$

The distribution of R so derived is called a generalized Rayleigh distribution because there are no restrictions on the parameters. For applications to the RRA, the variable R is recognized as windspeed or the modulus of the wind vector.

The probability density function for R is expressed as

$$f(R) = a_0 R e^{-a_1 R^2} \left[I_0(a_2 R^2) I_0(a_3 R) + 2 \sum_{k=1}^{\infty} I_k(a_2 R^2) I_{2k}(a_3 R) \cos 2k\psi \right] R \ge 0 .$$
 (29)

The functions $I_0(\cdot)$, $I_k(\cdot)$, and $I_{2k}(\cdot)$ are the modified Bessel functions of the first kind for zero order, kth order, and 2kth order. The coefficients are

$$\mathbf{a_0} = \exp \left[-\frac{1}{2} \left\{ \frac{\mathbf{\bar{X}}^2}{\sigma_{\mathbf{a}}^2} + \frac{\mathbf{\bar{Y}}^2}{\sigma_{\mathbf{b}}^2} \right\} \right] / \sigma_{\mathbf{a}} \sigma_{\mathbf{b}} ,$$

where $\sigma_a^{\ 2}$ and $\sigma_b^{\ 2}$ are the rotated variances to produce zero correlation between X and Y. $\sigma_a^{\ a}$ and $\sigma_b^{\ b}$ are the positive and negative roots of the expression

$$z^{2}_{(+,-)} = \frac{1}{2} \left\{ z_{x}^{2} + z_{y}^{2} \pm \left[(\sigma_{x}^{2} + \sigma_{y}^{2})^{2} - 4\sigma_{x}^{2} \sigma_{y}^{2} (1 - \rho^{2}) \right]^{1/2} \right\} ,$$

$$a_{1} = (z_{x}^{2} + z_{y}^{2})/4(1 - \rho^{2}) \sigma_{x}^{2} \sigma_{y}^{2} ,$$

$$a_{2} = \frac{\left[(\sigma_{x}^{2} - \sigma_{y}^{2})^{2} + 4\sigma_{x}^{2} \sigma_{x}^{2} \sigma_{y}^{2} \right]^{1/2}}{4(1 - \rho^{2}) \sigma_{x}^{2} \sigma_{y}^{2}} ,$$

$$a_3 = \left[\left(\frac{\bar{X}}{\sigma_a^2} \right)^2 + \left(\frac{\bar{Y}}{\sigma_b^2} \right)^2 \right]^{1/2} ,$$

$$\begin{bmatrix} \sigma_{\mathbf{x}}^{2} - \mathbf{K} & \sigma_{\mathbf{x}} \sigma_{\mathbf{y}} \rho \\ \\ \sigma_{\mathbf{x}} \sigma_{\mathbf{y}} \rho & \sigma_{\mathbf{y}}^{2} - \mathbf{K} \end{bmatrix}.$$

where K is $\sigma^2_{(+,-)}$, and σ_a and σ_b are analogous to the standard deviation of the major and minor axes of the bivariate normal probability ellipse.

^{1.} This computational form is obtained from the determinant

and

$$\tan \psi = \frac{\overline{Y}}{\overline{X}} \frac{\sigma_a^2}{\sigma_b^2} .$$

Since this density function cannot be integrated in closed form from zero to R, numerical integration is used to obtain practical results for the probability distribution function; i.e.,

$$F(R) \approx \int_{0}^{R*} f(R) dR \qquad . \tag{30}$$

A number of special cases can be obtained from the general Rayleigh distribution [equation (29)], the simplest of which is to let $\sigma_{X} \equiv \sigma_{y} = \sigma$ and $\overline{X} = \overline{Y} = 0$ with independent variables X and Y. This gives

$$f(R) = \frac{R}{\sigma^2} e^{-R^2/2\sigma^2} , \qquad (31)$$

which is recognized as the classical Rayleigh probability density function. The density function, equation (31), can be integrated in closed form over any range of the variable R. Hence, the probability distribution function, F(R), for equation (31) is

$$F(R) = 1 - exp \left\{ \frac{-R^2}{2\sigma^2} \right\}$$
 (32)

C.3.3. The Derived Distribution of Wind Direction

Considering the wind as a vector quantity and bivariate normally distributed, the wind direction can be derived. This is done by first writing the bivariate normal probability density function in polar coordinates whose variables are

$$g(\mathbf{r}, \theta) = rd_1 e^{\frac{1}{2}(a^2r^2 - 2br + c^2)},$$
 (33)

where

$$a^{2} = \frac{1}{(1 - \rho^{2})} \left[\frac{\sin^{2}\theta}{\sigma_{\mathbf{x}}^{2}} - \frac{2\rho \cos\theta \sin\theta}{\sigma_{\mathbf{x}}^{3} \mathbf{y}} + \frac{\cos^{2}\theta}{\sigma_{\mathbf{y}}^{2}} \right] ,$$

$$b = \frac{-1}{(1 - \rho^{2})} \left[\frac{\mathbf{x} \sin\theta}{\sigma_{\mathbf{x}}^{2}} - \frac{\rho(\mathbf{x} \cos\theta + \mathbf{y} \sin\theta)}{\sigma_{\mathbf{x}}^{3} \mathbf{y}} + \frac{\mathbf{y} \cos\theta}{\sigma_{\mathbf{y}}^{2}} \right] ,$$

$$c^{2} = \frac{1}{(1 - \rho^{2})} \left[\frac{\mathbf{x}^{2}}{\sigma_{\mathbf{x}}^{2}} - \frac{2\rho \mathbf{x} \mathbf{y}}{\sigma_{\mathbf{x}}^{3} \mathbf{y}} + \frac{\mathbf{y}^{2}}{\sigma_{\mathbf{y}}^{2}} \right] ,$$

$$d_{1} = \frac{1}{2\pi\sigma_{\mathbf{x}}^{3} \mathbf{y}} \sqrt{1 - \rho^{2}} ,$$

 $r=\sqrt{x^2+y^2}$ is the modulus of the vector or speed, and θ is the direction of the vector. After integrating $g(r,\theta)$ over r=0 to ∞ , the probability density function of θ is

$$g(\theta) = \frac{d_1}{a^2} e^{-\frac{1}{2}c^2} \left[1 + \sqrt{2\pi} \left(\frac{b}{a} \right) e^{\frac{1}{2} \left(\frac{b}{a} \right)^2} - \phi \left(\frac{b}{a} \right) \right] , \qquad (34)$$

^{2.} This expression, equation (33), in Smith 1976) is given with respect to the mathematical convention for a vector direction.

where a2, b, c2, and d_1 are as previously defined in equation (33) and

$$\div \left(\frac{b}{a}\right) = \div (x) = \frac{1}{\sqrt{2\pi}} \int_{-\pi}^{X} e^{-\frac{1}{2}t^2} dt$$

is taken from tables of normal distribution functions or made available through a computer subroutine.

If desired, equation (34) can be integrated numerically over a chosen range of θ to obtain the probability that the vector direction will lie within the chosen range; i.e.,

$$F(\theta) = \int_{\theta_2}^{\theta_1} g(\theta) d\theta . \qquad (35)$$

One application may be to obtain the probability that the wind will flow from a given quadrant or sector as, for example, onshore.

C.3.4. The Derived Conditional Distribution of Windspeed Given the Wind Direction (Wind Rose)

Continuing with the considerations in section C.3.3. of this chapter, the conditional probability density function (pdf) for windspeed, r, given a specified value for the wind direction, θ , can be expressed as

$$f(\mathbf{r} \mid \theta) = \frac{a^2 \mathbf{r} e^{-\frac{1}{2} (a^2 \mathbf{r}^2 - b\mathbf{r})}}{1 + \sqrt{2\pi} \left(\frac{b}{a}\right) e^{\frac{1}{2} \left(\frac{b}{a}\right)^2} : \left\{\frac{b}{a}\right\}},$$
 (36)

where the coefficients, <u>a</u> and <u>b</u> and the function $\{\frac{b}{a}\}$ are as previously defined in equation (33) and in equation (34).

From equation (36) the mode (most frequent value) of the conditional windspeed given a specified value of the wind direction is the positive solution of the quadratic equation,

$$a^2 r^2 - br - 1 = 0$$
 , (37)

which is

$$(\mathbf{r}\mid \theta) = \frac{1}{2a} \left[\left(\frac{\mathbf{b}}{\mathbf{a}} \right) + \sqrt{4 + \left(\frac{\mathbf{b}}{\mathbf{a}} \right)^2} \right]$$
 (38)

The locus of the conditional modal values of windspeed when plotted in polar form versus the given wind directions forms an ellipse.

The noncentral moment for equation (36) is expressed as

$$\mu_{\mathbf{n}}' = \int_{0}^{\infty} \mathbf{r}^{\mathbf{n}} \mathbf{f}(\mathbf{r} | \theta) d\mathbf{r} . \qquad (39)$$

Now the first noncentral moment is identical to the first central moment or the expected value, E $(r|\theta)$. The integration of equation (39) for the first moment is sufficiently simple to yield practical computations and can be expressed as

$$E(\mathbf{r}^{\dagger}e) = \frac{\left(\frac{b}{a}\right) + \left[1 + \left(\frac{b}{a}\right)^{2}\right] \sqrt{2\pi} e^{\frac{1}{2}\left(\frac{b}{a}\right)^{2} + \left\{\frac{b}{a}\right\}}}{a\left[1 + \left(\frac{b}{a}\right) \sqrt{2\pi} e^{\frac{1}{2}\left(\frac{b}{a}\right)^{2}} + \left\{\frac{b}{a}\right\}\right]}.$$
 (40)

Hence, equation (40) gives the conditional mean value of the windspeed given a specified value for the wind direction.

The integration of equation (36) for the limits r=0 to $r=r^*$ gives the probability that the conditional windspeed is $\leq r^*$ given a value for the wind direction, θ . This conditional probability distribution (PDF) can be written as

$$\Pr\left\{\mathbf{r} \leq \mathbf{r}^* \mid \mathbf{a} = \mathbf{\theta}_0\right\} = 1 - \left[\frac{e^{-\frac{1}{2}\mathbf{r}_S^2 + \sqrt{2\pi}\left(\frac{\mathbf{b}}{\mathbf{a}}\right)\left\{1 - \mathbf{\phi}\left(\mathbf{r}_S\right)\right\}}}{e^{-\frac{1}{2}\left(\frac{\mathbf{b}}{\mathbf{a}}\right)^2 + \sqrt{2\pi}\left(\frac{\mathbf{b}}{\mathbf{a}}\right)\mathbf{\phi}\left(\frac{\mathbf{b}}{\mathbf{a}}\right)}}\right]. \tag{41}$$

where
$$r_s = \left[a r^* - \left(\frac{b}{a} \right) \right]$$

By definition, equation (41) is an expression for a "wind rose." Empirical wind rose statistics are often tabulated or graphically illustrated giving the frequency that the windspeed is not exceeded for those windspeed values that lie within assigned class intervals of the wind direction. After evaluation of equation (41) for various values of windspeed, r*, and the given wind directions, \$\tilde{\theta}\$, interpolations can be performed to obtain various percentile values of the conditional windspeed.

For the special case when <u>b</u> in equation (33) equals zero (i.e., for x = y = 0), the conditional modal values of windspeeds [equation (38)], the conditional mean values of windspeeds [equation (40)], and the fixed conditional percentile values of windspeeds [interpolated from evaluations of equation (41)], when plotted in polar form versus the given wind directions, produce a family of ellipses.

For the special case when $\bar{x} = \bar{y} = 0$, equation (36) reduces to the following simple case:

$$\Pr\left\{\mathbf{r} + \mathbf{r}^* + \cdots = \cdots_0\right\} = 1 - e^{-\frac{\mathbf{a}^2 \mathbf{r}^*}{2}}$$
 (42)

There is a special significance of equation (42) when related to the bivariate normal probability distribution. If r^* and θ are measured from the centroid of the probability ellipse, then the probability that $r \le r^*$ is the same as the given probability ellipse. Further, solving equation (42) for r^* , gives

$$r^* = \frac{1}{a} \sqrt{-2 \ln (1 - P)}$$
 (43)

If a probability ellipse P is chosen, equation (42) gives the distance of r along any θ from the centroid of the ellipse to the intercept of the specified probability ellipse. If there is an interest in conditional probability of winds for a given θ relative to the monthly means, equation (43) is applicable. If it is desired to find the magnitude of the wind along any θ relative to the monthly mean to the intercept of a given probability ellipse, equation (43) is applicable.

D. Statistical Parameters With Respect To Any Orthogonal Axes

The five wind statistical parameters presented in table I are given with respect to the standard meteorological coordinate system; i.e., these parameters are for the U and V components. For many aerospace vehicles and range applications, there is a need for wind statistics with respect to orthogonal axes other than west to east and south to north. For example, it may be required to present wind statistics with respect to a flight azimuth of an

aerospace vehicle whose flight azimuth is α degrees from true north measured in a clockwise direction. The following sets of equations are presented to compute the five parameters for the new coordinate axes rotated α degrees clockwise from true north.

a. Rotation of the means through α degrees:

$$\overline{X}_{ij} = \overline{X} \cos (90 - \omega) + \overline{Y} \sin (90 - \omega)$$
 (44)

$$\overline{Y}_{x} = \overline{Y} \cos (90 - \alpha) - \overline{X} \sin (90 - \alpha)$$
 (45)

b. Rotation of the variances through α degrees:

$$\sigma_{\mathbf{x}_{,1}}^{2} = \sigma_{\mathbf{x}}^{2} \cos^{2} (90 - \alpha) + \sigma_{\mathbf{y}}^{2} \sin^{2} (90 - \alpha)$$

$$+ 2\rho \sigma_{\mathbf{x}} \sigma_{\mathbf{y}} \cos (90 - \alpha) \sin (90 - \alpha)$$
(46)

$$\sigma_{\mathbf{y}_{\alpha}}^{2} = \sigma_{\mathbf{y}}^{2} \cos^{2} (90 - \alpha) + \sigma_{\mathbf{x}}^{2} \sin^{2} (90 - \alpha)$$

$$- 2\rho\sigma_{\mathbf{x}}\sigma_{\mathbf{y}} \cos (90 - \alpha) \sin (90 - \alpha) . \tag{47}$$

c. Rotation of the linear correlation coefficient through α degrees:

$$\rho_{\alpha} = \frac{\operatorname{cov}(X,Y)_{\alpha}}{{}^{\sigma} x_{\alpha} {}^{\sigma} y_{\alpha}} , \qquad (48)$$

where cov $(X,Y)_{\alpha}$ is the rotated covariance,

cov
$$(X,Y)_{\alpha} = \text{cov } (X,Y) [\cos^2 (90 - \alpha) - \sin^2 (90 - \alpha)]$$

+ $\cos (90 - \alpha) \sin (90 - \alpha) (\sqrt[3]{v} - \sqrt[3]{x})$

and

$$cov(X,Y) = \log_x \sigma_y$$

By using these rotational equations, the bivariate normal distribution with respect to any desired rotated coordinates can be obtained from sample estimates that have been computed with respect to a specific axis. The marginal distributions after rotation are also normally (univariate) distributed. Using the rotational equations greatly reduces computational efforts for applications requiring statistics with respect to several coordinate axes.

Appendix A presents some illustrative examples for the wind statistics of the specific RRA.

CHAPTER III. STATISTICS OF THERMODYNAMICS QUANTITIES AND MODELS

A. General Considerations

A.1. Objectives

The objective inherent in developing the thermodynamic section of the RRA was to describe the thermodynamic characteristics of the atmosphere using a minimum of data tabulations. A set of parameters was selected which, together, thermodynamically describe the climatological state of the atmosphere. These parameters are the pressure, temperature, density, dewpoint, virtual temperature, and water vapor pressure. Used together, these parameters permit the calculation of a large number of derived quantities. (Symbols used in the calculations in this chapter are summarized in table D.) Some of these quantities, such as the speed of sound, are dealt with in section III.E.

The probability distribution of each of the six thermodynamic RRA parameters is described by its mean value, its standard deviation, and its skewness. Several of these parameters (temperature, pressure, dewpoint and density) have probability distributions that are close to a univariate normal distribution; the others do not. The skewness parameter gives an estimate of the asymmetrical departures of a probability distribution.

Hydrostatically modeled mean values of pressure and density were calculated (table IV), so that users may determine the departure of the actual climatological values of these parameters from hydrostatic conditions. This was done by hydrostatically integrating the pressure from the lowest RRA data level to the termination altitude of the particular RRA.

A.2. Data Quality Control

Data limits derived from the following parameters were used to screen the thermodynamic portion of the RRA data base: temperature, pressure, dewpoint (for the 0- to 30-km portion only), and density (for the 30- to 70-km portion only). These limits were set to plus and minus six standard deviations from the mean values of each of these quantities. These limits were used to screen the thermodynamic portion of the RRA data base, according to the procedures described in section I.C. The data base used to generate the thermodynamic portion of the RRA (tables I, II, and IV) was considered to be free from errors under the following conditions:

- a) The skewness values of the pressure and temperature were between -2.5 and 2.5 at all data levels.
- b) The skewness values of the density were between -3.5 and 3.5 at data levels between 0 and 30 km.
- c) The skewness values of the density were between -3.0 and 3.0 at data levels between 30 and 70 km.
- d) The skewness values of the dewpoint were between -2.5 and 2.5 at all data levels with more than 10 data values.

TABLE D. LIST OF SYMBOLS USED IN CHAPTER III

C - Speed of sound

 \mathbf{C}_d Collision diameter

E - Vapor pressure

g. Gravity at latitude:

H Geopotential height

 H_{m}^{-} Geopotential height at a mandatory radiosonde data level

 H_{ζ}^{-} - Geopotential height at a significant radiosonde data level

 K_{t} Coefficient of thermal conductivity

L - Mean free path length

M - Mean molecular weight of air at sea level

M3Q - Annual or monthly third moment of quantity Q

n - Refractive modulus

N - Refractive index

NA - Avogadro's constant

No Number of values of quantity Q

P - Pressure

P_m Pressure at a mandatory radiosonde data level

P_c Pressure at a significant radiosonde data level

 $P_{\rm h}$ Hydrostatically integrated mean monthly or annual pressure

Q - Any tabulated RRA quantity

R* - Universal gas constant

R' - Specific gas constant of dry air

r', r* Parameters used in converting z to h and vice versa

TABLE D. (concluded)

S Sutherland's constant, used in the calculation of dynamic viscosity

T - Temperature

T_d - Dew point

 $T_{_{_{\mathbf{U}}}}$ - Virtual temperature

T. Virtual temperature at a mandatory radiosonde data level

 T_{ye} - Virtual temperature at a significant radiosonde data level

V - Mean air particle speed

V_e - Mean collision frequency

 Parameter used in the hydrostatic interpolation of pressure and density

Z - Geometric altitude

Wavelength

 ${}^{\circ}Q$ - Skewness of quantity Q

- Constant used in the equation for viscosity

- Ratio of specific heat at constant pressure to specific heat at constant volume

- Kinematic coefficient of viscosity

Dynamic coefficient of viscosity

Density

.h - Mean monthly or annual density derived from pressure height

Standard deviation of the quantity Q

A.3. Limitation of Thermodynamic Statistics

The correlation coefficients between the thermodynamic quantities and the moisture-related quantities were not calculated at discrete altitudes, nor were any of the correlations between altitudes. Therefore, valid statistical dispersion models that require the relationship between two or more of these quantities at the same altitude or between altitudes cannot be derived. Approximations for the correlation coefficients between pressure, virtual temperature, and density at discrete altitudes may be obtained from the coefficients of variation as developed by Buell (1970). The coefficient of variation is the standard deviation divided by the mean. The mean values and the standard deviations are taken from table II. A model for the profile of monthly and annual mean pressure, virtual temperature, and density that is in excellent agreement with the respective statistical mean values is given by table IV. This agreement results because the physical relationships, given by the hydrostatic equation and the equation of state, were used to derive table IV. When only the monthly or annual mean values for pressure, virtual temperature, and density are required, it is recommended that table IV be used.

B. Establishing Data Samples at the Required Altitude Levels

This section describes the computational procedures used to establish data samples of the thermodynamic RRA parameters at the RRA data levels. References are cited only when an equation given is one of many available in the literature or when an equation is stated in an unusual form.

B.1. Conversion of Data Recorded in Geopotential Heights to Geometric Altitude

The upper air rocketsonde observations used to obtain the table values above 30 km were recorded in terms of geometric altitude and can be interpolated directly to the altitude intervals shown in the tables. However, the radiosonde observations used to obtain the tabular values below 30 km were recorded in terms of geopotential heights. The change of coordinates from geopotential heights to geometric altitudes (h to z) is accomplished by calculating a table of geopotential heights that correspond exactly to the geometric altitudes at which the atmospheric parameters are tabulated. The radiosonde observations are then interpolated to these goepotential heights. The relationship used to calculate geometric altitude from geopotential height is

$$H = (r'z)/(r*z) \qquad . \tag{49}$$

where

$$r' = gr*/9.80665$$

and

$$r^* = -2g_{\frac{1}{2}}/(3g_{\frac{1}{2}}/2g_{0})$$
.

g is the sea-level gravity at the latitude ϕ corresponding to the proper location. This value is given by (List, 1968)

$$g_1 = 9.780356 (1 + 5.2885 + 10^{-3} \sin^2 - 5.9 + 10^{-6} \sin^2 (2^{-1})).$$
 (50)

 $\frac{\partial g_{p}}{\partial z_{0}}$ is the rate of change of gravity at the sea level. This quantity is given

by the equation

$$\frac{g}{20} = -3.085462 + 10^{-6} + 2.27 + 10^{-9} \cos(2z) - 2 + 10^{-12} \cos(4z).$$
 (51)

The units used for gravity are meters per square second, while the units for

$$\frac{\partial g}{\partial z_0}$$
 are per square second.

The resulting table of values of H obtained by using even increments of 2 in equation (49) is shown in table IV of the RRA. The values of H above 30 km are not used in the interpolation of original data, but are included for the convenience of the user.

B.2. Calculations on the Original Rawinsonde Data Records

It was necessary to interpolate the information from the original rawin-sonde data records to the geometric altitudes specified as the RRA data levels. The parameters for which this interpolation was required were the temperature, dewpoint, and pressure. The other parameters were calculated from the interpolated values at each RRA data level. These "derived" parameters were the water vapor pressure, density, and virtual temperature.

B.2.1. Calculation of the Geopotential Height at Significant Levels

Two somewhat different interpolation procedures were used to obtain data from radiosonde and rocketsonde observations at the levels shown in the tables. The procedure used to interpolate radiosonde observations began with the calculation of virtual temperature at each data level in a sounding. The virtual temperature was computed by

$$T_v = T/(1. - 0.379 (e/p))$$
 , (52)

where $\mathbf{T}_{\mathbf{v}}$ and \mathbf{T} are in degrees Kelvin and \mathbf{e} and \mathbf{p} are in millibars.

The radiosonde soundings contain a mix of data taken at "mandatory" and "significant" levels. Pressure, temperature, and dewpoint information was given in these soundings at both types of levels. However, geopotential height information was only given at the mandatory levels. The heights at the significant levels were "filled in" (calculated) hydrostatically using pressure and temperature data from these levels. This procedure permitted the use of most of the significant level data in the calculation of the RRA tables. The equation used for this process was

$$H_{s} = H_{m} + 29.2712617 \frac{(T_{vs} - T_{vm})}{2} \ln(P_{s}/P_{m})$$
, (53)

where the subscripts s and m denote quantities at significant and mandatory levels. This equation was not used if the difference between two adjacent mandatory levels was greater than 200 mb. All soundings with such data gaps were rejected for use in compiling the RRA.

B.2.2. Temperature

Radiosonde temperatures were interpolated logarithmically with respect to pressure using the equation ${\sf respect}$

$$T = T_U + (T_L - T_U) \frac{\ln p - \ln p_L}{\ln p_U - \ln p_L}$$
, (54)

where the subscripts U and L indicate values at the nearest data levels in the actual sounding above and below the interpolated level.

B.2.3. Pressure

The pressure values in each radiosonde sounding were interpolated to the RRA data levels using the equation

$$p = p_{L} exp\left(\frac{H_{L} - H_{U}}{29.2712617(0.5)(T_{V_{U}} + T_{V_{L}})}\right)$$
(55)

where the subscript L indicates virtual temperature, geopotential height, and pressure values at the data level below and closest to the level at which data were required.

B.2.4. Dewpoint Temperature

$$T_{d} = T_{dU} + (T_{dL} - T_{dU}) \left(\frac{\ln p - \ln p_{L}}{\ln p_{U} - \ln p_{L}} \right) . \tag{56}$$

The subscripts U and L indicate data at the nearest upper and lower data levels in a sounding.

B.2.5. Derived Water Vapor Pressure

The water vapor pressure was calculated from the interpolated dewpoint values at the RRA data levels using Teten's approximation:

$$7.5(T_d - 273.15)/(T_d - 35.86)$$

e = 6.11 mb × 10 . (57)

B.2.6. Derived Density

The density values derived from radiosonde observations were calculated at the RRA data levels using the equation

$$p = 348.36787 \text{ p/T}_{V}$$
 (58)

B.2.7. Derived Virtual Temperature

The virtual temperature values were calculated at the RRA data levels for each sounding using the equation

$$T_{V} = T/(1 - 0.379(e/p))$$
 (59)

where T_{v} and T are in degrees Kelvin, and p and e are the pressure and vapor pressure, respectively, in millibars.

B.3. Calculations on the Original Rocketsonde Data Records

The rocketsonde data records used to calculate the RRA table values above 30 km were given in terms of geometric altitude. For this reason, slightly different calculations were required to convert the recorded data values to values at the RRA data levels. The pressure, temperature, and density were all interpolated to the RRA data levels; moisture-related parameters (virtual temperature, water vapor pressure, and dewpoint) were not calculated, since atmospheric moisture at altitudes above 30 km was considered to be negligible.

No interpolation was done across gaps in the pressure or temperature data within a sounding larger than 7,000 m. Data values at the RRA levels within such a gap were set to missing.

B.3.1. Temperature

Rocketsonde temperatures were interpolated linearly with respect to geometric altitude using the equation

$$T = T_U + (T_L - T_U) \frac{Z - Z_L}{Z_L - Z_L}$$
, (60)

where the subscripts U and L indicate values at the nearest data level in the actual sounding above and below the interpolated level.

B.3.2. Pressure

The pressure values in each rocketsonde sounding were interpolated to the RRA data levels using the equation

$$P = P_{L} \exp \left(-\frac{g_{\phi}}{R^*} \frac{M(Z - Z_{L})}{\overline{T}v} \cdot W^2\right) , \qquad (61)$$

where $\overline{T}_V = \frac{T_{VU} + T_{VL}}{2}$ and $W = \frac{r^*}{\left(r^* + Z + \frac{Z - Z_L}{2}\right)}$.

B.3.3. Density

Rocketsonde density values were interpolated using the equation

$$\rho = \rho_{L} \exp \left(-\frac{g_{\phi}^{M}}{R^{*}} \frac{(Z - Z_{L})}{\overline{T_{v}}} \cdot w^{2} \right) \quad . \tag{62}$$

where W is specified in section III.B.3.2.

C. Computation of Statistical Parameters for Tables II and III

A three-step procedure was used for computing the monthly and annual means, standard deviations, and skewness values from the data values at the RAA data levels. Initially, certain statistical sums were calculated and stored as the soundings in the data base were processed. These sums were then used to calculate the monthly statistics given in the RRA tables. The annual statistics were then calculated from these stored sums and the monthly statistics.

C.1. Stored Statistical Sums

The sums calculated were

$$\sum Q$$
, $\sum Q^2$, and $\sum Q^3$,

where Q is any one of the quantities given in the thermodynamic part of the RRA.

C.2. Calculation of the Monthly Statistics

C.2.1. Monthly Means

The mean monthly values of the thermodynamic RRA quantities were calculated using the equation

$$\bar{Q} = \sum_{Q} Q/N_{Q}$$
,

where $N_{\tilde{Q}}$ is the number of observed values of the quantity Q for a given month.

C.2.2. Monthly Standard Deviations

The monthly standard deviations of the thermodynamic RRA quantities were calculated using the equation

$$\sigma_{Q} = \sqrt{\frac{(N_{Q} \Sigma' Q^{2}) - (\Sigma Q)^{2}}{N_{Q} \cdot (N_{Q} - 1)}} . \tag{63}$$

C.2.3. Monthly Skewness Values

The monthly skewness values of the windspeed and of the thermodynamic RRA quantities were calculated using the equation

$$\alpha_{\mathbf{Q}} = \frac{M3_{\mathbf{Q}}}{^{\circ}_{\mathbf{Q}}} \quad ,$$

where M3 $_{\rm Q}$ is the third moment of the quantity Q, $\sigma_{\rm Q}$ is its standard deviation, and

$$M_{3Q} = \left[\frac{\chi_{Q}^{3}}{N_{Q}} - \frac{3\chi_{Q}\chi_{Q}^{2}}{N_{Q}^{2}} - \frac{2\chi_{Q}^{3}}{N_{Q}^{3}} \right] \cdot \frac{N_{Q}^{2}}{(N_{Q} - 1)(N_{Q} - 2)}$$
(64)

C.3. Calculation of the Annual Statistics

Equations (63) and (64), used to calculate the monthly values of the standard deviations and skewness values, involve taking the differences between two pairs of large sums containing Q^2 and Q^3 , where Q is any thermodynamic RRA quantity. Using these equations to compute the annual statistics would have resulted in a substantial loss of precision, as these sums become larger by several orders of magnitude in such a case. This problem was avoided by calculating the annual means, standard deviations, and skewness values from the monthly statistics.

C.3.1 Annual Mean Values

The annual mean values of the thermodynamic RRA quantities were calculated using the equation ${\sf NRA}$

$$Q_{ANN} = Q_A/N_Q$$

where Q_{A} is the total of all observed values of Q and N_{Q} is the total number of observations of Q.

C.3.2. Annual Standard Deviations

$$Q_{ANN} = \sqrt{\frac{1}{N_{Q}} \sum_{i=1}^{12} (N_{Qi} Q_{i}^{2}) + \frac{1}{N_{Q}} \sum_{i=1}^{12} (N_{Qi} \overline{Q}_{i}^{2}) - Q_{ANN}^{2}}, (65)$$

where N_{Qi} = the number of data values for Q in month i (i = 1 to 12), Q_i = the monthly mean of Q, and σ_{Qi} = the standard deviation of quantity Q in month i.

C.3.3. Annual Skewness Values

The annual skewness values of the thermodynamic RRA quantities were calculated using the equation

$$M3Q_{ANN} = \frac{1}{N} \sum_{i=1}^{12} (N_{Qi} M_{3Qi}) + \frac{3}{NQ_{ANN}} \sum_{i=1}^{12} (N_{Qi} \ddot{Q}_i - Q_i^2)$$

$$+ \frac{1}{NQ_{ANN}} \sum_{i=1}^{12} (N_{Q_i} Q_i^3) - \frac{3\tilde{Q}_{ANN}}{NQ_{ANN}} \sum_{i=1}^{12} (N_{Q_i} Q_i^2)$$

$$-\frac{3\overline{Q}_{ANN}}{N\overline{Q}_{ANN}}\sum_{i=1}^{12} (N_{Qi} \circ_{Qi}^{2}) + 2\widetilde{Q}_{ANN}^{3} , \qquad (66)$$

where $\rm M_{3Qi}$ = the third moment about the mean of quantity Q in month i and $\rm M_{3Q_{ANN}}$ = the annual third moment about the mean of the quantity Q.

D. Derived Monthly Mean and Annual Mean Model Atmospheres

A set of modeled monthly mean and annual mean hydrostatic values of pressure and density was calculated from the lowest RRA data level (0 km, mean sea level) upwards to 30 km, and from 30 km upwards to 70 km. The integration from 0 to 30 km was computed independently of the integration from 30 to 70 km because of the difference in data sources. The two different values for 30 km are provided for comparison. When 30-km data are required, the values given in the 0- to 30-km table should be used. These hydrostatically modeled mean values, which are given in table IV, are useful as a check on the validity of the pressure and density values given in table II. In most cases, the values in tables II and IV for any given data level are within 1 percent of each other. The hydrostatic pressure values in table IV were calculated using the equation

$$p_{1} = p_{0} \exp \left(-\frac{0.034162 (H_{1} - H_{0})}{0.5 (T_{v_{1}} + T_{v_{0}})} \right) . \tag{67}$$

where ${\rm H_1}$ - ${\rm H_0}$ is in meters and a "O" subscript refers to v. lues at the RRA data level immediately below the level being checked. ${\rm p_0}$ at the lowest data level is set equal to the RRA mean pressure; ${\rm p_1}$, calculated for the next highest data level, is taken as ${\rm p_0}$ for the level above that. This process is repeated for all the other RRA data levels. The hydrostatic density corresponding to the hydrostatic pressures is calculated from these pressures and the RRA virtual temperature values using the formula

$$T_{\rm H} = 348.36786 \ P_{\rm H}/T_{\rm V}$$
 (68)

where $\rho_{\rm H}$ and $P_{\rm H}$ are the hydrostatic density and pressure shown in table IV of the RRA.

E. Thermodynamic Quantities Derivable from the Basic Tables

Several other quantities can be calculated from the statistics listed in tables I and II. Primary physical constants used in these calculations are listed in table E. The equations given in this section can be used to calculate the approximate mean values of these quantities at each RRA data level. It is not possible to infer or derive any information concerning the standard deviation or skewness values of these quantities from the data in tables II and III of the RRA.

E.1. Mean Air Particle Speed

The mean air particle speed, V, is the arithmetic average of the speeds of all air particles in the volume element being considered. For a valid average to occur, there must be a sufficient number of particles involved to represent mean conditions. The equation for V for dry air is

$$V = \sqrt{\frac{8}{M} \cdot \frac{R*T}{M}} \quad . \tag{69}$$

A computational form for dry air, using tabulated values, is

$$V = \sqrt{7.3094 \times 10^2 \times T} \text{ (meters per second)}, \qquad (70)$$

where T is the temperature in degrees Kelvin from table II. Equation (69), when corrected for moist air, becomes

$$V = \sqrt{\frac{8}{\pi} \cdot R' T_{V}} . \qquad (71)$$

The computational form for moist air is

$$V = \sqrt{7.3094 \cdot 10^2 \cdot T_V} \text{ (meters per second)}, \qquad (72)$$

where T_{v} is the virtual temperature in degrees Kelvin from table III.

TABLE E. LIST OF PRIMARY PHYSICAL CONSTANTS

- $P_0 = \text{standard atmospheric pressure at sea level}$ $\sim 1.013250 \sim 10^5 \text{ Newton/m}^2 = 2116.22 \text{ He/ft}^2$
- standard atmospheric density at sea level $= 1.2250 \text{ kg/m}^3 = 0.076474 \text{ lb/ft}^3$
- T_{Ω} standard temperature at sea level = 288.15 K = 15.0°C 59.0°F
- go = standard gravity at sea level at latitude 45°32'33" $= 9.80665 \text{ m/s}^2$
- = Sutherland's constant used in calculation of dynamic viscosity = 110.4 K
- T_1 ice point temperature at $P_0 = 273.15 \text{ K}$
 - constant used in calculation of dynamic viscosity
 - $\approx 1.458 \times 10^{-6} \text{ kg/s m K}^{\frac{1}{2}}$
 - = $7.3025 10^{-7}$ lb/s ft R^{$\frac{1}{2}$}
- a ratio of specific heat of air at constant pressure to specific heat of air at constant volume
- C_D = mean effective collision diameter of air molecules $\approx 3.65 \times 10^{-10} \text{ m} \approx 1.1975 \times 10^{-9} \text{ ft}$
- N_a = Avogadro's constant $= 6.022169 \times 10^{26} / \text{kg mol} = 2.73179 \times 10^{26} / \text{lb mol}$
- $R^* = gas\ constant = 8.31432\ J/mol\ K$
- $R' = gas constant for dry air = 2.8704 > 10^2 J/kg K$
- molecular weight of dry air = 28.966 g/mol

E.2. Mean Free Path

The mean free path, L, is the mean value of the distance traveled by each neutral air particle in a selected air parcel, between successive collisions with other particles in that parcel. A meaningful average requires that the selected parcel be large enough to contain a substantial number of particles. The equation for L is given by

$$L = \left(\frac{\sqrt{2}}{2\pi}\right) \left(\frac{R*T}{N_a C_d^2 P}\right) , \qquad (73)$$

where C_d is the effective collision diameter of the mean air molecules. The 1976 standard atmosphere value of 3.65 x 10^{-10} is valid for the range of altitudes in the RRA.

A computational form for moist air, using tabulated values, is

$$L = 2.335 \cdot 10^{-7} \frac{T}{P} \text{ (meters)}$$
 (74)

where T is the temperature in degrees Kelvin from table II and P is the pressure in millibars from table II.

A form of (73) to correct L for moist air is

$$L = \left(\frac{\sqrt{2}}{2\pi}\right) \frac{R'MT_v}{N_a C_d^2} \qquad (75)$$

The computational form for moist air is

$$L = 2.3325 \times 10^{-7} \frac{T_{v}}{P} \text{ (meters)}$$
, (76)

where T_{ν} is the virtual temperature in degrees Kelvin from table III and P is the pressure in millibars from table II.

E.3. Mean Collision Frequency

The mean collision frequency, $\mathbf{V}_{\mathbf{C}}$, is considered to be the average speed of air particles contained in an air parcel, divided by the mean free path of the particles inside that parcel. Computationally this is equivalent to

$$V_c = \frac{V}{L} (sec^{-1}) \qquad (77)$$

To determine V_C for dry air, use V and L from equations (70) and (74). To determine V_C for moist air, use V and L from equations (72) and (76).

E.4. Speed of Sound

The expression for the speed of sound, $C_{\rm S}$, in meters per second in dry air, is

$$C_{s} = \sqrt{\frac{R*\Gamma}{M}} . (78)$$

To compute C_{ς} for dry air from tabulated values, use

$$C_s = \sqrt{4.0185 \times 10^2 \times T}$$
 (meters per second) , (79)

where T is the temperature in degrees Kelvín from table II. One form for the speed of sound in moist air is

$$C_{S} = \sqrt{R'T_{V}} . ag{80}$$

where T_{ν} is the virtual temperature from table III. A computational form for moist air is

$$C_s = \sqrt{4.0185 - 10^2 T_V}$$
 (meters per second), (81)

E.5. Dynamic Coefficient of Viscosity

The coefficient of dynamic viscosity, μ , is defined as a coefficient of internal friction developed where gas regions move adjacent to each other at different velocities. The following expression is taken from the U.S. Standard Atmosphere (1976):

$$\frac{3 + T^{3/2}}{T + S} \qquad . \tag{82}$$

The computational form is

$$\frac{(1.458 + 10^{-6}) T^{3/2}}{T + 110.4}$$
 (kilograms per second per meter), (83)

where T is temperature degrees Kelvin from table II.

E.6. Kinematic Coefficient of Viscosity

The kinematic coefficient of viscosity, designated as γ_i , is defined to be the ratio of the dynamic coefficient of viscosity of a gas to its density, or

The computational form is

$$1.0 ext{ } ext{ }$$

where α is the dynamic coefficient of viscosity from equation (83) and α is the density in grams per cubic meter from table II.

E.7. Coefficient of Thermal Conductivity

The empirical expression used for the coefficient of thermal conductivity, designated as $\rm K_{\rm t}$, is given in the 1976 Standard Atmosphere as

$$K_t = \frac{2.65019 + 10^{-3} + T^{3/2}}{T + 245.4 + 10^{-(12/T)}}$$
 (watts per meter per degree Kelvin) , (86)

where T is in degrees Kelvin.

E.8. Refractive Modulus and Refractive Index

The refractive modulus or refractivity (Selby and McClatchey, 1975; Smith and Weintraub, 1953) is defined as N, where

$$N = (n - 1) \cdot 10^{6} \tag{87}$$

and n is the refractive index.

For microwave frequencies below approximately 30 GHz (equivalent to wavelengths above 1 cm), N, the refractive modulus, is given by the empirical equation

$$N = 77.6 \frac{P}{T_d} + 3.73 \times 10^5 \frac{e}{T^2}$$
 (dimensionless), (88)

where E and P are in millibars and ι and T_d are in degrees Kelvin.

The following expression is valid for the visible and infrared wavelengths shorter than approximately 30 μm (0.03 mm).

$$N = 77.6 \frac{P}{T} + 0.584 \frac{P}{T} \quad (dimensionless) , \qquad (89)$$

where λ is the wavelength in microns and T is in degrees Kelvin.

The expression for N for the wavelength from $0.03\ \mathrm{mm}$ to 1 cm is an extremely complex function of wavelength.

CHAPTER IV. CONCLUSIONS AND RECOMMENDATIONS

Conclusions

This document satisfies the technical objectives established for the RRAC by the RCC MG. Upper air statistics and models for wind and thermodynamic quantities for the specific site have been derived in a consistent and uniform manner, which will be used in publications for all other assigned site locations. These RRAs represent an improvement over the previously published RRAs because of the availability of more extensive upper air data bases and the adaptation of more advanced statistical techniques. A statistical measure of central tendency (mean values) and a measure of dispersion (standard deviation with respect to the mean values) for monthly and annual reference periods have been tabulated for all variables in a consistent manner from data bases that have been edited and quality-controlled in the same manner. Further, a statistical measure for symmetry (skewness coefficient that involves the third statistical moment) has been tabulated for all variables except the U and V wind components. Even with these improvements, the user of these RRAs must recognize certain limitations of the statistical tabulations:

- 1) The wind profile structure with respect to altitude cannot be modeled from the RRA statistics because the interlevel and crosslevel correlations were not computed.
- 2) The profile structure with respect to altitude for any of the thermodynamic variables or any quantities derivable from these variables cannot be modeled because the prerequisite correlations were not computed. However, the profiles of monthly and annual means for pressure, virtual temperature, and density are in agreement (table IV) with the hydrostatic equation and the equation of state.

The preceding limitations are cited to prevent a misuse of the RRAs. More extensive statistical tabulations were beyond the scope of this committee's task. As greater insight is gained through usage of these RRAs, many adaptations of the statistical tabulations for specific engineering and scientific applications are envisioned.

Recommendations

It is recommended than the wind and thermodynamic statistical tabulations and attendant models contained in the RRAs be used as a standard reference source, as may be appropriate, by the ranges and range users. It is further recommended that the respective Range Staff Meteorologist or responsible agency staff member be consulted for the applicability of the RRAs for specific engineering applications.

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In addition to the documents above and the present RRA for Vandenberg AFB, California, the revised series will include RRAs for the following locations:

Edwards AFB, California White Sands Missile Range, New Mexico Point Mugu, California Dugway (Michael AAF), Utah Eglin AFB, Florida Ascension Island, South Atlantic Wallops Island, Virginia Taquac (Guam) Barking Sands, Hawaii

CONVERSION UNITS

Physical Constants and Conversion Factors

Numerical values in this document are given in the International System of Units (SI, Système International d'Unités). The values in parentheses are equivalent U.S. Customary Units, which are English units adapted for use by the United States of America. The SI and U.S. Customary Units provided in table F are those normally used for measuring and reporting atmospheric data.

By definition, the following fundamental conversion factors are exact:

Туре	U.S. Customary Units	<u>Metric</u>
Length Mass Time Temperature	<pre>1 U.S. yard (yd) 1 avoirdupois pound (1b) 1 second (s) 1 degree Rankine (°R)</pre>	0.9144 meter (m) 453.59237 gram (g) 1 second (s) 9/5 degree Kelvin (K)

To aid in the conversion of units, conversion factors based on the above fundamental conversion factors are given in table F.

TABLE F. FACTORS FOR CONVERSION UNITS

	MI 1RIC		USCUSIONARY	I \ K \		CONTINUO	
type Date	l me	Vbbreviation	Unit	Vibration	Multiply	By	loter
TAMPRAILE							
Vorbigat Terra granting	degree Colson	J	degree Lahrenher	-	1 - 32	9555'0	
	degree Kelkin	4	degree Rankine	×	Ų	.8.	5
					×	. 100 1	_965t+1,
					K 45967	•190	_
					; ;	• tut -	(+273.15
					N 273 16	•	J
Longoratury Change	degree Celsius	_	datter Laurenheit	_	**	J.x.	temp, change
	derrec Kelvin		degree Kankine	×	x	333	temp change CorK
015413							
Water Caper	to the true to the		error ner alm form	~: :	· ·	100,74	£, ii
Absolute Humidity	group per cubic centimeter	7.2		;	11.	2.2883	~ E :
and America Density					, m		i min
					, mod	4,370×105	, . E
					.118	2,288 × 10 ⁶	, no
W1/1)							
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			feet per second		tu	51.00	× 10 ×
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		-			7 - ,		1 :
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1981 880							
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	An accordingly	_				ニンナー	1
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					;	: \$ E	1

TABLE F. (continued)

	MI IRIC		LSCUSIONARY	MARY		CONVERSION	
Lype of Data	Lmr	Abbres tation	t nıı	Abbrey 14' to n	Madaphy	Rs	Lotet
DISTANCE (Concluded)					3	.901	a.
					1	3977-7105	Ē
						6 101	ē
					-	11 1 15 1	≘
WASS							
Weight	gram	ta.	unn	Į:	£	0.45359337*	и •
	kilogram	ž	punad	Ib.	£	455,59237*	3.
					k ç	2,20462	£
					u	15 4324	13.
					μī	0.06480	u
PRISSURI							
Amospheric	newton per square meter	newton m	pound force per	lb in. 2	qw	10.3*	hat
			square meh		bar	. 151	ı III
	millimeter of Mercury	appropri	inch of Mercury	m.Hg	newton m-		, qu
					newton m.2	1,4504 × 10.4	
					lb m	6.8948 v 10°	n, with a
	bar	hur			, qui	201 V \$057 L	P. m. 1
	sullibar	nu.			Thina.≟	68 948	÷
	dyne per appare	dyne in 2			ap.	; <u>:</u>	dim int
	centimeter innerobati	,			dyne cm 2	; :	410
	kilogram force per	Ne m -			. E E	6 8948 × 10	dynes, m. *
	Apart meter				dyne, m	_ 14504.1	, s £
					, dui	2541.01	
					kem.	0.0980665	÷
					. m 4	25.30 5.00	
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					dut	2.9530 v 10 2	in Hg + 2, 1 i
					y.u.	90002.0	1) Hustu
					in Hg + 32 T +	.04 <	could, 100
					willight Ci	2200	+
		:			10. He (32.1.)	カンニ	· .
	Parsonal	Pa			P.,	1 00.0	n wton m

* Defined on a law croon factor

TABLE 1-1. WIND STATISTICAL PARAMETERS

JANUARY

STATION	- 723930	VANDEN	BEPS AFE						
Z	MEAN U	5.D. U	R(U,V)	MEAN V	5.0. V	MEAN HS	S.D. WS	SKEH HS	NOBS
kМ	M/S	M/S		M/S	M/5	M/S	H/S		
. 100	. 37	2.78	-,4934	72	3.33	3.59	2.57	1.22	207.
1.000	.83	4.20	0637	-1.44	6.97	5.91	14.61	1.11	857.
2.000	3.15	5.50	.0705	-2.38	7.54	8.81	5.15	.79	863.
3.000	5 .79	7.29	. 1400	-3.10	8.90	11.55	6.47	.80	873.
4.000	8.11	8.99	.1056	-3.47	9.86	14.65	7.64	.70	875.
5.000	10.29	10.53	.2130	-3.40	10.78	16.35	8.79	.56	876.
6.000	12.10	12.02	.2394	-3.39	12.02	18.52	10.01	.57	877.
7.000	13.98	13.37	.2606	-3.64	13.12	29.97	10.94	.59	875.
9.000	15.67	14.91	.2652	-3.99	14.19	23.29	11.93	.57	868.
9.000	17.52	16.19	.2720	-4.43	15.35	25.66	18.81	.55	859.
10.000	19.65	17.21	.2479	-4.30	16.08	27.96	1.5.54	.52	657.
11.000	21.60	17.30	.2465	-5.12	15.78	29.23	13.66	.47	844.
12.000	23.19	16.30	.2339	-5.07	14.96	23.54	13.43	.59	832.
13.000	23.72	13.74	.2655	-4 38	12.70	27.71	11.54	.5+	828
1+.000	21.45	11.65	. 3335	-3.81	10.94	25.25	9.85	.31	916.
15. COJ	13.93	9.99	£635.	-3.52	9.41	22.09	8.52	.60	80€.
16.000	15.25	8.36	. 3465	-3.07	7,91	19.84	7.14	,42	800.
17.000	3.28	7.22	. 3329	-3.00	6.43	15.58	5.99	.63	781.
18.000	9 87	6.41	.2918	-3.04	5.18	12.15	5.20	1.00	760.
19.000	6.93	5.61	.2925	-2.99	4.25	9,44	4.48	1.13	763.
20.000	4.35	5.87	.2607	-3.08	3.73	7.69	4.18	1.19	747.
21.000	2.34	6 48	.2370	-3.15	3.55	7.21	4.24	1.46	723.
21.010	. 73	7.10	.2641	-3.14	3.46	7.51	4.05	1.36	713.
23.000	. 17	7.70	.3055	-3.10	3.54	8 01	4.15	1.52	705.
2+.000	23	8.97	.3508	-2.86	3.94	8.92	5.02	1.53	705.
25.000	-1.76	10.35	.3743	-2.59	4.13	9.94	5.75	1.62	695.
20.000	8+	11.79	.4353	-2.57	4.50	11.10	6.56	1.36	C80.
27.000	33	13.29	.5145	-2.53	5.08	16.31	7,54	1.34	535.
č11.000	,43	14.47	.5727	-2.70	5.94	13.62	8. (5	1.30	586.
27.000	1.46	15.16	.60+8	-2.69	6.74	15.33	8.97	1.24	516.
32.000	3.15	17.98	.5363	-2.48	7 58	17.16	10.09	1.21	452
32.000	7.29	19.73	.5:44	:6	7.47	18.50	10.62	.81	167.
34.000	10.77	21.15	.5814	31	8.75	21.73	12.89	.62	167.
050.00	13.29	23.09	.6009	81	3.21	23.66	15.26	.66	167.
39.000	15.92	24.73	.5109	-1.58	9.92	25.49	17.67	.61	16a.
40.000	18.55	24.63	.4082	-1.57	زح.11	27.27	18.29	.62	168.
42.000	22.20	25.32	.3070	. 35	13.28	30.42	19.56	.55	158
44.000	28.77	25.53	.3903	2.75	15.31	35.32	21.25	. 35	168.
45.000	36.23	30.13	.4236	6.74	10.45	44.96	24.10	.43	167.
48.000	42.91	31.79	.4329	8.72	19.03	51.47	25.23	. 26	167.
50.000	46.30	31.52	.4139	10.50	18.99	54.03	26.16	.21	166.
52,000	48.14	30.08	.4032	10.53	17.53	54.83	24.99	03	166.
54.CC0	50.10	29.81	.6019	10.30	17.69	55.69	24.50	08	168.
59.000	5:.83	29.84	.3181	9.20	16.87	57.85	24.50	33	158.
53.000	55.21	23.70	.23!8	10.01	17.55	€0.19	26.67	29	136.
6 3.060	59.92	32.44	.4857	8.38	20.56	64.78	30.57	20	93.
62.000	53.74	30.52	.4814	11.83	18.57	73.58	€9.33	36	64.
59,000	77.55	32.97	.3750	9.41	18.33	eo.9 5	31.06	30	57.
65.000	84.97	31.44	.3150	3.56	15.83	97.21	2 9.8 5	32	56.
68.000	월4.36	28.90	. 3563	-2.91	15.75	95. 29	27.51	30	55.
73.000	78.61	30.23	.8033	-5.42	17.28	81.21	2a.63	28	53.

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TABLE 1-2. WIND STATISTICAL PARAMETERS

FEBRUARY

STATION	723930	VANDEN	BERS AFB						
Z	HEAN U	5.D. U	R(U,V)	MEAN V	5.D. V	MEAN US	S.D. KS	SKEH HS	NOBS
KP1	M/S	M'S		4/5	M/S	M/S	H/S		
100	.82	2.98	5922	93	3.47	3.88	2.72	1.06	733.
1.000	.51	4.23	1799	-1.42	7.36	7.33	4.45	. 80	777.
2 000	2.66	5.30	1010	-1.91	8.39	9.07	5.18	.61	788.
3.000	5.43	6.75	0052	ہیں جے۔	9.47	11.34	6.48	.64	787.
4.000	8.02	0.33	0224	-2.62	10.59	13.88	7.74	.67	783.
5.000	10.35	9.60	.0267	-2.57	11.44	16.07	8.85	.67	78 9 .
6.000	12.34	10.85	.0743	-2.66	12.62	18.40	9.68	.73	784.
7.000	14.30	12.31	. 1200	-3.06	19.11	21.04	11.02	. 87	783.
8.000	16.31	13.66	.1112	-3.52	15.07	23.53	11.74	.65	778.
9.000	18.70	15.30	.1552	-3.8+	16.03	15.85	12.97	. 69	770.
10.000	21.01	16.69	.1926	-4.09	16.74	28.59	14.12	. 🖰 1	758.
11.000	2 2 . 87	10.36	.1945	-4.00	16.46	29.70	13.95	.69	755.
12.000	24.51	14.91	.2004	-3.52	15.29	29.83	13.36	.57	744.
13.000	2+.25	12.91	. 1845	-2.56	13.14	28.24	11.58	. 5 5	738.
14.000	23.04	11.55	.1570	-1.81	11.34	26.16	10.55	. 52	730.
15.000	20.43	9.74	.1552	-1.70	9.86	23.09	8.88	. 37	72 6 .
15.000	17.62	8.35	.1771	-1.64	8. <i>2</i> 9	19. 85	7.55	.49	723.
17.000	14.46	5.9 4	. 1783	-1.45	6.83	16 . 35	6.20	. 56	706.
18.000	11.22	6.34	. 1341	-1.56	5.63	12.95	5.70	. 93	712.
:9.000	0.11	5.64	. 1972	-1.73	4.50	9.86	4.84	. 87	703.
20.000	5.5≥	5.69	.2604	-1.70	3.95	7.81	4.50	1.47	700.
21.000	3.25	6.01	.1866	-1.77	3.45	6.64	4.20	1.64	5 ^ל 5.
22.000	1.79	6.34	. 1373	-2.09	3.13	6.49	3.93	1.52	6 61.
23.000	. 93	5.75	. 1 387	-2.08	2.77	6.62	3.60	1.39	650.
24.000	, 444	7.44	.1011	-2.03	3.11	7.12	4.31	1.21	644.
25 . CUB	.43	8.22	.0786	-1.95	3.28	7.74	4.73	1.08	631.
₽€ 000	1.00	9.35	.1313	-1.82	3.58	8.73	5.30	1.05	615.
27.000	2.85	10.23	.1714	-1.71	3.69	9.70	5.93	. 99	540.
28.000	4.93	11.46	.2261	-1.57	3.83	11.30	5.69	. 98	511.
29.000	7.10	13.17	. 3045	-1.35	4.24	13.58	7.67	. 9 9	425.
30.000	9.23	15.09	.2938	-1.20	4.53	15.88	9.09	. 95	464.
32.000	11.00	18.42	.4303	72	5.12	19.61	10.04	.22	166.
34.000	15.60	21.73	.5111	04	5.45	24.75	11.90	03	166.
76.000	20.11	25.01	.5548	29	7.08	29.29	14.62	05	165.
38.000	24.15	28.12	.5250	09	6.59	33.59	17.79	.06	169.
40.000	26.99	29.18	.4533	57	10.75	36.44	19.08	. 12	163.
42.000	29.66	29.52	.4467	. 22	12.44	38.82	19.89	.06	169.
44 CCO	35 50	29.91	.4457	2 50	15 02	42.01	19.85	.08	169.
46.000	34.85	30.27	. 3839	4.79	15.87	44.60	20.31	.00	169.
48.000	36.90	29.29	.3748	6.94	14.95	45.96	19.33	09	168.
50.000	38.93	27.64	.3590	7.92	16.34	47.59	18.40	11	168.
52.000	41.35	26.30	.3945	7.99	15.73	48.92	17.76	04	166.
54.000	45.66	24.75	.4000	8.16	15 65	51.73	18.16	11	158.
56.000	49.56	25.83	.3845	8.39	15.61	55.26	19.53	.11	149.
58.000	54.27 60.73	25.04	.4049	9.10	15.42	58.98	20.28	53	120.
60.000 6 2.000	60.72 67.99	23.64	.4025 .2683	7.64 9.52	10.69	65.62 71.77	18.77 19.93	38	91. 56.
6≥.000 6÷.000	57.99 72.70	22.94			17.76			. 14	96. 47.
		26.04	.0698	8.36	15.26	75.64	23.17	. 44	
66.000	73.61	27.15	.1421	5.79	13.32	76,20	23.48	.31	44 .
68.000	72.47	28.33	.0140	2.99	12.70	75.54	22.54	03	41.
70.000	68.19	22.05	1098	-2.01	17.07	70.72	20.21	16	39.

TABLE 1-3. WIND STATISTICAL PARAMETERS

MARCH

STATION -	723930	VANDENE	ERG AFB						
Z	MEAN U	5.D. U	R/U.VI	HEAN V	5.D. V	MEAN WS	S.D. WS	skeh HS	NO 9 5
KM	M/5	M/S		M/5	M/S	M/S	M/S		
. 100	1.82	2.69	5954	-1.92	3.51	4.18	3.01	. 82	835.
1.000	1.24	4.04	1138	~3.07	5.46	7.27	4.00	.67	96 4 ·
2.000	3.05	5.12	0780	-3.09	7.73	9.02	4.83	.53	885
3.000	5.76	6.75	0456	-3.33	9.04	11.48	6.30	.65	886.
4.000	8.34	8.65	0078	-3.38	10.47	14.21	7.98	. 76 . 83	989.
5.000	10.59	10.39	.0339	-3.19	11.62	16.64	9.39	.73	889. 895.
6.000	12.72	11.83	.0778	-3.22	12.91	19.16	10.56		
7.006	14.75	13.24	.1217	-3.48	14.36	21,72	11.80	.66	884.
8.000	16.59	14.43	. 1517	-3.82	16.07	24.20	13.04	.63	880.
9.000	19.50	15.32	. 2 21 0	-3.94	17.34	26.46	13.83	.53	9 76 ·
10.000	20 77	15.60	. 2520	-3.77	17.96	28.45	14.06	. 38	871.
11.000	£2.83	15.07	.2456	-3.46	17.26	29.57	13.64	. 29 . 38	860. 853.
12.000	24 50	13.73	.2485	-2.52	15.43	29.57	12.59	. 23	852.
13.000	24.48	11.50	.2414	-1.62	13.33	28.21	10.78 9.63	.52	8+5
14.000	23.32	10.05	.2387	-1.15	11 - 34	26.11			841.
15.000	20.64	8.05	. 1981	74	9.34	22.83	7.57	.09 75.	840.
16.000	17.85	7.23	.1592	61	7.94	19.69	5.96	.37	820.
17.000	15.00	6.49	. 1423	77	6.44	16.53	5.99	.59	82 3 .
18.000	11.83	5.88	. 1296	65	5.19	13.13	5.43		
19.000	8.83	5.33	.18+4	- 85	4.19	10.12	4.67	.58	817.
20.000	6.29	5.18	.1404	93	3.58	7.98	4.04	.62	813.
21.000	4.25	5.52	.0755	-1.03	3.24	6.81	3.70	.93	789.
22.000	2.78	5.84	.0787	-1.13	3.03	6,40	3.36	1.06	772.
23.000	2.09	6.24	. 1859	98	2.71	6.31	3.43	1.23	759.
24.000	1.63	6.94	. 3053	74	5 63	6.62	3.94	1.26	750
25.000	1.97	7.78	.3179	69	5· 8 +	7.28	4.46	1.19	749.
26.000	2.50	8.57	. 3706	67	2.85	8.05	4.83	1.02	730.
27.000	3.57	9.82	.4012	67	3.14	9.40	5.58	.80	665.
29.000	5.65	11.40	.4332	<i>T7</i>	3.59	11.47	6.61	.69	505·
29.000	7.44	13.17	.4211	72	3.77	13.66	7.53	. 59	528.
30.000	9.48	14.84	. ۲۰۰۱9	46	4.17	15.88	8.68	.40	502.
32.000	13.10	15.20	.3004	1.09	5.10	17.92	10.39	.48	140.
34.000	18.23	17.00	.2374	2.16	5.87	22.49	12.40	. 35	140
36.000	23.32	18.90	.4021	2.06	7.13	27.70	14.68	. 23	140.
38.000	28.42	21.42	.4207	2.35	7.99	32 . 30	17.06	. 23	141.
46.600	32.03	22.47	.2574	3.43	9.02	35. 86	:0.29	. 06	141.
42.000	34.47	20.89	.2407	4.32	10.94	37.85	18.12	02	141
44.000	35.85	19.85	.2889	5.68	11.62	39.24	17.60	03	141.
46.COO	36.63	18.72	. 3385	8.00	11.69	39.62	17.95	. 11	191
48.000	38.02	17.73	.2779	8.89	11.39	40.82	17.34	. 06	141.
50.000	38.10	17.43	. 3243	9.49	12.52	41.64	16.36	. 09	140.
52.000	38.10	17.53	.3462	11.01	13.15	41.97	17.03	.04	139
54.000	39.11	16.97	.3933	11.83	13.03	42.82	17.10	. 14	135
56.000	41.88	17.91	.3389	13.20	13.24	45.11	17.46	. 12	128
58.000	42.73	20.14	. 3701	10.88	13.48	46.56	19.01	.00	114.
60.000	44.56	21.80	. 3506	8.47	14.20	47.71	21.35	.01	79.
62.000	43.42	22.89	.1844	6.22	15.73	46.95	22.07	. 03	59.
€4.030	40.14	24.71	.2398	3.02	16.33	44.06	23.43	01	47.
66.000	35.52	24.30	.0904	.61	18.38	41.50	21.38	. 09	44,
66.000	27.52	24.03	0429	-1.05	16.11	359	18.58	. 33	42.
70.000	20.53	24.04	0753	50	16. 64	31.27	16.88	. 33	41.

TABLE 1-4. WIND STATISTICAL PARAMETERS

APRIL

STATION	723930	VANDENE	ERG AFB						
Z	MEAN U	5.D. U	RIU.VI	HEAN Y	5.0. V	MEAN HS	5.0. HS	SKEH HS	NOB5
iO1	M/S	M/S		M/S	H/S	H/S	M/S		
. 100	2.11	2.80	6346	-2.31	3.23	4.32	3.09	. 85	766.
1.000	1.52	3.83	086 9	-3.93	5.55	7.02	3.73	. 65	B13.
2.000	2.63	4.58	0967	-3.53	6.82	8.20	6.43	.62	8 25.
3.000	5.50	5.99	0161	-3.69	8.53	10.70	€.15	1.02	826.
·.C00	8.47	7.70	.0444	-3.92	10.50	13.87	6.05	. 90	82 6 .
5.000	11.19	9.47	. 1490	-3.53	11.85	16.73	9 36	. 79	82 5 .
6.000	13.71	11.18	.1883	-3.42	13.34	19.62	10.84	. 75	822.
7.000	15.99	12.49	.2314	-3.39	15.03	22 42	12.09	.74	819.
8.000	18.07	13.95	1085.	-3.49	16.44	25.03	13.29	.8:	815.
9.000	19.79	14.66	. 3644	-3.39	17.01	27.01	13.32	.57	809.
10.000	21.52	15.00	. 3801	-3.46	17.12	28. 58	13.26	.45	805.
11.000	2 8.93	14.40	.3779	-2.79	16.19	29.01	12.55	. 37	793.
12.000	23.81	13.35	. 3728	-1.60	14.98	29.86	11.82	.51	788.
13.000	23.40	11.19	.3480	34	12.61	26.93	10.29	. 60	787.
14.000	51.90	9.34	. 3395	. 85	10.72	24.59	8.61	.41	782.
15.000	19.52	7.92	. 3444	1.22	9.29	21.74	7.65	. 39	777.
16.000	16.61	6.76	.3096	1.29	7.90	18.49	€.50	. 38	774.
17.000	13.61	5.71	.2609	1.30	6.39	15.1 9	5.45	. 37	758
10.000	10.42	5.10	.1779	1.27	5.16	11.79	4.89	.46	756
19.300	7.44	4.75	.0992	1.13	4.10	8.84	4.23	. 69	753.
20.000	5.08	4.45	.0711	.70	3.39	6.66	3,64	. 99	747.
51.000	3.29	4.57	.0738	.40	2.96	5.40	3.29	1.44	723.
E2.300	2.21	4.83	. 1488	. 20	2.66	5.06	3.10	1.46	714.
23.000	1.80	5.09	. 1593	. 16	2.41	4.98	3.18	1.68	704.
₽4.000	1.69	5.55	.1726	. 10	2.57	5.24	3.58	1.58	710.
25.000	2.54	5.93	.2005	10	2.66	5.84	3.82	1.51	708.
<i>2</i> 6∵000	3.50	6.48	.2734	19	2.71	6 54	4,34	1.60	633.
27.000	4.97	7.02	. 3131	09	3.03	7.66	4,94	1.20	627.
26.000	6.96	7.27	.3315	. 05	3.35	9.02	5.57	. 97	580
29.000	8.34	7.89	. 3132	. 11	3.81	10.80	6.17	.92	534.
30.000	10.74	8.07	.2940	.09	4.01	12.34	6.65	.93	5¢3.
<i>\$2</i> . 000	11.05	8.23	. 2853	.99	4.83	13.17	7.41	.57	145.
34.000	15.69	9.24	.3127	1.20	5.40	16.56	€.67	.41	145.
¥1.000	18.03	10.69	. 4647	1.74	5.79	19.29	10.27	. 53	147.
38.000	19.21	15.65	. 3762	. 34	7.16	21.07	11.62	. 35	197.
40.C33	18.30	15.64	. 3 20 0	64	6.71	21.12	13.36	.48	;47. 147.
42 000	14 50	16.73	.0435	1.05	7.95	19.61	17.05	.69	
44.200	13.20	:5. 35	.1457	4.00	8.20	18.96	12.97	. 79	147. 147.
~6.¢00	13.40	17.01	-5510	5.06	8.26	19.43	13.66	.74	147.
48.COO	12.83	18.45	1755.	5.98	7.14	20.04	13.70	.80	-
50.000	1 82	18.43	.1001	5.53	7.78	50.18	17.65	ج. 7 .	146.
52.000	10.65	19.36	.1250	5 19	7.62	19 36	12.62	.78	146 143
54 330	7.41	:9.33	. 26.34	4.75	8.85	18.64	11.94	.76	135
56 000	5.55	18.29	.2315	6.75	8.38	18.31	11.02	.96 .83	126.
58.000	4 13	17.18	.1297	6.60	9.25	19.41	10.03 5.94	. 83 , 64	B7.
60.000	5 . 23	18.41	.2710	4.32 5.70	10.37	19 18 16.63	£.33	. 36	51.
62.000	. 19	15.93	.0003 1153	4.30 3.90	9.03 10.15	16.16	E.33 E.51	.30	45.
64.000	-1 08	14.82	1123	1.48	11.98	16.10	8.77	.39	43.
66.000	-2.24	14.60	3729 0621	87	12.05	16.74	7.21	.39	42.
60.000 70.000	-2.73	10.33	.1416	-4.23	8.40	14.76	7.76	.33	41.
70.000	-5.14	12.94	. 17.0	-4.63	6.40	17.70	, . 76		•••

TABLE I-5. WIND STATISTICAL PARAMETERS

MAY

STATION	- 723930	VALQEN	BERS AFB						
7	MEAN U	5.D. U	RIU.VI	MEAN V	5.D. V	MEAN WS	S.D. WS	SKEH HS	NOBS
KM	M/5	M/S		M/S	M/S	H15	H/S		
. ເວດ	2.23	2,42	5244	-2.18	2.66	3.86	2.79	.90	BC5.
1.000	1.00	3.32	- 1672	-3.83	4.37	5.94	3.24	.72	B43.
2.000	. 97	3 96	~.35;0	-3.09	5.37	6.39	3. ~7	. 99	89 0.
3.000	2.71	5.65	~.3692	-2.70	6.+3	7.93	5.00	1.05	882.
4,000	4.61	7.19	~.2545	-2.63	7.33	9.72	6.31	1.14	983,
5.000	5.18	8.42	1401	-2.49	0.19	11.19	7.58	1.47	883.
6.000	7.62	9.62	0740	-5.63	9.18	12.86	9.75	1.37	881.
7.000	8.84	10.62	.0083	-2.93	10.34	14.52	9.76	1.20	879.
8.000	9.91	11.91	1080.	-3.13	11.72	16.23	10.58	1.04	9 75.
9.000	11.24	12.35	.1219	-3.34	12.96	18.09	11.42	.96	874.
10.000	12.52	13.25	.1735	-3.36	13.93	19.83	12.01	.99	872.
11.000	13.65	13.53	. 2521 . 2521	-3 86 -2.55	14.15	10.05	11.95	. 72 . 76	969. 2 66.
12 000 13.000	14.79 14.98	13.04 10.83	.2587	-1.29	13.29	21.09 19.59	11.25 9.17	. 54	864 .
15.000	14.66	8.75	.1766	~.17	8.96	17.68	7.68	.47 .54	863.
15.000	13.10	7.02	.1597	.64	7.35	15.28	6.45	.60	8 60.
16.000	11.05	5.67	.1308	1.03	6.02	12.76	5.60	.64	854.
17.000	8.53	4.B3	1051.	1.11	4.71	10.01	4.50	.53	833.
18.000	5.79	4.05	1001.	.84	3.73	7.22	3.53	.65	829.
19.000	3.04	3.62	.0525	.50	2.93	4.83	2.80	1.24	823.
20.000	.79	1,29	.0726	.07	2.40	3.61	2.05	1,00	811.
21.000	-1.01	3,16	.0797	28	2.19	3.47	1.97	.82	788.
22.000	-2.00	3.37	.0131	45	2.08	3.89	2.18	. 73	783.
23.000	-2.40	3.42	.0248	55	2.04	4.11	2.54	.57	767.
24.000	-2.39	3.61	.0555	60	2.24	4.33	2.30	.71	762.
25 000	-2.15	3.94	.0452	60	2.18	4,44	2.35	.63	755.
26,000	-1.64	4,41	.0102	48	E.27	4.62	2.48	.71	745.
27,000	-1 55	4.B2	0073	37	2.54	୴୍ଦମ	2.69	.69	57 6 .
28 GOQ	44	5,54	0212	41	2.64	5.11	2.76	.46	543.
23.000	. 14	6,14	.0037	39	2.73	6.47	2.89	.61	501.
30.000	. 66	6.30	.0126	- , 44	2.71	6.17	3.10	.48	477,
35 .000	+,14	5.73	.0141	1.57	3.35	6.00	3.22	.75	(64.
34 . 600	. 29	6.16	.1085	1.64	3.56	6.43	3.50	.gg	164.
W. 000	95	סל,ל	.0881	1.63	3.61	7.53	4.18	.70	164.
38 000	-2.03	8.62	0405	. 12	4.10	8.72	4.75	1.07	165.
40.000	-6.27	9.53	325.9	11	4,44	10.04	5.53	.79	165.
42.000 44.000	~10.10 ~13.79	8.29 7.50	~.1420 ~.0830	.03 1.34	4.26 4.87	11.99 14.97	6.70 6.9₩	.50 .13	165. 164.
45.000	-16.22	8.27	.1839	3.97	5.11	17.92	7.20	.08	164.
48.000	-18.02	8.62	.1939	6.08	5.43	20.20	7.57	.12	164.
50.000	-18.81	9.57	.0773	6.33	4.90	21.16	8.33	. (9	163.
52 600	-19 66	9.39	1-65	5.37	6.63	21.63	8.83	.20	162.
54 000	-23.55	9.15	1683	3.83	6.06	24.68	8.97	.42	156.
54 000	-26.85	9.98	1833	3.42	6.86	27.99	9.79	.03	144.
56 000	-30.67	9.58	.2199	3.27	9.72	32.41	9.29	.31	123.
60.000	-31.60	11.24	.3544	5.80	10.33	34.29	10.03	~.17	86.
52.000	-32,46	13.63	.2634	6.03	9.94	35.00	12.15	24	62.
64.000	-33.15	13.73	1118	4,54	11.88	35.57	13.44	40	49.
66.000	-32.16	13.66	.0086	5.87	9.06	34.18	12.92	.46	49.
58.000	-27.5เ	17.44	1600	4.08	11.65	31.20	15.32	. 99	49.
20.000	-25.41	14.03	2516	3.34	12.15	28.79	12.99	.61	48.

TABLE I-6. WIND STATISTICAL PARAMETERS

JUNE

STATION	- 723330	VANDEN	OEPG AFB						
Z	MEAN U	5.D. U	R(U,V)	HEAN V	5.D. V	MEAN WS	5.D. HS	SKEW HS	NOB5
K24	M/S	M/5		M/S	M/5	M/S	M/5		
.103	2.25	2. <i>2</i> 9	6058	-1.92	2.47	3.64	.2 50	.96	־38
1.000	. 89	3.17	1978	-3.61	يوال يوا	5.59	3.14	1.01	752.
2.000	1.02	3.91	2983	-2.45	4.73	5.8∂	3.30	.85	782.
3.000	2.78	5.32	S003	-1.19	5.59	7.12	4.24	.91	784
4.000	4.37	6.45	0818	38	6.58	0.75	5 24	.91	785.
5.000	5.75	7.43	0178	. 09	7 49	10.30	6. ! 8	.94	784
6.000	7.13	8.42	0161	, 44	8.70	11.95	". 39	1.24	783.
7.000	8.66	9.56	.0190	.76	9.98	13.81	0.68	1.19	783.
8.000	9.94	10.71	.0751	.94	11.44	15.78	9.8	1.00	784.
3.000	11.18	11.60	.1436	1.31	12.71	د6 17	10.57	.70	780.
10.000	12.83	12.65	.1842	1.74	13.84	19.72	11.48	.62	783.
11.000	14.76	13.25	.2316	2.24	14 56	21.67	11.84	.47	777.
12.000	16.30	13.11	.2765	3.11	14.23	22 65	11 68	40	774.
13.000	16.81	11.99	.2926	9.01	12.98	55.58	10.71	. 23	773.
14.600	15.45	9.80	.2315	4.37	11.01	19.82	9.07	.29	769.
15.600	12.45	7.40	.1561	4.15	8.55	15.92	5.85	.25	767.
15.000	8.84	5,44	0330	3.13	6.76	11 48	5.00	.26	761.
17.000	5.18	4.17	0257	2.09	4.61	7.55	3.57	.43	737.
19.000	1.45	3.63	0670	1.27	3.51	4.81	2.46	.85	741.
19.000	-1.71	3.25	0362	. 70	2.63	4.10	5.05	.71	738.
20 000	-3 83	3.12	- 0420	.45	2.08	4.80	2.43	.75	730.
21.000	5.35	2.08	0391	رة.	1.91	5.03	2.69	.77	710.
23.000	-6.51	2.82	.0449	16	1.78	6.90	2.68	.80	710.
23.000	-7.59	2.97	.0471	38	1.72	7.84	2.83	.79	702.
₹+.C00	-8.55	3.43	.0152	41	1.81	8 56	3.19	44	633.
25.000	-8 93	3 59	.0051	41	1.90	9.16	3.42	. 37	703.
25.000	-9.37	3.79	0220	- 34	1.87	9.63	3.60	. 34	595.
27.000	-9 .57	4.09	.0084	20	2.13	10.01	3.82	. 18	628
29.000	-10.02	3 91	.0143	.00	1.92	10.29	3.67	. 15	574.
29.000	-10.48	3.85	.0043	. 05	2.18	10.76	3.70	.14	525.
30.000	-10.83	4.04	.0244	06	2.06	11.10	3.84	.06	556.
32.000	-14.56	4.86	0749	1.39	2.80	14.91	4,79	.05	144.
34.000	-16.01	5.35	0320	1.42	2.75	16 32	5.28	28	144.
36.000	-18.38	5.45	0571	.58	3.02	18.65	5.38	15	145.
39.000	~22.18	5.36	.1446	.49	3.36	22.46	5.25	.03	145.
40.000	-25.91	6.39	.1834	.58	3.65	26.20	6.28	19	145.
42.000	-29.67	6.99	1242	.41	4,30	29.99	6.98	.20	145.
44.000	-33.15	6.13	1053	2.50	5.26	33.66	6.09	02	145.
45.000	-35.77	6.75	1+24	9,70	5.17	36.48	6.51	34	145.
48.000	-3/ .50	7.36	0929	4.73	5.29	39.17	7.26	25	144.
50.000	-41.36	8.25	.0216	5.45	5.15	42.22	8.00	.05	142.
52.000	-44.07	8.93	.0796	6.12	6.09	44.95	8.69	08	132.
5~.000	-46.75	9.41	0417	5.39	6.76	47.48	9.39	. 10	124.
56,000	-50.39	9.92	1145	5.39	6.51	51.09	9.87	.23	117.
59 000	-53.04	11.10	-1542	3.13	7 82	53.71	102	.30	90.
£0.000	-53.52	12.24	.0233	5.78	10.22	54.47	12.55	. 37	62.
62.000	-57.70	14.32	.1682	5.66	14 06	59.50	14.44	05	41.
64.000	-55.49	17.39	.7488	8.51	10.03	57,24	16.49	. 33	33.
65.000	-52.61	19.91	3780	7.18	11.32	54 22	14.32	32	32.
68.000	-49.79	18.84	0700	5.97	12.72	51.25	18.65	09	31.
70.000	-44.92	21.59	.1080	9.20	13.49	48.41	19.95	.07	29.
70.030			. 1000	3.04	13.43	-0.71			

TABLE 1-7. WIND STATISTICAL PARAMETERS

JULY

STATION =	723930	VANDENE	SERG AFB						
Z	MEAN U	5.D. U	RIU.VI	MEAN V	5.D. V	MEAN WS	S.D. WS	SVIDH HS	NOSS
101	M/S	M/5		M/S	M/S	M/S	H/5		
. 100	2.05	2.13	5745	-1.78	5.10	3.23	2.43	. 37	725.
1.000	.25	2.63	2496	-2.06	3.92	4.48	2.54	.83	753.
2.000	17	2.97	2205	- 49	3.89	4.25	2.47	1.10	841.
3.000	1.22	3.86	1138	1.35	4.16	5.12	3.06	1.19	842.
₩.000	2.01	4.76	.0281	2.62	4.4B	6.30	3.73	1.32	B+3.
5.000	2.52	5.58	.0809	3.38	4.83	7.28	4.39	1.19	844.
6.000	3.17	6.47	.1183	3.91	5.39	B.27	5. <i>2</i> 6	1.17	Br. v
7 000	4.22	7.23	.1317	4.51	6.C9	9.54	€.04	1.25	844.
8,000	5.30	8.11	1506	5.34	6.83	11.02	6.9 6	1.21	6+5.
9 000	6.60	0.98	. 1350	6.55	7.65	15.9	7.67	: .06	Briti.
10.000	7.84	9.81	.1351	7.87	8.40	14.84	8.38	1.01	₽+1.
000.11	9.02	10.54	.1216	9.50	9.25	16.89	9.08	. 95	838.
12.000	9.88	10.56	.1094	10.60	9.36	17.94	9.32	. 80	934.
13,000	10.01	10.19	.1522	10.80	9.10	17.81	9. <i>2</i> 9	.76	829.
14.000	8.76	8.92	.2063	9.77	₿.0₩	15.83	9.11	. E9	€28.
15 000	6.28	7 35	.2201	7.62	6.20	15 53	6.36	.67	52 ₩.
16.030	2.87	5.50	.2045	5.43	4.55	6 36	4.3C	. 78	855
17.000	43	4.09	.2254	3.54	3,53	5 80	2.87	.87	789.
18.000	-3.27	3.38	.2676	₹.06	2.73	5.33	2.30	.42	790.
19.000	-5.64	2.68	.1751	1.26	2.04	€.3	2.42	. 34	786.
020.03	-7.3a	2.39	.1257	. 62	1.77	7.67	2. <i>2</i> 6	. 30	775.
21 000	-9.05	2.55	.0730	.51	1.78	9.25	2.48	.14	762 .
22.000	-10.44	2,44	.0627	. 16	1.72	10.58	2.43	. 26	747.
23.000	-11.84	2.44	.0600	08	1.70	11.96	2.42	.20	732.
გ4.000	-13.18	2.55	0250	13	1.81	13.30	2.55	-10	724.
25.000	-14.18	2.61	0314	09	1.74	14.29	2.60	. 18	724.
26.000	-15.02	2.79	0180	.05	1.90	15.15	2.78	. 44	709.
27.000	-15.72	3.00	.¢287	03	2.11	15.86	3.00	. 36	675.
29 .00 0	-16.15	2.93	0307	. 06	1.95	16.27	2.93	.22	588.
29.000	-16.69	3.10	.0107	. 13	2.22	{6. 83	3.09	.05	570.
30,000	-17.42	3.19	.0323	01	2.11	17.54	3.18	.12	540.
32.000	-22.68	3.62	1768	1.62	5.74	55.90	3.64	15	139.
34.000	-23.71	3.45	.0000	1.35	3.06	23.95	3.42	.01	140.
36.000	-26.52	4.35	0731	1.03	3.40	26.7G	4.32	03	140.
38,000	-29.23	4.81	1289	1.18	4.27	29.58	4.74	21	142.
40.030	-33.29	4.27	.0572	~.09	4.25	33.55	4.33	~.05	142.
42.000	-38.10	4.87	.0443	.05	5.28	39.46	4.87	~.20	142.
44.000	-42.09	5.35	. 0585	2.13	5.87	42.56	5.25	2:	142.
46.000	-44.74	6.25	.1210	4.62	5.34	45.30	6.15	.23	142.
48.000	-47.31	6.55	.1203	4.97	6.18	47.98	6.48	. 19	142.
50.02 0	-51.35	7.15	.1017	5.79	5.95	52.04	7.05	01	141.
52.000	-53.83	8 32	.2111	7.11	7.00	54.78	8.07	. 04	136.
54.000	-54.76	9.04	.1272	7.42	7.32	55.78	8.60	24	153.
56.000	-57.97	10.73	.1770	5.20	9.67	59.10	10.30	. 03	182.
58.000	-59. 85	13.02	.24+8	1.75	12.31	61.18	12.69	~.06 ~~	105.
60.00 0	-60.03	17.21	. 1480	2.25	13.50	e: es	16.71	~.2 5	76.
68.000	-62.04	20.10	.0455	5.62	12.38	ちょ.と	19.77	.08	61 .
64.00 0	-56.71	51.39	.1401	7.79	11.35	58 56	20.77	. (3	54.
£5.000	-45.11	23.71	.1581	10.43	14.17	13 52	21.80	.04	51. 49.
58 .00 0	-35.03	21.35	0473	9.30	51 .55	42.90	19.30	.45	46.
70.000	-25.92	22.64	.0338	5.10	25.12	37.96	19.59	.58	70.

TABLE 1-8. WIND STATISTICAL PARAMETERS

AUGUST

STATION	- 723930	VANDEN	BERG AFB						
Z	MEAN U	5.0. U	R(U.V)	MEAN V	5.0. Y	MEAN HS	S.D. NS	SKEH HS	NOBS
KP4	H/S	M/S		H/S	M/S	M/S	H/S		
. 100	1.94	2.01	5937	-1.54	2.00	3.00	2.27	.95	795.
1.000	.47	2.60	2735	-1.98	4.00	4.47	2.62	.75	807.
2.000	. 11	3.29	3116	41	4.14	4.54	2.75	1.12	₽45.
3.000	1.44	4.19	2384	1.16	4.19	5.32	3.20	. 89	844.
4.000	2.24	5.04	1396	2.10	4.33	6.22	3.85	1.20	e 50.
5.000	2.87	5.96	0397	2.67	4.70	7.23	4.55	1.37	952.
€ 000	3.92	6.75	0023	3.01	5.45	8.37	5.45	l . 35	852.
ניסם . ד	5.27	7.29	.0653	3.€≥	6.38	9.79	6 .22	1.37	853.
8.0CG	6. <i>7</i> 7	7.69	.0553	4.39	7. 15	11.35	7.05	1.30	856.
9.000	8.35	8.53	.0610	5.39	7.9₩	13.21	7.75	1.19	857.
10.000	9.96	9.27	.0885	6.60	8.52	15.22	8.44	. 99	858.
11.000	11.55	10.16	.0853	7.77	9.36	17.33	9.17	. 83	858 .
12.000	12.49	10.37	.0279	8.76	9.36	18.49	9.27	.62	856.
13.000	12.47	9.84	.0182	9.04	8.96	18.32	9 .86	.61	853.
14.000	11.13	8.33	.0147	0.22	7.75	16.28	7.49	. → 0	84B.
15.000	8.29	6.73	.0149	6.55	5.94	12.63	5.72	. 40	845.
16.000	4.61	5.27	0363	4.70	4.45	8.63	4.06	.58	838.
17.000	1.!0	4.39	0080	2.94	3.56	5.71	3.04	1.06	814.
18.000	-1.89	3.65	.0507	1.82	2.79	4.75	2.32	.45	813.
19.000	-4,43	3.21	0057	. 99	2.22	5.44	2.49	. 54	9 06.
20.000	-6.43	2.74	0745	. 59	1.89	6.82	2.50	. 23	793.
81.000	-9.04	2.70	0233	. 36	1.85	8.28	2.63	.06	78⊶.
88.000	-9.57	2.58	0242	.06	1.56	9.71	2.56	.20	769.
53 000	-11.01	2.57	0515	.02	1.63	11.13	2.55	. 22 .	7 56 .
24.000	-12.34	2.74	~.1185	05	1.78	12.47	2.74	. 05	75C.
25.000	-13.37	2.77	1167	05	1.73	13.48	2.76	. 13	744.
26.000	-14.30	2.80	0069	12	1.79	14.41	2.79	. 17	731.
27.CCO	-15.04	3.06	0036	.01	1.92	15.16	3.05	.05	704.
29.000	-15.47	3.17	.0676	. 15	1.86	15.58	3.1 5	. 09	584.
<i>2</i> 9.000	-15.93	3.36	0517	.21	2.10	16.07	3.34	.22	5 43.
30.000	-16.37	3.30	0570	. 11	≥.08	16.51	3.26	. 05	457.
32 .000	-20.93	3.57	.0391	1.64	a.78	21.18	3.55	02	126.
54 . 000	-21.71	4.96	.2729	1.17	2.72	21.92	4.B8	~.08	126.
36 .000	-23.34	5.34	.0641	.72	3.07	23.56	5.30	26	124.
38.000	-25.44	6.10	0518	. 17	3.89	25.74	6 07	.10	130.
40.000	-27. 30	7.53	.0218	. 10	4.39	27.65	7.51	11	132.
42.000	-30.51	7.68	.0360	01	4.60	30.87	7.59	. 38	132.
44.000	-34.58	8.42	1267	1.02	4.68	34.91	8.40	.53	133.
46.000	-36. 56	7.63	0489	2.53	6.17	37.25	7.60	.01	133.
'48.COO	-37.52	9.74	0358	4.78	7.50	38.62	9.45	15	133.
50.000	-38.48	10.98	2193	6.09	7.71	39.80	10.64	20	133.
52.000	-37.82	13.18	1219	6.07	8.79	39.47	12.64	- , 444	132.
54.000	-37.13	14.25	.0231	6.34	9.36	39.02	13.64	. 02	131.
56.000	-36.07	17.96	.0825	5.18	10.02	38.30	16.81	. 12	123.
58.000	-33.72	17.78	0014	4.34	10.48	36.15	16.55	.46	115.
60.000	-32.06	17.75	.0782	2.06	12.60	35.07	16.55	. 25	85.
62.000	-32.40	19.15	.3019	1.15	13.68	35 .85	17.77	17	67.
64.000	-24.69	19.63	. 1932	3.29	15.19	30.66	17.04	.50	56.
56.000	-16.35	19.05	.0879	1.98	19.21	26.91	16.44	.61	54.
60.000	-11.01	23.18	.3064	1.46	20.83	27.11	18.72	. 70	54.
70.000	~1.99	21.64	. 2588	2.87	16.05	23.39	13.42	1.10	51.

TABLE 1-9. WIND STATISTICAL PARAMETERS
SEPTEMBER

STATION .	270 71	VANCERE	ERG AFB						
Z	MEANU	5.D. U	R(U,V)	MEAN V	5.D. V	HEAN HS	5.D. WS	skeh hs	NOB5
KM:	M/5	M/S		M/5	H/5	H/S	H S		
100	1.67	2.15	5420	-1.40	2.21	2.93	2.30	. 96	764
1.000	33	2.68	- 2944	-1.48	4.43	4.69	2.83	.26	804
2.000	51	4.07	2976	09	5.11	5.54	3.50	1.32	838
3.000	.69	5.29	2091	. 83	5.71	6.68	4.12	1.13	836 .
4.000	1.74	6.43	~.1358	1,14	6.36	7.73	5.05	1.08	039 .
5.000	3.01	7.36	0730	.96	7.09	8.89	5.93	1.10	837.
6.000	4.29	8.51	.0216	.74	8.03	10.31	7.03	1.13	837.
7.000	5.61	9,47	.1054	.65	8.99	12.04	7.60	.98	836.
8.000	7.24	10.43	.1963	1.05	10.12	13.99	8.30	.90	835.
9.003	9.08	11.53	.2876	1.43	11.33	16.14	9.30	.96	835.
10.000	11.23	12.59	. 3252	2.00	12.29	18.28	10.26	. 75	837.
11.000	13.62	13.46	.3314	2.53	12.84	20.29	11.23	.72	833.
12.000	15.41	13.32	3271	3.22	12.59	21.25	11.49	.78	835
13.000	15.83	12.25	. 3067	3.61	11.73	20.72	11.06	.87	8 28.
(4 220	14.44	10.09	.2840	3.38	9.75	18.26	9.13	. 70	826.
:5.000	11.79	0.18	.2573	2.66	7.80	14 87	7.25	. 68	820.
16.000	8.35	6.58	.2218	1.90	5.93	10.85	5.84	1.18	804.
17.000	4.91	5.15	.1154	.97	4.46	7.29	4.28	1.12	781.
17.000	1.81	4.31	.1047	. 🔀	3.41	4.97	2.98	1.16	783.
19.000	50	3.93	.1245	03	2.65	4.14	2.35	1.07	769.
50.000	-2.03	3.73	.0377	بدخ _	2.16	4.23	2.21	.60	766.
21.000	-3.35	3.55	.0410	35	2.10	4.78	2.36	. 67	745.
22.000	-4.28	3.43	.6344	39	1.84	5.24	2.47	.28	733.
23.000	-5.05	3.72	.1103	38	1.74	5.93	2.70	. 18	718.
24.000	-5.72	4.20	.0730	26	1.94	6.64	3.17	.72	711.
25.000	-6.21	4.33	.0970	18	1.89	7.08	3.27	.28	719.
26.000	-6.75	4.71	.0670	10	1.96	7.63	3.60	. 32	697
27.000	-7.09	5.12	.0550	.00	2.01	8.35	3.97	. 36	634
28.000	-7.43	5.08	.0-18	. 17	1.98	8.33	3.89	.25	545.
29.600	-7.60	5.25	3300.	.29	2.14	8.61	3.97	. 37	501
30.000	-7.45	5.3→	. (66 5	.24	2.17	8.45	4,16	. 32	473.
32.000	-9.04	5.80	.1583	1.46	2.87	10.01	5.03	. 52	111.
34 000	-7.35	5.84	.1810	2.60	3.33	9.27	4.45	. 36	111.
36.000	-5.06	6.75	.1430	1.06	3.33	8.29	5.07	. 58	112.
38.000	-6.80	7.35	0398	13	4.17	9.39	5.39	.51	112.
40.000	-8.31	8.47	0810	73	4.00	10.96	6. 35	.49	113.
42.000	-9.74	8.52	.0728	.50	5.06	12.12	5 .77	. 30	113.
44.000	-10.59	8.82	0290	1.33	5.93	13.16	7.30	.47	113.
46.000	-10.10	10.47	0130	2.60	5.46	13.75	7.64	.78	113.
48.000	-8.38	11.00	0924	3.55	5.62	12.95	8.19	.93	112.
50.000	-7.03	11.33	0344	4.33	6.78	13.20	8.07	.95	111.
52.000	-4.97	12.70	.0056	يها . نها	6.81	13.28	8.63	1.05	107
54.000	-1.85	12.66	1756	5.94	6.23	13.65	7.06	.81	104.
56.000	£.75	11.12	2022	5.08	7.52	13.08	6.40	- 114	99.
58.000	4.53	12.45	.0026	ı. B0	8.07	14.20	6.38	.60	69.
53.000	4.56	15.02	.06+0	2.55	8.38	15.81	6.36	.55	68. 44.
62.000	7.77	15.00	1038	5.83	7.52	16.70	9.63	.76	41.
E4.000	12.61	12.69	0533	6.51	8.79	19.22	8.13	. 24	40.
66.000	15.09	12.13	337 7	5.69	9.80	20.97	7.65	.23	39.
69.000	16.03	10.87	0277	4.23	9.21	19.49	9.77	.59	39.
70.000	19.64	12.98	.2132	-1.21	11.05	23.00	12.04	. 39	39.

TABLE I-10. WIND STATISTICAL PARAMETERS

OCTOBER

34,000 15.27 10.87 .2372 3.04 5.12 17.09 9.74 .83 139 36.000 19.74 11.16 .3955 2.89 5.41 20.91 10.70 .62 139 38.000 23.33 13.08 .4642 2.17 5.66 24.27 12.75 .34 139	9 0. 31.
Not M/S M/S M/S M/S M/S M/S M/S M/S M/S 1.000 1.333 2.377 5680 -1.333 2.599 3.090 2.590 1.057 831 2.000 .411 4.42 2882 -1.377 6.099 6.64 3.83 .86 855 3.000 1.89 5.88 2.299 -1.56 7.07 8.14 4.92 1.09 856 855 3.000 3.64 7.45 -1.021 -1.93 8.38 10.13 6.32 1.05 857 5.000 5.24 8.73 0.179 -1.81 9.56 12.62 7.32 95 857 6.000 6.73 9.92 0.0721 -1.69 10.69 14.02 8.29 9.90 8.22 11.15 1.195 -1.78 12.43 16.17 9.38 .84 857 8.000 11.24 13.38 .284 -1.43 15.31 20.34 11.23 6.2 655 10.000 12.88 13.98 .3149 -1.33 16.20 22.13 11.64 53 655 10.000 12.88 13.98 .3149 -1.33 16.20 22.13 11.64 53 655 11.000 16.46 14.11 .3.499 -7.78 15.18 23.399 12.01 .59 651 13.000 16.46 14.11 .3.499 -7.78 15.18 23.399 12.01 .59 651 15.000 14.18 9.30 .2375 -4.49 9.39 17.48 8.37 .46 6.90 14.100 14.18 9.30 .2375 -4.49 9.39 17.48 8.37 .46 6.50 6.37 5.39 11.100 14.18 9.30 .2375 -4.49 9.39 17.48 8.37 .46 6.50	31.
1.00	31.
1.000	
3 000 1.89 5.882239 -1.56 7.07 8.14 4.92 1.09 856 4.000 3.64 7.45 -1.021 -1.93 8.38 10.13 6.32 1.05 857 5.000 5.24 8.73 .0179 -1.81 9.56 12.02 7.32 .99 857 6.000 6.73 9.92 .0721 -1.68 10.89 14.02 8.28 .90 857 7.000 8.22 11.15 .1195 -1.78 12.43 16.17 9.38 .94 857 9.000 11.24 13.38 .2594 -1.43 15.31 20.36 11.23 .62 855 10.000 12.88 13.99 .3149 -1.33 16.20 22.13 11.64 .53 854 11.000 14.79 14.37 .3318 -1.04 16.13 23.30 11.96 .54 851 12.000 16.46 14.11 .3489 -7.78 15.18 23.3.59 12.01 .59 851 13.000 16.61 12.43 .2951 -56 13.45 22.39 10.81 .38 851 14.000 15.69 10.88 .2651 -28 11.56 20.25 9.71 .46 850 15.000 14.18 9.30 .2375 -49 9.39 17.48 8.37 .46 845 17.000 9.03 6.24 .211 -7.7 5.64 11.04 5.55 .50 801 19.000 6.37 5.39 .1738 -1.05 4.44 8.33 4.59 1.2 888 875 19.000 1.61 4.22 2401 -1.28 3.52 6.28 3.56 1.15 792 20.000 2.59 4.28 .3013 -1.27 3.20 5.2 2.9 1.06 783 21.000 1.61 4.23 .215 -1.65 792 22.000 1.61 4.24 .23 .2951 -5.66 2.69 7.35 14.16 6.99 .42 824 23.000 1.61 4.29 .23 .2401 -1.28 3.52 6.28 3.56 1.15 792 24.000 3.98 4.72 .2401 -1.28 3.52 6.28 3.56 1.15 792 25.000 2.59 4.28 .3013 -1.27 3.20 5.32 2.92 1.06 783 25.000 2.59 4.28 .291 .738 -1.05 4.94 8.33 4.59 1.12 801 19.000 3.98 4.72 .2401 -1.28 3.52 6.28 3.56 1.15 792 25.000 3.98 5.57 .2000 -0.09 2.78 6.09 4.09 1.35 6.71 25.000 3.99 5.57 .2000 -0.09 2.78 6.09 4.09 1.35 6.71 25.000 3.99 5.57 .2000 -0.09 2.78 6.09 4.09 1.35 6.71 25.000 3.99 5.57 .2000 -0.09 2.78 6.09 4.09 1.36 6.75 27.000 9.01 7.31 .2095 .14 3.10 9.30 5.48 1.40 5.44 6.33 4.59 1.20 6.30 6.35 6.24 6.25 1.999 .07 2.91 7.05 4.69 1.30 5.49 1.40 5.40 5.40 6.30 6.30 6.30 6.30 6.30 6.30 6.30 6.3	
3.000	
5.000 5.24 8.73 .0179 -1.81 9.56 12.02 7.32 .95 857 6.000 6.73 9.92 .0721 -1.68 10.69 14.02 8.28 .90 .97 7.000 8.22 11.15 .1195 -1.78 12.43 16.17 9.38 .84 .95 8.000 9.67 12.37 .1756 -1.56 13.92 18.30 10.36 .75 .955 9.000 11.24 13.38 .2594 -1.43 15.31 20.36 11.23 .62 .655 10.000 12.68 13.98 .3149 -1.33 16.20 .22.13 11.04 .53 .65 .655 11.000 14.79 14.37 .3318 -1.04 16.13 .23.30 11.96 .54 .651 12.000 16.46 14.11 .3489 -7.78 15.16 23.59 12.01 .59 .651 13.000 16.41	
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17.000 9.03 6.24 .211177 5.64 11.04 5.56 .50 801 18.000 6.37 5.39 .1738 -1.05 4.44 8.33 4.59 1.12 801 19.000 3.98 4.72 .2401 -1.28 3.52 6.28 3.56 1.15 792 20.000 2.59 4.29 .3013 -1.27 3.20 5.32 2.92 1.06 783 21.000 1.71 4.25 .2674 -1.25 2.92 4.76 2.91 1.31 757 22.000 1.61 4.23 .2175 -1.15 2.75 4.58 2.89 1.45 745 23.000 1.81 4.24 .227286 2.64 4.46 2.99 1.52 726 24.000 2.21 4.71 1.72656 2.64 4.92 3.35 1.60 723 25.000 2.95 5.07 .140126 2.69 5.32 3.66 1.56 717 25.000 3.84 5.57 .200009 2.78 6.09 4.04 1.36 695 27.000 4.92 6.25 1.999 .07 2.91 7.05 4.69 1.39 635 28.000 6.66 6.71 .2085 1.4 3.10 8.30 5.48 1.40 552 28.000 8.01 7.31 .2894 1.6 3.31 9.57 6.08 1.38 511 30.000 9.11 7.92 .2934 .19 3.45 10.58 6.75 1.37 461 32.000 15.27 10.87 2.372 3.04 5.12 17.09 9.74 .83 38.000 15.27 10.87 2.372 3.04 5.12 17.09 9.74 .83 38.000 23.33 13.08 .4642 2.17 5.66 24.27 12.75 .34 133	
18.000 6.37 5.39 1.738 -1.05 4.44 8.33 4.59 1.12 801 19.000 3.98 4.72 2.401 -1.28 3.52 6.28 3.56 1.15 792 20.000 2.59 4.28 3.013 -1.27 3.20 5.32 2.92 1.06 783 21.000 1.71 4.25 2.674 -1.25 2.92 4.76 2.91 1.31 757 22.000 1.61 4.23 2.175 -1.15 2.75 4.58 2.89 1.45 745 23.000 1.81 4.24 2.27286 2.64 4.46 2.99 1.45 745 24.000 2.21 4.71 1.72656 2.64 4.92 3.35 1.60 723 25.000 2.95 5.07 1.40126 2.69 5.32 3.66 1.56 717 25.000 3.84 5.57 200009 2.78 6.09 4.04 1.36 695 27.000 4.92 6.25 1.999 .07 2.91 7.05 4.69 1.39 6.55 28.000 6.66 6.71 2.005 1.4 3.10 8.30 5.48 1.40 5.54 29.000 9.11 7.92 2.934 1.9 3.45 10.50 6.75 1.37 46.3 30.000 9.11 7.92 2.934 1.9 3.45 10.50 6.75 1.37 46.3 34.000 15.27 10.87 2.582 1.77 3.95 13.47 9.03 1.01 1.35 34.000 15.27 10.87 2.372 3.04 5.12 1.70 9.74 .83 1.33 34.000 15.27 10.87 2.372 3.04 5.12 17.09 9.74 .83 1.33 34.000 19.74 11.16 3.355 2.89 5.41 20.91 10.70 6.2 1.33 36.000 23.33 13.08 4.642 2.17 5.66 24.27 12.75 .34 13.3	
19.000 3.98 4.72 .2401 -1.28 3.52 6.28 3.56 1.15 792 20.000 2.59 4.28 3.013 -1.27 3.20 5.32 2.92 1.06 783 21.000 1.71 4.25 .2674 -1.25 2.92 4.76 2.91 1.31 757 22.000 1.61 4.23 .2175 -1.15 2.75 4.58 2.89 1.45 745 23.000 2.21 4.71 1.1726 -1.56 2.84 4.92 3.35 1.60 723 25.000 2.21 4.71 1.1726 -1.56 2.84 4.92 3.35 1.60 723 25.000 2.95 5.07 1.401 -226 2.69 5.32 3.66 1.56 717 25.000 3.84 5.57 .2000 -0.09 2.78 6.09 4.04 1.36 695 27.000 4.92 6.25 1.999 0.7 2.91 7.05 4.69 1.38 693 28.000 5.66 6.71 .2085 1.14 3.10 8.30 5.48 1.40 554 29.000 8.01 7.31 .2894 1.6 3.31 9.57 6.08 1.38 511 30.000 9.11 7.92 .2934 1.19 3.45 10.58 6.75 1.37 463 32.000 15.27 10.87 2372 3.04 5.12 17.09 9.74 .83 1.37 463 34.000 15.27 10.87 2372 3.04 5.12 17.09 9.74 .83 1.33 36.000 19.74 11.16 3.355 2.89 5.41 20.91 10.70 .62 133 36.000 23.33 13.08 .4642 2.17 5.66 24.27 12.75 .34 133	
20.000	
21.000 1.71 4.25 .2674 -1.25 2.92 4.76 2.91 1.31 757 22.000 1.61 4.23 .2175 -1.15 2.75 4.58 2.89 1.45 745 23.000 1.81 4.24 .227286 2.64 4.46 2.99 1.52 726 24.000 2.21 4.71 1.72656 2.64 4.92 3.35 1.60 723 25.000 2.95 5.07 1.40126 2.69 5.32 3.66 1.56 717 25.000 3.84 5.57 .200009 2.78 6.09 4.04 1.36 695 27.000 4.92 6.25 1.999 .07 2.91 7.05 4.69 1.38 635 27.000 4.92 6.25 1.999 .07 2.91 7.05 4.69 1.38 635 28.000 5.66 6.71 .2085 1.4 3.10 8.30 5.48 1.40 552 29.000 8.01 7.31 .2894 1.6 3.31 9.57 6.08 1.38 511 30.000 9.11 7.92 .2934 .19 3.45 10.58 6.75 1.37 461 32.000 11.78 10.28 .2582 1.77 3.95 13.47 9.03 1.01 135 34.000 15.27 10.87 2.372 3.04 5.12 17.09 9.74 .83 133 36.000 23.33 13.08 .4642 2.17 5.66 24.27 12.75 .34 133	
22.000 1.61 4.23 .2175 -1.15 2.75 4.58 2.89 1.45 745 23.000 1.81 4.24 .227286 2.64 4.46 2.99 1.52 726 24.000 2.21 4.71 1.72656 2.84 4.92 3.35 1.60 723 25.000 2.95 5.07 1.40126 2.69 5.32 3.66 1.56 717 25.000 3.84 5.57 .200009 2.78 6.09 4.04 1.36 695 27.000 4.92 6.25 1.999 .07 2.91 7.05 4.69 1.38 635 28.000 5.66 6.71 .2095 1.4 3.10 8.30 5.48 1.40 554 29.000 8.01 7.31 .2095 1.4 3.10 8.30 5.48 1.40 554 29.000 8.01 7.31 .2095 1.4 3.10 8.30 5.48 1.40 554 30.000 9.11 7.92 .2934 1.9 3.45 10.58 6.75 1.37 463 32.000 11.78 10.28 .2582 1.77 3.95 13.47 9.03 1.01 133 34.000 15.27 10.87 .2372 3.04 5.12 17.09 9.74 .83 133 36.000 23.33 13.08 .4642 2.17 5.66 24.27 12.75 .34 133 130.000 23.33 13.08 .4642 2.17 5.66 24.27 12.75 .34 133	
23.000 1.81 4.24 .227286 2.64 4.46 2.99 1.52 726 24.000 2.21 4.71 .172656 2.64 4.92 3.35 1.60 723 25.000 2.95 5.07 .140126 2.69 5.32 3.66 1.56 717 25.000 3.84 5.57 .200009 2.78 6.09 4.04 1.36 695 27.000 4.92 6.25 1.999 .07 2.91 7.05 4.69 1.36 635 28.000 5.66 6.71 .2005 .14 3.10 8.30 5.48 1.40 554 29.000 8.01 7.31 .2094 .16 3.31 9.57 6.08 1.38 511 30.000 9.11 7.92 .2934 .19 3.45 10.58 6.75 1.37 463 32.000 15.27 10.87 .2372 3.04 5.12 17.09 9.74 .83 13 34.000 15.27 10.87 .2372 3.04 5.12 17.09 9.74 .83 13 38.000 23.33 13.08 .4642 2.17 5.66 24.27 12.75 .34 13	
24.000 2.21 4.71 .172656 2.84 4.92 3.35 1.60 723 25.000 2.95 5.07 .140126 2.69 5.32 3.66 1.56 717 25.000 3.84 5.57 .200009 2.78 6.09 4.04 1.36 695 27.000 4.92 6.25 1.999 .07 2.91 7.05 4.69 1.38 6.35 28.000 5.66 6.71 .2085 1.4 3.10 8.30 5.48 1.40 554 29.000 8.01 7.31 .2084 1.6 3.31 9.57 6.08 1.38 511 30.000 9.11 7.92 .2934 1.9 3.45 10.58 6.75 1.37 461 32.000 11.78 10.28 .2582 1.77 3.95 10.58 6.75 1.37 461 32.000 15.27 10.87 .2372 3.04 5.12 17.09 9.74 .83 101 138 38.000 15.27 10.87 .2372 3.04 5.12 17.09 9.74 .83 138 38.000 23.33 13.08 .4642 2.17 5.66 24.27 12.75 .34 133	
25.000 2.95 5.07 .140126 2.69 5.32 3.66 1.56 717 25.000 3.84 5.57 .200009 2.78 6.09 4.04 1.36 695 27.000 4.92 6.25 1.999 .07 2.91 7.05 4.69 1.38 635 28.000 5.66 6.71 .2085 1.4 3.10 8.30 5.48 1.40 552 29.000 8.01 7.31 .2894 1.6 3.31 9.57 6.08 1.38 511 30.000 9.11 7.92 .2934 .19 3.45 10.58 6.75 1.37 461 32.000 11.78 10.28 .2582 1.77 3.95 13.47 9.03 1.01 135 34.000 15.27 10.87 .2372 3.04 5.12 17.09 9.74 .83 135 38.000 23.33 13.08 .4642 2.17 5.66 24.27 12.75 .34 135	
25.000 2.95 5.07 .140126 2.69 5.32 3.66 1.56 717 25.000 3.84 5.57 .200009 2.78 6.09 4.04 1.36 695 27.000 4.92 6.25 .1999 .07 2.91 7.05 4.69 1.38 635 28.000 5.66 6.71 .2085 .14 3.10 8.30 5.48 1.40 554 29.000 8.01 7.31 .2894 .16 3.31 9.57 6.08 1.38 511 30.000 9.11 7.92 .2934 .19 3.45 10.58 6.75 1.37 461 32.000 11.78 10.28 .2582 1.77 3.95 13.47 9.03 1.01 139 34.000 15.27 10.87 .2372 3.04 5.12 17.09 9.74 .83 13 36.000 19.74 11.16 .3955 2.89 5.41 20.91 10.70 .62 135 38.000 23.33 13.08 .4642 2.17 5.66 24.27 12.75 .34 133	
27.000 4.92 6.25 .1999 .07 2.91 7.05 4.69 1.38 635 28.000 6.66 6.71 .2095 .14 3.10 8.30 5.48 1.40 554 29.000 8.01 7.31 .2094 .16 3.31 9.57 6.08 1.38 511 30.000 9.11 7.92 .2934 .19 3.45 10.58 6.75 1.37 463 32.000 11.78 10.28 .2582 1.77 3.95 13.47 9.03 1.01 133 34.000 15.27 10.87 .2372 3.04 5.12 17.09 9.74 .83 135 36.000 19.74 11.16 .3955 2.69 5.41 20.91 10.70 .62 135 38.000 23.33 13.08 .4642 2.17 5.66 24.27 12.75 .34 133	
28.000 5.66 6.71 .2085 .14 3.10 8.30 5.48 1.40 554 29.000 8.01 7.31 .2084 .16 3.31 9.57 6.08 1.38 511 30.000 9.11 7.92 .2934 .19 3.45 10.58 6.75 1.37 461 32.000 11.78 10.28 .2582 1.77 3.95 13.47 9.03 1.01 133 34.000 15.27 10.87 .2372 3.04 5.12 17.09 9.74 .83 155 26.00 19.74 11.16 .3955 2.89 5.41 20.91 10.70 .62 135 38.000 23.33 13.08 .4642 2.17 5.66 24.27 12.75 .34 13	
29.000 8.01 7.31 .2894 .16 3.31 9.57 6.08 1.38 511 30.000 9.11 7.92 .2934 .19 3.45 10.58 6.75 1.37 461 32.000 11.78 10.28 .2582 1.77 3.95 13.47 9.03 1.01 139 34.000 15.27 10.87 .2372 3.04 5.12 17.09 9.74 .83 138 38.000 19.74 11.16 .3955 2.89 5.41 20.91 10.70 .62 138 38.000 23.33 13.08 .4642 2.17 5.66 24.27 12.75 .34 133	
30.000 9.11 7.92 .2934 .19 3.45 10.58 6.75 1.37 463 32.000 11.78 10.28 .2582 1.77 3.95 13.47 9.03 1.01 139 34.000 15.27 10.87 .2372 3.04 5.12 17.09 9.74 .83 139 36.000 19.74 11.16 .3955 2.89 5.41 20.91 10.70 .62 139 38.000 23.33 13.08 .4642 2.17 5.66 24.27 12.75 .34 139	
32.000 11.78 10.28 .2582 1.77 3.95 13.47 9.03 1.01 135 34.000 15.27 10.87 .2372 3.04 5.12 17.09 9.74 .83 139 36.000 19.74 11.16 .3955 2.89 5.41 20.91 10.70 .62 135 38.000 23.33 13.08 .4642 2.17 5.66 24.27 12.75 .34 135	
39.000 15.27 10.87 .2372 3.04 5.12 17.09 9.74 .83 139 36.000 19.74 11.16 .3955 2.89 5.41 20.91 10.70 .62 139 39.000 23.33 13.08 .4642 2.17 5.66 24.27 12.75 .34 139	
36,000 19.74 11.16 .3955 2.89 5.41 20.91 10.70 .62 139 38.000 23.33 13.08 .4642 2.17 5.66 24.27 12.75 .34 139	39.
38.000 23.33 13.08 .4642 2.17 5.66 24.27 12.75 .34 13	
38.000 23.33 73.00 7.012 2.11	39 .
uningan persentua puen 146 174 13.92 146 146	39.
	40.
45,000 60.73 10.64 .0407 .34	40.
44,070 31.00 13.03	40.
40.000 33.00 10.04	39.
40.000 33.43 10.04 .1330 3.33	39.
10.000 40.13	30
36.000 43.33 10.00 .101	35
74 000 41/22 11/34 12/3C) 8/10 0/20 12/20 1	32.
30.000 30.03 77.10 3003 0.33	31.
20,000 20,00 10.00 1.00	٠, يوح
00.030 35.31 10.43 14031 0.10 10.0. 30.3	90.
CE:000 33.30 E0.45 10335 0.13 11.01 3.130 0.13	65.
04.000 54.17 E3.15 1.104 F.O.	53.
QC.000 31.80 27.18 .3303 4.34 47.73 33.73 2.73	53.
64.000 47.25 Sc.81 (2.35 3.30 St.01 St.02	52.
70.000 45.35 30.33 .009105 15.78 49.38 27.91 .14 41	٦ ٠ .

TABLE I-11. WIND STATISTICAL PARAMETERS

NOVEMBER

STATION	723330	VANCEN	BIERG AFB						
Z	HEAN U	5.D. U	RIU.VI	MEAN V	S.D. V	MEAN HS	5.D. #S	SKEH HS	NORS.
KC4	H/5	M/S		H/S	11/5	M/S	H/S		
. 100	.82	2.61	~.5500	-1.29	3.09	3.53	2.49	1.19	B+4.
0C2.1	. 29	3.70	¢8 →5	-1.89	6.65	6.51	4.22	.96	874.
8.000	2.12	4.91	~.0642	-1.89	7. 6 4	8.23	4.78	.68	9 92.
3.000	4.60	6.54	.0165	-2.43	8.79	10.64	5.81	.73	894.
₩ .000	7.00	8.09	.0737	-2.50	9.96	13.07	6.99	.58	897.
5.000	9.16	9.60	.1483	-2.43	11.21	15.40	B. 37	.69	8 97.
€.000	11.08	10.95	.2033	-2.40	12.64	17.92	9.60	. 84	894.
7.600	12.79	12.17	.2473	-2.67	14.56	20.38	10.74	. 83	892.
8.000	19.47	13.34	.2790	-2.75	15.74	22.57	11.52	.67	8 94.
9.000	16.12	14.55	.3308	-5.83	17.33	24.8:	12.80	.76	8 82.
10.000	17.68	15.42	. 3474	-3.04	18.19	26.64	12.42	.73	8 78.
1:.000	18.97	15.68	. 3666	-3.24	18.07	27.67	13.31	. 65	867.
15.000	20.03	15.33	.3758	-2.91	17.23	27 79	12.99	.62	9 63.
13.000	50.05	13.73	.3731	-2.58	15.15	26. 36	11.41	.48	8 59.
14.000	18.50	11.49	. 3674	-1.97	12.54	23.34	9.50	. 34	8 51.
15.000	16.61	9.55	.3483	-1.96	10.66	20.40	B. 22	. 36	846.
16.000	14.07	8.02	.3242	-1.55	8.62	17.91	7.05	. 33	8 ₩1.
17.000	11.59	6.88	.3091	-1.66	7.13	14.06	6.12	.45	0 13.
18 000	8.70	6.01	+583.	-1.71	5.61	10.93	5.15	. 65	812.
19.000	6.46	5.44	.2760	-1.75	4.62	8.70	4.48	1.00	802.
20.000	4 . 84	5.23	.2169	-1.93	3.96	7.39	3.92	1.07	792.
81,000	3.69	5.40	.1424	-2.02	3.55	6.82	3.79	.92	778.
55.000	3.51	5.9≥	.1169	-5.04	3.48	6.90	4.00	1.45	773.
83.000	3.66	6.40	.1783	-1.67	3.19	7.09	4.12	1.23	766.
24.000	3.87	7.21	.1677	-1.37	3.20	7.60	4.61	1.06	762.
25.000	4.96	7.95	.2661	99	3.33	8.46	5.21	1.33	751.
26.000	5.95	9.07	. 3901	84	3.29	9.46	6.31	1.08	731.
27.000	7.0B	10.64	.4473	~ .64	3.53	10.89	7.58	1.09	569 .
26.000	9.03	12.20	.4895	58	4.01	13.02	8.78	. 99	590.
29.000	10.72	13.30	.5287	- , 44	4.31	14.51	10.00	1.01	531.
30.000	12.72	14.37	.5465	23	4.79	16.23	11.30	.96	512.
32.000	20.05	15.95	.5868	1.99	5.63	21.79	14.72	.75	99.
34.000	24.41	17.33	.5526	2.79	6.23	25.93	16.41	٥٦.	99.
36.000	29.23	16.78	.5215	3.65	7.42	30.62	16.31	. 38	101.
38.000	33.92	18.39	. 5 65 6	2.57	7.36	35.15	17.69	. 30	101.
48.000	37.76	19.32	.5942	1.65	7.62	38.74	18.92	. 30	ימו.
42.000	40.88	19.07	.5222	3.57	7.10	41.53	19.03	. 15	100.
44.000	45.81	19.82	.4125	ટ.ફા	7.98	46.58	19.74	· C B	100.
46.000	51.36	21.79	.3918	3.79	9.45	52.32	21.88	12	100.
48.000	55.88	23.62	. 3984	6.67	11.59	57.35	23.86	03	100.
50.000	60.62	26.03	. 3974	8.36	13.42	62.61	26.62	07	99.
50.000	63.97	27.54	.4548	8.73	15.14	66.21	27.74	08	98.
54.000	66.87	27.58	. 3958	8.86	14.65	68.88	27.93	20	97.
56.000	67.78	26.63	.3155	7.45	14.36	69.68	26.61	37	93.
58.000	65.33	26.29	.2997	4.33	16.48	68.54	26.08	35	89 .
60.000	59.57	27.74	. 38 32	1.06	18.31	62.91	26.31	23	70.
62.000	59.65	27.63	.5009	.58	21.46	63.43	27.35	. 00	46,
64.000	55.70	27.12	.6446	-3.08	19.57	59.46	26.14	.50	37.
66.000	54.45	27.08	.6277	-3.58	26.06	61.06	25.27	. 10	36.
68.000	54.66	26.08	.5110	.51	23.59	60.0 8	24,44	.00	36,
70.000	53.62	23.04	.5227	-2.04	23.51	59.15	21.10	.51	34.

TABLE I-12. WIND STATISTICAL PARAMETERS

DECEMBER

STATION .	723930	VANDENE	EDRS AFB						
Z	HEAN U	S.D. U	RIU, VI	HEAN V	S.D. V	MEAN HS	5.D. WS	skeh ns	NOB5
101	M/S	M/S		M/5	M/S	M/5	M/S		
. 100	.47	2.70	5086	-1.11	3.00	3.50	2.34	1.09	652.
1.000	.75	4.32	1554	-2.22	7.20	7.32	4.73	.93	909.
2.000	3.07	5.64	C641	-3.01	8.20	9.36	5.47	.64	925.
3.000	5.70	7.22	.0108	-3.81	9.29	11.81	6.77	.69	926.
4 .000	8.28	9.08	.0245	جه. به -	11.16	14.83	8.64	.69	929.
5.000	10.45	10.54	.0855	-4.57	12.42	17.23	9.92	. 68	930.
6.000	12.48	11.97	.1524	-4.86	14.10	19 85	11.28	.66	929.
7.000	14.38	13.46	.2154	-5. <i>32</i>	15.61	22.48	12.68	.62	925
8.000	16.19	14.98	.2640	-5.55	17.13	83. • 5	13.92	.68	916. 899.
9.000	17.83	16.06	.3132	-5.73	18.01	26 BL	14.54	.64 .65	883.
10.000	19.54	16.67	. 3469	-5.98	18.71	28 64	15.00	.52	871.
11.000	20.87	16.62	. 3358	-5.98	18.00	29.29	14.58	.50	963.
15.000	21.83	15.39	.3053	-5.46	16.76	28.87	13.60	.53	959.
13.000	21.46	13.56	.3114	-4.52	14.59	26.90	12.40	.53	855.
14.000	20.02	11.53	.3466	-3.53	12.71	24.40	10.59 8.77	.44	847
15.000	17.88	9.76	.3318	-3.05	10.52	21.40 18.05	7.39	.64	837
16.000	15.03	8.16	. 3571	-2.71	8.98	14.96	7.39 6.39	.92	800.
17.000	12.30	7.06	.3608	-2.57	7.55	11.60	5.48	1.09	799.
18.000	9.23	6.12	. 3731	-2.39	6.03	9.01	4.81	1.02	792
19.000	6.38	5.74	.3025	-2.61	4.89 3.94	7.19	4.29	1.32	783
20.000	4.08	5.53	.3206	-2.70 -2.80	3.66	6.60	4.04	1.08	736.
21.000	2.40	5.73	.2456	-2.66	3.79	7.05	4.21	1.45	725.
22.000	1.29	6.67	.2611 .2533	-2.50	3.65	7.37	4.30	1.70	719.
23.000	.57	7.28	.e533	-2.66	3.59	7.97	4.42	1.02	730.
24 000	.04	7.84 8.92	.3017	-2.53	3.99	8.64	5.23	1.26	720
25.000	.29	10.42	.3533	-2.40	4.54	9.66	6.50	1.44	709.
26.000	. 98 2 . 38	12.18	. 3958	-2.29	92	11.05	7.81	1.30	637.
27.000	3.62	13.59	.5930	-2,42	5.48	12.33	9.03	1.38	595
29.000 29.000	5.83	15.43	.5419	-2.49	6.14	14.46	10.32	1.44	523 .
30.000	8.38	16.91	5-05	-2.64	7.07	16.65	11.64	1.38	561.
32.000	12.87	21.23	.6253	-2.34	7.42	51 68	14.00	. 60	142.
34.000	20.56	24.50	.6840	-1.05	8.81	29.33	15.63	.51	143.
36.000	28.66	25.74	.7300	13	9.80	35.73	17.31	. 11	144.
38.000	37.02	26.54	.6913	.07	10.53	42.70	18.95	13	144.
40.000	43.95	26.37	.6860	. 35	11.29	48.78	19.28	- 32	144.
92.000	50.11	27.07	.5720	3.43	13 29	55.02	20.04	52	144.
44.000	57.63	27.50	.4416	6.39	14.22	62.63	19.8→	69	144.
46.000	64.73	27.95	.3451	9.57	16.10	70.04	20. 27	68	144.
48.000	70.51	28.56	.3397	12.84	16.79	75.97	21.70	- 45	143.
50.000	73.94	23.62	.2343	14.41	18.13	79.41	21 89	25	142
52.000	75.62	30.96	.2607	15.44	19.46	91.11	25.93	23	141.
54.000	77.17	31.75	+455.	15.11	19.57	B2 . 09	29.16		1-0
56.000	79.83	31.51	.1994	12.03	18.45	82 44	29 86	29	∤35.
58.000	78.39	31.65	.2741	11.21	51 15	82 31	30.62	07	121.
60.000	75.9 5	33.96	.3312	8.65	24.06	8C.70	32.33	.01	97
62.000	73.71	31.37	.3101	3.57	28.78	79.15	31.26	35	40. 39.
6+.000	72.26	29.19	.5334	9.03	22.48	75. 79	30.06	43	39. 38.
66.000	69.4 6	30.01	.4224	6.65	23.29	73 37	30 26	3 <i>2</i> 39	36.
68.000	69.20	31.20	.2920	4.05	25.52	73.75	31.19	06	36. 34.
70.000	68.55	32.93	.3178	1.09	25.67	73.32	32.34	6	٦٩.

TABLE I-13. WIND STATISTICAL PARAMETERS

ANNUAL

STATION .	723930	VANDEN	BORG AFB						
Z	MEAN U	5.0. U	R(U,V)	HEAN V	5.D. V	MEAN HS	S.D. NG	SKEH HS	NOB5
KM	M/S	M/S		H/S	M/S	M/S	M/S		
- 100	1.47	2.60	5816	-1.53	2.90	3.57	2.64	1.04	9452.
1.000	.63	3.60	1568	-2.41	5.77	6.11	3.89	1.11	9890.
2.000	1.56	4.75	1587	-1.99	6.62	7.18	4.60	1.01	10225.
3 COO	3.65	6.31	1216	-1.77	7.75	9.03	5.9:	1.08	10236.
4.000	5.60	7.94	0826	-1.66	8.93	11.12	7.38	1.07	10251.
5.000	7.34	9.40	0205	-1.46	9.97	13.00	8.64	1.06	10262.
6.000	8.98	10.74	.0299	-1.40	11.21	15.01	9.92	1.03	10245.
7.000	10.62	11.97	.0758	-1.43	12.59	17.13	11.09	1.01	10230.
8.000	12.20	13.15	.1103	-1.38	13.85	19.22	12.10	.95	10191.
9 000	13.84	14.17	. 1570	-1.22	15.01	21.36	12.87	.87	10140.
10.000	15.61	14.97	.1737 .1701	-1.00	15.83	23.24	13.39	.80	10107.
11.000 12.000	17.24 18.53	15.13 14.54	.1538	58 .09	15.96 15.12	24.54	13.26	83. 33.	10016. 9954.
13.000	18.56	12.93	.1238	.83	13.12	24.91 23.74	12.77 11.38	.57	9934.
19.000	17.30	11.22	.0982	1.15	11.47	21.44	9.94	.53	99G3.
15.000	14.94	9.63	.0932	.96	9.47	18.27	8.53	.53	9904.
15.000	15.01	8.5≥	.0077	.61	7.64	14.80	7.53	.62	9725.
17.000	9.02	7.74	0:95	. 14	6.11	11.64	6.56	.72	9429.
18.000	5.94	7.16	0385	23	4.87	8.98	5.45	1.04	9-39.
19.000	3.22	6.71	0529	55	3.94	7.24	4.34	1.19	9344.
20.000	1.14	6.44	0648	-,76	3.37	6.42	3.67	1.82	92+0.
21.000	51	6.51	0936	91	3.09	6.32	3.61	1.03	e370.
22.600	-1.52	6.82	0651	-1.05	2.93	6.69	3.74	.95	8851
23.000	-2.29	7.32	0165	-1.02	2.76	7.16	4.03	.84	8703.
24.000	-2.74	8.05	5750.	95	2.89	7.80	4.55	. 75	8670.
25.000	-2.76	8.93	.0691	85	2.94	8.47	4.27	. 90	8616
26.000	~2.55	9.98	.1212	78	3.09	9.26	5.54	. 87	8→20.
27.000	-2.12	11.25	.1632	68	3.35	10.23	6.17	.93	7726.
28.000	-1.05	12.58	8+05.	66	3.70	11.33	6.73	1.09	€855.
29.000	35	14.00	.2279	58	4.04	12.53	7.38	1.25	6200.
30.000	. 75	15.44	.2476	56	4.40	13.76	8.33	1.33	5953.
32 . 000	1.86	18.75	.20 +9	.77	5.00	16.64	10.20	.92	1682.
34.000	4.47	21.73	.2626	1.23	5.77	19.58	12.00	. 91	1684.
36.000	6.61	24.96	. 3443	1.02	6.32	82.68	14.02	. ד ד.	1693.
38.000	8.03	28.50	.3100	. 56	7.03	25.82	16.14	. 74	1703.
40.000	8.58	31.46	.2589	. 18	7.71	28.56	17.54	. 66	1707.
42 000	9.54	34.29	.2551	1.04	8.87	31.30	18.69	.57	1706.
44.000	9.19	37.49	. 24 32	2.89	10.00	34 . 70	19.87	.52	1706.
46.000	10.68	40.70	.2515	5.12	11.07	38.16	21.53	. 59	1704.
48.000	12.13	43.40	.2847	6.76	11.40	40.97	22.97	.61	1700.
50.000	12.84	45.55	2762	7.74	12.09	43.12	24.24	. 64	1689.
52.000 54.000	13.80	46.84 48.28	.2730	8.05	12.34	44.38	25.15	.61	1660.
56.000	14.58		.2859	9.04	12.46	45.88	25.75	.63	1611.
58.00 0	15.49 17.08	50.13 50.98	.26 36 .265 6	7.58 6.51	12.52 13.80	47.73 48.98	26.27 26.94	.51 49	1540. 1357.
60.000	18.00	51.93	.2553	5.53	15.53	50.18	27.87	.50	980.
62.000	15.99	54.20	.1856	5.68	16.00	51.61	29.66	. 36	664.
64.000	18.00	53.88	.1534	5.86	15.03	50.85	30.10	.53	558.
66.000	20.32	52.06	.0449	4,29	16.46	49.69	30.80	. 64	540.
68.000	20.92	49.61	0077	2.54	17.25	47.22	31.20	.64	526.
70.000	21.34	45.89	0695	. 33	17.70	44.62	29.8	.77	503.
	21.34	43.03	.0033			77.UL	£ 3.0	• • •	505.

TABLE II-1. THERMODYNAMIC STATISTICAL PARAMETERS

JANUARY

0 SBON		Š	8 97.	B	.	8	88	86	.883	883.	. 689	88	978	2 (2		9	955	832.	827.	. 208	785.	630.	613.	606	, ,	1. 1.	703.	. 60.5	, a	473.	77	150.	150.	150.		.001	149	149.	64		146.	145.	123.	91	93.	. 4	•	ž s ř	
M085 1	ļ		967			-68	. . .	•6	883.	683.	880	880	878	67.00 67.00	10 10 10 10 10 10 10 10 10 10 10 10 10	8	20	935	8 27.	805.	, 18	630.	615.	606.	, ,	14 14	703.	. 20 m		473.	146.	. 151	. 121	<u> </u>		6	145.	1 2 2 1 .	147.	.50	47	143.	Ķ.	93.	53.	, ,	ا و	ŻŔ	
d SBCN	į		. 867.	8 8	ž	8	1984.	88.	8 83.	883.	. 880	. 880	979.	9/0	, , , ,	958	855.	832.	B 27.	80S.	6	630.	615.	606 .		. 176	703.			473.	145.	150.	150.	150.	. 50	150.	6,1	149.	148.		146.	Ş	123.	6	53.	47.	· •		
SKEH D	i	Ý,	55,	9 4	1.51	8.	15.	£	χ. Έ	76	-1.53	6.1-	R:	·	: X	K	23.	نع	ĸ	Ę	نع	9.	<u>.</u>	2	5. 5.	<u>.</u>	9	, , ,	S	9	8	88	39	ŗ.	5.	· *	-1.02	-1.09	82	66.	57.	50	m ;	60.	25	, (07	B 9	
5.0.0	6/ M3	22.6600	21.4500	16.4400	11.0700	8.2560	6.9630	5.3010	5.4340	5.3150	6.0530	7.9033	10.5800	20/0.21	26.40	6.8520	5.8190	4.7190	3.5850	2.5090	1.7930	1.3190	9858	.7726	90.9	1155.	8 10 2	25/2	100	4160	4154	.3328	1775.	. 2000	1353	1260	0769	.0585	4080.	6440	.0356	0630	6520.	.0173	7110.	7000 ·	6000	6400.	
HE AND	C, M3	2.e. rcca	229.0000	0000	901,5000	812.3565	732000	653,9000	593,2000	532.6000	475.8000	422. F300	372.000	300.4000	236 5000	203.4000	174.6000	149.4000	126.9000	107.4000	90. E200	76.E100	65, 1150	55.6800	46.9300	39.9700	36.5300	24.5000	2003	17.9760	13, 5200	9.5370	7.0270	5.2080	3. E8 /0	2.1970	1.6620	1.7090	1.0270	.6051	. FeE	€ 33×.	9	0683	3 615.	1595	300	(867).	
SKEH T		_	_			_	_	_	_	_	_					_	_	_	_				_					_					_					_		_		_		_		_		5 20 20	
5.D. T	X (4.67	Х (-	i i i	8	9. '4	£.	4.73	4.67	15. 3.	9	3.76	# W	n 4	; ;	16.5	4.16	4.22	4.07	3.68	3.5	3.49	N M	đ.	ZX I	24 (m)		R <u>\$</u>	; F	98 1 M	5.67	6.79	8.53	10.01	5 5 6 7	1 10	8.93	13.1	6.40	e K	5.53	6.48	6.43 C4.3	5 27	6 }.⊖:	11.03	£ :	9 KO	
FEAN 1	20 20 31 31	284.73	24.33	78.5	7. W	54.75	260.73	53.7	245.22	239.53	630.83	223.63	S : 2	010.10	23.5	211.62	209.52	208.47	208.43	209.4 6	210.71	212.39	213.41	3.	215.67	216.91	20 c	250.00	222.11	223.83	230.35	235.52	240.68	26.15	<u>6</u> %	25.97	¥.032	255.70	262.73	23.83	53.53	25.33	753.57	= Ñ	2.5.33	S	53. 63	88.7.22 88.2.23	
VANOENBERG AFB D. P. SKEH P.	į	17	7	Ž č	3	64.	50	8	55	53	, ,	en :	· .	y =	2 0	2	55.	.23	.07	.03	ão.	05	<u> </u>		8. 8.	ĸ.	5 (ה ה ה		61.	.31	ů.	61.	X,	 	27.	- 69	53	љ. Т	53	33	- 05		83	æ,	3 . 1	ල වි.	£8	
VANDEN S.D. P	P	点	9 (B)	1,10.1	5,9265	6.4647	6.8535	7.0749	7.0283	6.9833	6.74	6.3052	 	4.7300	3 0097	2,3450	1.8014	1.3620	1.0140	8000	.6701	.5933	.5581	5250	+82+ ·	4655	4300	5005.	2	Ŕ	5.67	.1536	. 1253	. 1065	4000	52.0.	. 3636	.0529	8£ 3.	.0353	£ 120 ·	. 0216	.0166	.0133	3 600.	7,00	5700.	. 003+	
* 723930	œ	C18.9000	ECS. 7000	304.3100 900 9300	707.95.00	623.3300	548.4700	480,7100	419.3200	354.5300	315.5+00	271.4700	2X . 7500	199.9000	144,0900	123.4700	105.1000	89.3350	75.9040	64.5320	54.9170	46. 75.CO	39.8800	34.0390	23.0970	6633	61.5350	15.63.51	13,4250	11.平60	6.5361	6.4435	4.8523	3.6753	1 0 1 0 1 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0	1.6538	1.2857	9398	. 7753	5935	6134	5500	13	.2083	7.10	5 911.	000	5.5 5.6 6.6	
STATION .								6.039	7.000	8.003	000.6																																					70 036	

TABLE II-2. THERMODYNAMIC STATISTICAL PARAMETERS

FEBRUARY

86 86 98	763.	Ë.	ě	ě	ě	£ 5	6	2 8	ē	780	779.	11.	772.	767	759.	ė Pi	į			, K	9	1	59	.099	ż	634.	5	044	. 650			· ·	162.	142.	142.		<u>;</u>	9			. 0			Š	, <u>1</u>		ñ	Ŕ
NO85 1	763.	Ė.	Ę.	Ę.	ď.	783.	793.	784	187	780	. 6	.t.	772.	767.	5.	Ė	į	?		5 K	Ş	2	\$63	999	044	6.34		دون	, ,	- e	1	9	147.	9,1	146.		٠ <u>٠</u>	<u>.</u>		ý	<u> </u>		8	\$,	F	2	તં
NOBS P	763.	Ė.	784.	₹	, 6	783.	, 60.	763	781	760.	779.	.626	772.	767.	759.	1	į,		, , , , , , , , , , , , , , , , , , ,		8	ž	563.	.099	644.	6 %	ž,	0 7 3	.024	c		-	3	142.	142.	2	- - - -			2	, <u>8</u>		£	3	S	įπ	, m	ĸĊ
SKEH D	. 18	.13	æ.	<u>e</u>	8	£.	? 6	52.	8	57.1-	1	-1.20	94	ج.	0.	= !	20.5		- 6		8	10	=	- 55	8 0 ·	₹.	.17	80.	۱ به	<u>.</u>	<u>,</u> 2	2 =	. 23	57	07	₹1.	F. 1	. 67	B (X .	, <u>.</u>	- 0	- 6	5 2	, E	9	8	Řį
S.D. 0	19.5800	18.3800	16.3500	13.0000	9.8 ⁴ 43	7.5220		1890	06.0	6.3330	8.5250	11.0000	12,1900	9.6253	7. 2330	6.3300	5.67.10	2000	5.0030	7697	3480	1.0130	.8082	64.28	5172	9034.	\$244.	6024.	3 696.	.3633	. 35 F	200	26	96,-	.1051	.0785	.0637	6950.		9650	58.5	8 - 0	515	5 5	0 E		1830	£620°
E SE	241.3300	228. "Jun	112.200	005.500	903.4.	813.9000	733, 7633	1000	532, 8000	475.7000	422.2030	371.1000	320,4030	273.3000	24.4000	201.9030	173.6030	148.5030	000.001	0001.00	76 7230	65, 0730	55.330	47,0000	39.9900	34.0230	20.9430	883 8	20 9000	17 9633	0000	05 K	5 2020	3.9030	2.95.10	S 25.30	ያ ረ	55.0	5.5	6 . 6	- 450	0.00	3 0 8 8	200	, r	₹ <u>20</u>	Q (3)	Ct 73
SKE.		_	_		_					_					_					_							_		_				_					_			_			_		ć &	_	
5.0. 1 DEG K	5.13	đ m	φ, •	4.73	n 3	R . 1	9) M	1	, m	3.83	7. 35	6.12	5. It	χ. 	ξή (10)	9.79	2.4	- F	7 6	5 5	. d	56.5	3.09	3.38	<u>₹</u>	3.16	87. ₹7.	ž M	£ (v.⊓ 38) () ()	; ≠0 - ac	6	60	7. 73	1.21	99	ر ا ا	R (7 6	6	ç ç	, , , ,	r a	6 6	(F)	6, 6
MEAN T	284.93	5.6 28.6	287.55	277.88	Si Si	表 8 心 8 形 8	8 S		247.53	230.00	222.38	217 47	215.42	215.60	214.58	212.49	210.43	\$18.1 \$		00.00	3 0	200	7.7.	215.47	216.62	517.88	P19 20	2.0 7	272.65	50 Y	3 2	8 E	() () ()	25.53	85 CK	80.53	₩ 1	۵ ا		F. 19		3 :	7 E	: <u>3</u>	: Z	7 5	98	55.0 49
VANCENDERG AFB D. P. SYEH P. B.	-1.07	61:1-	-1.08	85	ф.	ب ښ ا		9	. 71	63	87.	30	. IS	1. Of	00	3 :	= !	- ;		2 6		10	0	80	.33	ħ.	5	9∕.	53	62.	 	ָרָ מָּרָ בּי	8	10	12	- 28	1.27	€ €	S	90	ខ្លុ	,	P) k	្តិ	3 6	ر بر	a
VANDER S.D. P	7073. 1	60 K	4.4093	4.9:32	7.00 j	5, 20, 14 5, 17, 18	151.3.0 681.4.8	0.00		6.00	5.7664	5.1107	4.3359	3,5969	2.6773	2.35.40	. B008	- F	2007	0 6 F	5	53.7	5.64°	.4432	.4267	3965	. 57.3	3349	396	2673	יים איניים. מיניים ביים	177	. 1103	.3932	1.610	0630	 	5 0-0	£ 50.	မှ ငြ	0 3 3 5	3 6		i C	יים פיים פיים	4 F G C C	, , ,	. S. 35
* 723330 #[As. 0 #8	018,7000	CCE. FOOD	963, 8900	800.35.00	767.2330	60.3 0.03 1.03 1.03 1.03 1.03 1.03 1.03 1		418 0300	0090	314.0500	270.2100	231.5800	197.9300	163,0200	144 2500	123.0703	104 - 8300	96.1760	75.814C/	54 DOS	46 7000	39 8350	34.0000	29 0700	₹ .8663	21.2830	19 2183	15 6050	13, 350	3.38.5) (Q. Q. Q	9 6 6	¥ 707	6.8650	2.205.5	1.70-15	1, 37 CS	8028.T	P (6.3	,	9 <u>9</u>	9			1060 1060	600	250°
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TABLE II-3. THERMODYNAMIC STATISTICAL PARAMETERS

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O M3XS	.13	\$ 1.	31	55.	وي	8 9	P 2	9	, K	-1.87	-1.63	-1.16	39	OF.	ij.;	<u>v</u> :	- 1	. r	<u>;</u> =	20	3	17	6	23	13	13	<u>*</u>	20.	8.8	G	- 0	, m	£.	64.	.5.	75.	Ş. ;	, 0	55	02	18	٠. ١٢	₩	53.	Ŧ.	.82	95	.43
S.D. 0	18.1000	17.1400	18.3800	15.2400	11.0500	61.44.50	5500	0826.3	5.1440	6.4930	9.7080	11.0-00	12.4600	0.4:00	7.6180	5. 7083 1. 1369	7.7500	0.735.0	25.0	0245	1.1490	¥168	7169.	. F35	.4616	6 61₹.	.3741	- A	.3669	*CDC.	79197	21.26	.1536	2 <u>5</u> 2.	5501.	9360.	9690.	, C. 1	1750.	.0305	6520	2610.	6710.	.0106	7400	1 500.	7800.	9,00.
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EAN FOR	. B.	\$. Æ	292.61	8.7.	17.575	e s	3 : N	25.27	17.75	230.23	223.23	217.93	215.38	215.38	3.6	5 K	ם מ	7	2 - 2	201.97	213.06	214.45	215.68	216.98	219.36	219.71	221.43	223.23	ς, ξ. ξ.	100 m	238.74	民	20.17	s C	253. 10	262.9 4	194.73 184.73	8 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	6.75	25.38	381.81	250.83	150.21	3 S	26.63	€ ₹	532 49	255 85
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v, z	7	-	-	-	• •		•	_	_	•	•	•	-	•	•																																9400.	
* 723330 # ** P	1017.5000	005.7000	902.9200	193.4300	706.5200	5500	0000.75	17.7830	363.0:00	313.6800	27C. 1200	231.5700	197.9500	169.0400	144.5530	163.1000	2012.00	75.00.0	64.7.20	55.1250	46.9720	40.0840	34.2.80	29.3000	25.0360	21.4930	18.4350	15.8320	20.50	0007	6.5382	5.0187	3.6178	2 .9:63	2 K. V.	36.27.	1.55 to	B074	57.50	1954	. 3759	8368		56.31.	.128•	9360·	.5.0.	¥840.
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TABLE 11-4. THERMODYNAMIC STATISTICAL PARAMETERS

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N 280 T	839	8	931.	X	Sign	Ω χ		831.	8 29	96 98	93 93	956	99	822.	6	D a	793.	793.	8	776.	. 49	63	83	597.	719.	712.	اما	Ŗ.	0		ĸ	Ķ	<u>5</u>	Ē	ė į	2		121	123.	į	<u>5</u>	110.	ć	ñ			ξĦ
8 090	803.	8	831.	X	X X	i B	930.	831.	828	35B.	8 28	B26.	956	556	5		733	793.	782.	776.	634.	8	8	697.	719.	712.	, 60	6		. 021	122.	122.	123.	ž.	į į			103	123.	120.		103.	6	9	gi £	S	30.
O M3X5	5 .	08	22	8.	50.0	ķ 9	8	- 18	-1.19	3.	-2.04	-1.61	8 5	80.	- 6		, C	3	Ç.	90.	35	.	.67	ĸ.	g	60	98.	65.	2.0	S F	ķ	8.	61.	8	7	0.0	3 6		60.	5.5	37	=;	.65	£9.	8. <u>-</u>	. 4	3 5
S.O. D	16.9200	16.0800	CC13.61	16.1503	0009.21	7 7810	6.0510	4. B1 30	5.3~30	6 55.3	8.3220	9.90%	11.1900	9.9350	0.65.0	0.550	3.2960	2.5130	1.7790	1.3090	0.00	.682	6895	.5303	4714		. 3733	\$5.5E.	5.5.5 5.5.00 5.5.00	2	1.00 1.00 1.00 1.00	.2293	.1538	5021.	*450 .	66/0) P	0348	30 E O	(A)	ტიკე.	¥910.	₹.0.	9650	0800.		3
O NY D	239.000	226.0300	109.0000	999.0000	839000	730.2000	658,000	591,4000	530,4000	474.0000	421.2300	371.3000	323.1000	275.3300	201.000	17 2 2000	147.9200	125.8000	106.9000	90.85.00	77.0500	65.4300	55.6303	47.2330	40.2300	34 3100	29.7.23	20,00	10,320	13.50	9.8283	03:M	0.4810	4.1130	3.100	0100	0.1	0.50	26	9.9	8.5	≥9: 9 .	£.1	S.	• 181. • 181.	22.	0000
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r N C C C C	16 , 18 ,	3	a. ₹	75 8:2	2 K	2 X	65	3	5.1.16	231 28	9	2.9.5	214.73	614.53	, c	81.010	211.70	212.03	212.73	213.57	214.65	216.04	217.48	218.67	6-0.17	£61. 83	62.3.83	27.72	200 01	5 y y y	7 8	26 57	7.0.P.	<u>بر</u> این	86 : 68 (6)	2 K	6.6	500	200	昭 らわ	ァ ~ %	37.72	82,53	ម សូរូ សូរូ	الم الم الم الم الم الم الم الم الم الم	o 5	9: o:2
d Mark Buy Cadders	8	36	G O ;	8		90	-1.99	-1.05	5 -1-	16	57	6,	15.	50.	<u> </u>	÷ %	5.5	Z,	.21	.23	ď.	55.	91.	61.		.17	6	Ξ:	- 5	97.	02	19	30	#. i	1.5.	7.1	21.1	60	9.	£0.	13.	,	Ŧ,	M I	<u> </u>) y	<u>.</u>
S 0 P	3 C 3	5.7.53	3 .0.6 .	53.7° 20.8° 10.8°	- C	, 6 , 6	(C.2)	6.33%	6 11.82	5 6 97	ر ا ا	٠, ٢	3.6633	6.8157 6.00	C. 1030	S & S	9.20	64.7	SCH3:	1.65	5043	.4535	.4182	93 M	. 3739	3.82	1001	Ę,	6.4	25.23	1969	. 1513	16.18	\$600 1	ر بر د د	0 40 0 10 10 10) (C)	0334	%	0.00	.0165	23:0	£ 5	5000 6400	6903.		9200
- 7229.T	550, 615	505 3000	505 F250	779.4430	20 de 60	5000 LT	00 c6 00 00 00 00 00 00 00 00 00 00 00 00 00	418.7303	32 € 1700	315 1900	571.40.0	2 X2 . E 3 C D	60 0300	0000	0000	00% 4500	89 8333	76.5370	65.230	55.6370	47,4880	40.572C	3- 7070	3 2 £820	SS-4523	21.04.53	18	15.1763	13.93/0	E 3 40 . 6	6 8 7	5.1778	J. 9-76	67/30 E	1586.7	7 G	9000	2	Ş	C3:2:	100 3	35.35	2 29 5	1738	X :) () () () () () () () () () (1000 1000
27A780N +	51 555	11 001	000	0000		000	6000 9	7,000	000 8	000 6								ğ	000	000	000	8	8	8	20	8	200	0 0	3 6	8	900	000	000	000	3 6	2 5		000	8	000	003	000	8	800	14.000 16.000	5	000

TABLE II-5. THERMODYNAMIC STATISTICAL PARAMETERS

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Q 580N	626	.080	988	980	66			88	8		86	8	8	5/8	9 4 6 .	É	8	9	83. 83.	æ	. 779	. 299	ŝ	9	Y		. 613	3	5	- 	146		9	7	· •	, in	166	· * * * * * * * * * * * * * * * * * * *	143.	• •	130.	<i>;</i> ;	. 10	វិ	9 9 1		٠,	,
M085 1	.628	.088	889 89	. 660	.068	2 8	8 8	986	В	.683	. 188	86	98 1	8 75 9.75	o y	. 2	X B	ž.	8. 19.	99	677	86	651.	\$	20 1	Ė	. Q. Z.			6,7	150.	150.	<u>3</u>			8	139	Ķ	<u> </u>	139.	<u>N</u>	15.	& &	ጜ	ğ. 1	<u>ښ</u> ا	ri R	,
4 S80N	859.	.088	. 688	. 690	980	. 000	. 688	.888	88•	683	88	8	. 686	9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9	, d	, d	, X	9.5	934.	85 8	677.	962	651.	90	. 66.	, ()	61.61		2	145.	146.	146.		· ·		, T		45.		<u>.</u>	. 30	<u>;</u>	. 60	M	90.	57.	Š. 1	,
SKEW D	51	3	8	89 (3-	69.	ë t	. 0.	38	73	8	-2.80	-2.28	64.1-	<u>ڊ</u> ڊ		2	8	2	<u>5</u>	60	£.	23	8.	R.	33	ė:	0.0	3 6	90	8	61.	.26	.85	e c	5 5	9	S.	20	.53	ď	90.	ē. 9	.07	Ę,	. 60	3	1.07	0.
S.D. D	15.3900	14.6600	21.6100	15.8500	11.4800	6.6470	5,5670	4.7483	4.2090	4.4720	5.7820	7.4220	8850	9,50	2.50.7	2 2 2	3.7250	2.9270	2.0350	1.5410	1.1660	8348	.7096	288	74.	7914	19787	7997	5775	2012	. 1672	. 1453	.1295	#850.	. 4.0	82.40	0332	1620.	4+50.	.0189	.0157	6210.	.0108	,6 000.	9930.	750D	100	6000.
MTAN 0	233.0000	219,0000	0000 160	982.500	B8B. 2000	324 3C00	653.9000	589 1000	529, 7000	474.6000	423,3000	374.9000	368.4000	28.5.600 35000	275 5000	176 BOOD	150.9000	128.3000	108.9000	92.3000	78.2930	66.4400	55,4300	47.9200	00-10-0-	000B. #5	2000 K	0000	18 5900	13 6900	10.1100	7 5250	ა გ	4.2180	1000	1.8760	1.4533	1.11.00	8.J.C8	.7050	e B	1883	3372	65.9	.2051	1091	5551.	200
SKEH T																																													ત્રું ધ			
5.0.₹ 0.00 7.00	3.43	3.33	9.	λ.	Б .	, ñ	61.4	97	3.97	3.53	3 . 10	£. 5	# } •• .	8 9	9 K		3.23	88	44.5	2.13	S. 62	€.00	8 8	₹ ~	 	e :	יי קיים מיים	e g	, c	i m	T M	3.61	5 •	R :	2 \$	F. 17	7	. ₹ . ₹	Sh. r	£,	5.28	5.12	₩ ₩	6.51	7.05	P 55		<u>5</u>
HE AN	285.81	285. SP	287 53	3 1	5 F	0/ 1/V	259.12	250.50	% ≥.76	225.01	227.46	220.69	615.38	9 9	יים ה קיים ה קיים ה	36.	21.39	211.76	212.62	213.90	215.31	216.88	218.61	220.35	222.15	26.5	255.58 27.58	בייייייייייייייייייייייייייייייייייייי	23.40	237.27	₹.5. %	3 8.38	125 32 125 33	5.55 5.53 5.53 5.53 5.53 5.53 5.53 5.53	8 8 8 8 8 8	270.98	3	571.75	84 632	266 BT	86. E.S.	ان ا	K F	99. K	ው ! !	03 EE/	6. S	2. S. C.
YANDENBERG AFB S.O. P SYEH P MB	90	10	7.57	ر در ا	ب ب ب	60.	-1.05	-1.05	-1.08	-1.05	- 181	B	9 ! !		5 6) E	6	50.	. <u></u>	61	.0≥	.03	.03	. 25	9 !	S !	n -	==	0.7	3	.38	, 5	.63	ው <u>የ</u>	9 0	3 8	, S.	. 15	.13	.13	.13	. C3	.33	.93	છ.	66	F	F C . 1
VANDENI S.D. P	2.8820	€.81:8	€6-83 1	3.4.582	0.000	, r	5.4713	5.5259	5.5874	5.4271	5.1895	4.6349	7 (0.7)	6. 5! C4	7. Car	1.6745	1.3131	1.0582	6408	7.9	.6037	88	9694	6033	E365 .	200	3546	36	. E	3751	. 1239	6501.	.083 3	0170.		5:50.	.0311	0320.	+120.	.0178	.0153	2.5 10.	.0097	CB00	7+00.	5,05	5033	0. 1.
• 723933 HEAN P	015.3000	003.600	905.0100	900.500	708.3900 2001.300	51.6400	484.5500	423.6100	359.1400	320.1300	27. 35.30	4700	503.1700	110.4000	126 000	107.4500	91.5110	77.9-00	66.4300	56.66.50	48.3930	41.3840	35.4090	30.3120	6. 6. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8.	06/5/00	14.03.00 14.03.00 15.03.00	14. 4030	12.3520	9.3171	7.9276	5.3323	£.0732	5.1.33		7.5	1.1330	5638	.6939	- 3.	.4183	7 i	į,	. 183	0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	. 1073	5 (a)	0000
STATION .	1 000	1001.	1.000	000.	90 G		600.00	7.600	000.8	ກິດດ 6	000.01	500.11	14.600																																660.49			

TABLE 11-6. THERMODYNAMIC STATISTICAL PARAMETERS

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!	NO85	,	8	Ę	£		2	86	96	9	9 8	, 98	786.	186		. 181	.98	Ë	, Z.	. 772	9	, 6	2	738	\$	B.	533.	#0	633.	693	696	303	9	į į			162.	162.	121.		109.	20	99	9Š 1	Ġ Į	ġ)	e ş	Š F	××	éĸ	À	Ŕ
1	4 S	ř	8	5	6	790.	20		790.	7863	78 8	7 68 9	98	786.	587	791.	778.	.177	Ė	772.	, 9,	ę,	ž.	738.	374.	538	533.	280	633	683.	569.	509.	. 68	. 67	9 2		6	117.	117.	115.	116.	113.	- - - -	2	ġ.					i d		6
1	SKE D	3	9.	.63	ָּאָ	۲.	9	.33	.23	£0.	- 16	92	-, 53	-1.61	-2.00	-1.58	æ	Ž.	09	15	08	21		٠. 2	- , 09	03	20.	25	- 18	18	12	08		80.	9 8	5 5	, M	0₹	20.	£0.	03	- 12	80°-	ις 1	đ, ;	- 1	ž ė	,	· ·	8 _. a	<u> </u>	8
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7.7	<u>-</u> သဲ ရှာ	ָרָרְיָהָ ערייַשׁ	, (i	و رو د د د	ا بر ا بر	300 m	5 (C)	£6.	5(32)	S	£, 701.4	€ 300. •	1878	4.5110	9,50	3.7376	3.25.37	≥.6e∂3	2.08+5	1.5333	1.2072	15.6	901	₹ 8	BE 1.2.	6115	535	9 813.	3	: 3 463	3,39	3.1.35	<u>0</u>	٠ پر	0.57		67.0	. 870.	6 +30.	.05.23	15.6°	5.30	.C. 37	ම ද	0203	63 17 7	0010	7. S.	۽ ڇ ا		- C	. 0038
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TABLE IF7, THERMODYNAMIC STATISTICAL PARAMETERS

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S.D. D	13,7500	12.8000	14.1500	5.8350	5.0350	4,7150	4.1230	3.5560	3.2310	3.0170	2 8580	7.9050	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9830	4.7293	3.9730	2.8703	1.9890	1.3600	1.0530	8028.	5530	0 0	0.60±	5 47F	3165	.2929	.2655	. 2369	.2333	<u>S</u>	1051.	5480.	C703	7H .	.0473	.0375	0110	65.20	9 15	0010	2012	1 F	5.5	7 600	6200.	£400°
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- 723933 #FAN P	1.5,0000	0000.	903.1000	714.5300	533.2700	559,7800	55.5.50	•33.1000	579.0700	530.2700	385, 7233	77.750	100 4100	153,6500	132.5100	112.3000	98.233	80.9030	68.8310	58.7110	50.1750	#C.9030	30.70CU	51.0550	24.7.20	20.0750	17.2350	14.9230	12.9347	040E	7.5157 F F 737	F. 2159	3.2271	2.4860	1,9237	1.4320	1.1539	0808.	020/	0.40	1015	C	1.31	1363	1327	S. 158	£830°
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TABLE II-8, THERMODYNAMIC STATISTICAL PARAMETERS

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S.D. D	6/H3	13.6700	16.700	16.1400	0000	0.020	0,70	9	3.6020	3.3770	3.1480	3.0530	8 m	3.7000	7900	0630.6	006.0	0065	3.0000	0000	0300	22.5	5573	5335	0634.	006E.	.3430	3.9	.2786	٠. ا	6922.	3. 3.	5133	B(21.	2 843	1953	.0583	976	£ 7£ 0 .	1750.	1550.	0.550	.0163	50 C	* ! = !	CO:0:	7 NO. 6	2 05.22	6,00.
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F AN 1	x o o	£ 66.2	, p	33.69 1	S :	71.055	16.116	502.5	8. 8. 8. 8.	86.50 198	3.62	235.99	68.822	* .%	216.57	2	1 3 2	E (2)	700.00c	563.53		10 Y C	ξ. α.	219.76	3 .1.55	223.05	35 .22	87.6.33	98::22	529 33	233.98	275.80	233.12	2 C	X 5	8	بر در	あ だ	36. 31 36. 31	57. 12	90.36	S	S	EC 1	is Ž	ر د.			213.56
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• 723933 ME44 P	2	014.400	BC64. ₹00B	962.25.0	00761 5080	774.35.00	100 F 000	493.1200	437. 7CO	378.7000	323.9230	265,4500	23.53CD	212.7500	182.250	155.550	00%	112.000		02.00.03	1 2 2	30 75 BC	01.10	36 77.93	31.5390	27.0910	23.2510	60.000	17.2520	14, 86-60	12.8-83	9.6593	25.5	3. 4836 3. 4836 3. 4836		7. 4.	1.8950	1,4613	1.1339	.8737	₹.99°	66.5	£9.	ن را ا ا	8232	1.87	٠ • • •	130	3 S
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TABLE II-9, THERMODYNAMIN STATISTICAL PARAMETERS

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	NOBS 1	ic P	818	Š.	783.	783.	783.	789.	781.	780.	7 8 0.	780.	.67			.577	.577	767.	765	.151	. 161	789.	Ę.	Š	591.	578.	57.	.151	714.	568	SIB.	.181	₩23.	8	8	100	.00	. 60	9 9	9 5	. 8	8	6	88	8	æ	63.	3	ä	Ŕ	Ř	Ŕ
	A Seon	4	9.69	779.	783.	783.	783.	78.	.181	783.	780.	780.	779.	Ļ	Į.	772.	772.	767.	762.	ئ ب	731.	789.	78.	S	591.	578.		721.	714	568.	513.	.1 0 1	+63	8	9. 86	97.	97.	6	÷ 6		n 8	į	8	83	86	76.	·	6,	33.	×	32.	89.
:	O MEM	2	.53	۲۶.	15.	.37	S	60.	9.	.03	- O.	. 58	-1.15	-1.28	-1.09	7	S.	₽.	08	95	94.1	5.16	5.16	2.19	٠.40	2.46	85	2.50	ر ای	2.28	2 .21	€.07	96 	સ્ટ્ર	1.12	8	π.	eč.	Zi 8	ē. 6	ē -			1.57	1.76	1.12	1.32	.68	00.	25	69	გე:
,	S.O. 0	17, 2700	16.0300	17.1500	10.7400	7.3230	6.3130	5.60+0	4.8370	4.1660	3.7520	3.7700	4.3380	5, 6890	5.3640	5.5310	5.3640	5.0690	4.4460	3.3690	3.3370	2.6080	2.0490	1.7970	1.5080	1.2760	1.1250	.8646	.7399	.6566	.5689	3:05.	8/ 77	65.¥3.	1999	.1789	5751.	9211.	C 183.	0.00	100	1550	.0273	.0235	6050.	5710.	S 10.	1,000.	6500.	6400	₹50.	.0032
	# 6 2	P 15, 0000	201.0000	039.600	965.4000	875.1000	7-33, 1000	716.8330	5: 7.5000	5/34 . 0000	5.25.1000	472.4030	422.5000	375, 7000	331.1000	230.000	252.5000	218.4000	187.2000	158.5000	134 . 1000	112.7000	99.9 9	90 3+00	69.0900	57.8200	49.1700	41.6800	35.7300	30.5500	36.1400	22.4000	19.2200	14.1200	10.4800	7,7510	5.7730	6.31.0	3.6350	3 6	201	0661	, A.	3	55.5	83.13.	E3.	Х. Ж	1927	583	.1157	.ca75
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1	5.0. T	8	3.72	۴.90	3.68	3.03	88 .88	£6 ~i	2.67	2.33	ار 93	2.93	85 73	3. %	3.03	رب 96	2.73	<u>د</u> 8	3.18	3.00	€.59	₹.12	.	9 8	3 3	7.50	- -	1.60	1.69	<u>Б</u> .	80∵2	2.21	Ж. ~	3.69	3.70	93	۳. ۳	Z :	Ξ ? •	7 3	5 8	3 8	N D	53	er er	6 35	7.57	<u>දී</u> ක	7.45	7.01	გ თ	7.5
1	F AN OFG K	283.8	208.97	233.36	ا ينزو	و. د.	276.63	29. 29.	33.7	356.50	¥8.8ĭ	D	233.67	2.6.83	221.03	2:6.08	71.115	S08 : 00	206.30	206.59	208.22	210.72	213.23	215 34	217.19	219.00	820.69	27.5.12	223.64	275.30	276.71	5 58. 6	553° 38	234 57	237.62	<u>ም</u> ፈ	ا ا ا	60.05	្ត បិ	S 9	61, 103 CF 438	3	265.33	353.33	3	R9.48	82.53	₹8.52	200 E	233.91	324.50	218.33
SCRC AFB	X CE	- 38	8.	16	ō: ·	64.1	9.	57	C8 -	38.	, 60.	85	73	57	. 45	P.	Ķ	60	05	06	ال الح	2.57	7.51	ر گ	2.55	2.13	2.05	20.0g	16.1	1.67	- - -	1.50	1.39	.79	.8 5	3 2.	65.	55.		ي د د د د	, t) <u>s</u>	1.22	1.15	1.10	1.09	8.	<u>c</u> .	80.	.05	90.	51.
VANDENS	ر ان ق	2.5885	2.5780	2.4482	2.5556	3.0364	3.2935	3.3851	3.5139	3.5334	3.5612	3.4557	3.444.5	3.2625	2.835	2.5851	2.1835	79.7	00++	1.1374	- 256 - 256	1.3780	1.1767	1.1027	5695	ф. Ж	.7390	. 5860	1215	.4693	9:24.	35,35	. ¥27	. 1879	BC31.	.1363	-1016 -	2363	27.1.	0 to 0	55	55.0	.0.87	. ი2⊶3	1020.	.0173	54:0	1600	8+00	6200.	¥60.	.0028
123930	1 2 2 2	013.6000	001.7000	901.8300	852.2300	712.1700	570.4200	556.5630	430.3400	-29.9100	375.6000	326.3300	283.4900	P**.6203	210.0700	179.6200	153.4500	130.5000	110 6200	9. P. 30	80.1170	68.15+0	58.0930	49,6550	42.4510	36.3510	31.1520	2E.7010	55.9.00	19,7550	17.6140	14.6630	12.65+0	9.4813	3	5.3715	4.0745	5. 10.34 3 40.1	200	# 2000 T	7 7 7	25.5	57.50	5173	3338	5602.	. 2355	1771.	£2.	6398	3,57	6453.
STATION	~ ₹	_	_																	000	000	000	000	000	000	000	000	000	cca	000	000	000	000	000	00	000	000	3 6	3 (200	8	000	900	000	000	000	000	000	000	000

TABLE II-10. THERMODYNAMIC STATISTICAL PARAMETERS

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	¥095	;	, 20	6	865.	98	928	6	6 6 6 8	963.	863.	28	3	198	8.e	8	928	957	Š	933	. 218	915	. 603	800	ፈ	<u>ج</u> آ-	610.	9	731.	717.		310	Z :	3 8	. 60	. 6	<u>8</u>	<u>.</u>	6	.10.	<u>8</u>	<u>2</u>	103	<u>.</u>	. 60	B	., .,		ች <u>!</u>	j p	1	લં ફ	
	2 000 3 000	,	9 9	į	965	9 26	865.	965.	965.	96.3	963.	1963	3	28	96 86	æ.	828	857.	26	953.	. 19	815	807.	.008	634.	<u>.</u>	610.	6.6	731.	717.	363	200	5	. f. 6		, ,	106.	106	107.	107.	105.	133.	- 25 -	.101	2	3 5 (. :	Ġ	ន់	ė t	h	કું <u>ક</u>	
,	0 1 1 3 5	ţ	5 0.	3.	<u>۾</u>	.83	.	š	ē	55.	- 15	05.1	-1.28	36.	-1.61	-1.13	9 2.	9 5.	£.	اج	5.₹	60	Ş	.	<u> </u>	ĸ.	Ķ	=	5	8	03	60	5		R 5	2 5	١,٠	6,	£,	X	8.	0.5°	8	9.	ō.'	<u> </u>	5.6	e e	و د ا	9 6	, ,	<u>,</u>	
	S.C. D	5 F & C	18.2705	17.1900	18.9100	13.6800	9.7033	7.6930	6.5340	5.5340	0-38°±	4,4570	38.5	6.1620	7.4130	7.7390	7.2380	6.3720	5.5150	*.6850	3.7230	2.7510	1.90+0	010-	1.0280	1116	6369	96 96 97	5116	80**	8 2.8	- 7 5 M.	. 3. 186	8062	ָרְיָּלְ קיילי	2.5	23	9721.	. 1069	S 80	3620	.0535	.0473	59.0	0820	E G	6320.	\$ B. D.	BC 10	z (6	8800.	8800°	*3::0
	0 KY 0	2000	ecc. 2000	25r c000	CC007 - 460	675, 1000	Par	199,6000	727.3000	656,4000	186.1000	525.1000	474.2000	423,0000	374.9000	3.5.2000	286.3000	247.8300	213 COCO	181 2000	155.7000	131.5000	110,7000	93.3300	76 J. 7.30	66 5200	56,5300	¥6.000	46.9400	9. A.00	25.8730	83 X	21.8300	16 . 7030	0.00	27.72		F. 1.3430	1,0383	5. <u>3</u> -10	- 25°5		<u>ن</u>	9 :	67.16	1631.	600	6,06	. 233.		~ .	1163	£\$87.
	- 3																																																	3. i			
,	7.0.7	1 (C) 4	∓	₫ m	κ M	ធ្លី •	10 •	3.67	3.83	r m	3.66	3.53	8 8	ج 99.	3.21	3 51	.¥.5	3 73	3 ? 3	٠. ت		8	2.45	S. 18	6.10	£: ∂	E1 2	7 , ℃	2.23	ři N	Ç) N	93 2	5.83	6.93	; ; ;	3 3		8	5, 35	36 5	رن در	ှင် က	6.13	<u>ء</u> ا ن	p v	- N	(Q) (\$ i	B. 31	J. !) :) :	5 6	a, L
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SCOUNT.	a ci (r	0 0 0	20	66	3.3134	3.6623	£. 1623	1. P. O.	6 20 3	4 9753	7. 50.55 7.	100 G	4.7842	4.5100	4.0617	3.4855	2.9555	S. 44 19	1.93:9	7.3	1,1979	92.36	7861	.67 37	<u>\$</u>	ያ ለ	すいたま	0 T S T	ج ا	88	<u>گر</u> بر	5,57	3 €	₽	K 1.7.	7	20,75	1087	1060.	17.0.	28	5	0 8	F7 0	3 C	Ϋ́,	, e	9 (5 (D 10.	7900°)))	9 4	* C - C - C - C - C - C - C - C - C - C
. 723530	1 7 1	20.0	(00, 410	C03: 3000	903.6300	BC2. +500	711. 500	6.8 .700	254.4200	487. C.300	F26. 7530	372.3300	23.350	273,523	0008 0 %	206.4500	176.4700	150.5500	128 0300	108.7530	98.3030	78.3530	66.6030	56.7050	₩8.33CD	£ 239	35.2930	30, 1763	00 to 100	22.2.80	0080. 61	16.5793	06017	14.1460	0 ¥) (4) (4) (6) (7	(P)	2.36.93	ار الم	1,753	1.756	0.55. 1.05.	6.6	50.7 10.7 10.7			2 1 7	5.1.1	7171	y ;	, c	. y	6.65
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TABLE II-11, THERMODYNAMIC STATISTICAL PARAMETERS

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MO85 P	aya	885.	60 7.	995.	935.	<u>.</u>	į į	i d	9	883	889.	989	93.	879.	0	9	2	d	2	615.	8	676.	99	9 2	763.	. 18	, 8 3		2 7	79.	. 18	8	£ 6	6 a	83.	83.	98	. 10	6. 9.	: 1	ė I	ý [, ,	Ŕ	ĸĊ	ż
O H3XS	9	27	=;	ř.	. ق	ř.		7 8	2	8.	-1.78	97.1.	96.		ζ.	2 6	3 -	- 1	80	. 05	30.	20	- 16	05	57.	ē, ā	5 0	50.1	50.	<u> </u>	00.	75.	7.	F (4)	68	8	.97	8	.87	<u>.</u>	ą.	Q .	9 A	21.	50.	£::-	15.
S.D. D	בריט במאק כל	19.0900	17,7500	14.3100	10.9600	8.5830	0000	5.450	2,560	5.9-60	7.2640	8.8080	9.7730	9.4320	OFFR.	0.000	6.63	0 S 7 F	2.3300	1 5980	1.1150	1198	₹ 39.	.5287	.4733	9,54	5815	13411	7967	.2330	.6268	5025	6181.	505	0863	9930	.0534	9940	.0374	.0317		- C) # () ()	8110	6000	1,00	59:20
HEAN D	מטיט פצפ	218.0000	039.000	990.8000	693.3000	805.5000 300.5000	700 / 700 P	589, 5000	529.4000	473.7000	421.9000	373.5000	327.5000	283.9030	200 3000	109.7000	7000	0000. 051	109,000	92.0800	77, 8000	65.8000	55.8100	47.3820	40.3100	3000 A	2000 A	2000 FG	18.2500	13,4000	9.8210	7.2260	5.3700	5 5 6 5 6 5 6 5 6 5 6 6 7 7	. ¥00 . ¥00	1.7020	1.3050	1.0103	3.6	.6121	5.7	955	בקייל. קיילי	1750	1351	\$0.	2080
SKEH 1																																															36
S.D. ↑	ر ع بر بر	60	5.08	8 6	& - -	5 Q	1 5	7	£ .07	3.67	8 7	3.53	t. 15	g 9	9 6	2 6	ų ų G	L4.	3 .00	58.	2.19	2.10	٠. <u>١</u> ٠	2.23	83 ! n. i	2.57 or	2 K	3 A	, n	3.83	4.12	5.33	ن اف	5 K	68	d .	5.72	6.63	J.	6.33	5.93 1	8 8 • •	() a	. T	61.11	13.19	66.61
MEAN T	26.25	236.45	285.90	291.49	75.47	70.07	7. 1.7	20.03	242.57	235.09	257.92	221.39	216.15	515.62	2 6	20.77	206.72	207.35	208.75	210.13	211.73	213.21	214.78	216.11	217.49	239.86	10.000	27	223.65	228.78	232.95	237.49	ያ ያ ፙ	7 9 7 1 7 1	69.75	34.156	85. 83.	% %	8	19. 19.	3 . 3 . 3 .	5 C	5 g	1 6	235.97	225.93	218.75
SKEH P	80 11	. 62	85	. 79	76	B 6	2 6	77	L	73	59	* * * * * * * * * * * * * * * * * * *	. 30	, ,	ĵ -		6	X.	=	. 18	۲	<u>.</u>	<u> </u>	i.	55.	<u> </u>	<u>.</u>	į	. <u>.</u>	67	ř,	Ę	æ 8		- 0.	8	. 79	Ŗ	ĵ,	E	કે દ			ě	99.	8	8
723930 VANDENBERG AFB FEAN P S.D. P SKEH P	f.0617	3.9072	3.9636	£ .4941	5.1935	7.707.0	, i	6.4010	6.233	6.0309	5.6511	5.0785	£. 2255	2 6	, co	7.47	1.3335	1.0562	.7736	.6351	5399	8354.	.4203	4712	5577	8 8	. 5. X	, i	25.70	.2071	. 1576	. 1352	.:157	(a)	3,50	0550	0+63	.0383	.5321	5 150.	0220	n M	51.0	000	£900.	1500	7400.
- 723930 HEAN P	017.700	005.6000	924.0300	801.F+C0	729.5300	500 F 500	484 2200	423,1900	358.5630	•	ru	N I	ru ·				•																														
STATION		_	_	_				7.000	_	9.000	10.030	11.000	12.000	200.51	200.41	16.00	17.000	18.000	000	8	000	60	8	8	င္ပင္ပင္ပ	3 8	3 6	8	8	99	88	000	8 6	23.00	000	000	8	8	88	3 5	3 6	3 5	900	600	CCC	000	000

TABLE II-12. THERMODYNAMIC STATISTICAL PARAMETERS

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N085 1	600	. 6.6	D. D.	ф о	ልዕ	ፈ	933.	931.	931.	S	ė y	ė	953.	i e	, ,	911.	208	938	. 198	5¥9.	823.	2 9	657.		, 100	733.	Ċ		8	P	130	Ķ	ĕ	<u>R</u>	<u>.</u>	<u> </u>	<u>R</u>	ž	Ł	123.	<u>e</u>	- 5	<u>e</u>	ኔ '	,	E i	X I	ત્રે જ
4 S80W	600	500	26	100 100 100 100 100 100 100 100 100 10	, <u>Z</u> 6	26	933.	931.	931.	ģ 8		e S	965.	5	917.	- 16	905.	96.8	198	9.	923.	674	657.	941	30	733.	Ċ	<u>.</u>		478	127.	7 .	Ķ	<u>K</u>	ĊX	<u> </u>	9 <u>0</u>	126.	Ŕ	ĸ.	<u> 2</u>	6.5	. 62.	,	9	χi	E	é xè
Q H36	۵	: 2	97	7	.	89.	5۲.	ĸ,	67.	÷.	 	 	. i		60.	03	Ξ.	.33	Ŗ	69.	8	64.	en S	r.	E.	91.	50	ē. () •	10	17	3	80.	ช้.	8	3 15) F	بک	92°.	60.	3 .	£0.	= :	;	<u>ر</u>	CE:	((7. S.
5.0.0	52.55	21.4800	18.5100	15.6900	11.9630	9.2443	7.2170	5.9803	5.3910	5.7350	0.00	60.4.60	10.6100	10.4500	8.3140	6.8740	5.8700	€.8593	3.7350	2.€.60	1.8300	1.3070	.9705	575C.	.5820	.4870	£ 5 4 4 .	282	800¥.	35.6	6.62	8,5%	. 2350	.2631	2291	0470	0.756	₹÷ 50.	6+60.	6540.	.0397	73.50	en e	ر د د د	.016.7	6110	6600.	20:0:
EAN D	0000	0000 553	10.000	993 (500)	900,000	910,4006	730.5000	158.4000	93: 5000	530.5500	0007.77	0000	07.3670	78 5000	38.900	205 2000	176.0000	150,2000	127.5000	C7.8CC3	91,2160	7.0800	65. 3000	55, 3300	£7, C820	40.0500	0050 · 3	29,0300	10.10.00	18 5620	13.3500	9 75.0	7 1850	5.2930	3.93.0	669	0,99	1.285.0	1 00:00	2 6.39	5,13	96 1	1515	(a) (a) (b) (b) (a) (b) (a) (b) (b) (b) (b) (b) (b) (b) (b) (b) (b	Luis	2 2	7. M	1 (5).
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FAN 7		5	283.21	61.812	273.83	268.15	38 (₹ 1	ણ ; એ ત	1	6. 5. 6. 6. 6. 6.))	2 t	21.0.10	213.83	212.55	210.67	258.91	₹08.8¥	208.21	71.602	210. ¥	211.36	213.10	216.43	215.67	216.82	218.03	2:9.01	22.12	252.33	27.75	232.13	236.41	3 ? 1	3 X	6	8	8	٠. ئ	2) 2)	元 (た)	B (6 6 6 7	6 6	5 ' 1, '	2 i	B (2)	68. 88 .
VAPOLNEDRO AFB D. P. SKEn P.	62.	9	. 60	57	7.	81	6 6 1	C5.		6			, ,	60	61.	. 23	ķ	9 .	.33	Ç2.	6 0.	97.	6 0.	.	17	61.	02.	80.	<u>.</u> ا ا	2 7	16	8	đ,	6	P	, 6) (1)	ξ.	61.	=	<u>.</u>	ë S	<u>ن</u> 2	8.	-	6.1	B (9 C
5.0. P		4.4.57	1.53.	5.0718	5.8692	6.4364	6.9753	7. CO.	7.25.7	5.55.7	ب بر د ر	0 0	0	3. E. S. C.	3 1317	2.4515	1.9199	1,4551	1,0973	8 7	6563	5698.	61:C	5094.	5619.	51	189	() : () :	# # # # # # # # # # # # # # # # # # #		C+15.	. 1812	1551	1921	5851.	Cie	<u>ئ</u> ئى	P.	EC-53.	0415	ex 80.	٠ ا	9 (P	5. 5.	<i>2</i> (5)	7.	N I	c #33
• 723333 # 44 P	18,3003	56.7503	C4. 1200	P3, 6003	0256,70	1000	48.9533	81.2750	20 6159	155 3700 46 Write	0.00.00	0000	0031	73.8100	45.5603	C010.	05.4700	89.62:0	76.1350	F. 7110	55.0540	NE BANG	23	620 A	29.1440	5.83 2.83 3.83 3.83 3.83 3.83 3.83 3.83 3	61.55*0		13.50	23.5	B.715.8	9239	X. 8.*	3.6743	106.7	6.0	たんこ	Çi Hê	Ē.	8	25	E 61	, A.	,	• ·	S.	M ()	(1) (1) (2) (3)
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TABLE II-13, THERMODYNAMIC STATISTICAL PARAMETERS

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+ 723930 VANCENBERG AFE MEAN P S.O. P SKEH	BERG AT	ω °.	F SAN T	5.0. 7.0. ⊤	SKEH 1	HEN D	S.D. D	SKEM D	WORS P	NOBS 1	NOWS O
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90 000 90 10.0 M	7 C. U.S.		.		_	00.00.00.00	20.3550	ų,	1990		
3.5335 cc. 1533.58	2 7 3 8		7.7			1641.0330	76.7300		10229		0000
4.252980 293.39	20.33		5.37			98*.2000	21.4900	71.	10246.	10246.	10246.
5.353180 277.97	277 97		ا برج		۳. ا	833.3000	15,7400	.33	10245.	10245.	1025
7 0361 1.77 265.36	\$ 8. 5 %		5 Y			523.0000	0208.11	Ŀ.	203.0	102-0	1020
7.5293	i Mi		3 2		_	F. 4. 37.03	7.430	¥ º	10220	. 62.63	16239
7.861969 25.93	K2.93		61.9			549,000	6.2550	. S.	10226.	10226.	10226.
8:0233 -:62 245.40	3.52		6.11			529,3000	5.2390	8	10210.	162:0.	10210.
7,9055 -,53 275,82	275.82		34 36			473,9000	5.4560	15.1-	10198.	10198.	10198.
7.832238 238.5-	₹.8.2 		ا ا			0004.524	6.7:30	-2.15	16130.	:0:33.	10190.
7.410422 222.16	22.2.16		in i		_	373.6000	B. £ 300	88 :	10162.	<u>3</u>	2910
20.7.10 ED. 10.00 M	ξ (2 : n :			227.123	10.500	-1.25	10148.	10148	10148
20.412 00. 1823.C	0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0) d		_	2000 - CO	0010	8 :	10105	10166	10106
איז ריט דו	מייינים		5 a			30.000	00000	u 9	0000	0000	
20.013			5 6			2000-00-	200	<u> </u>	0000	0000	0000
5/ 10 J 10	יי מיע פיים אלי					0000		<u>.</u>	9330	8 5	. 6150
2.1663 3.8 2.9 23	209 23		. C.			000000000000000000000000000000000000000	200.4	5 6	. 400	. 20	. 20
1.8377 .43 210.78	210.78		M .03			103.6000	3.2280		9591.	9591	9591
1.60% 43 612.38	612.38		æ ~			92,6500	2.4130	.17	9-87.	£83.	9×87.
1.4531 .43 214.07	214.07		2.91			78.4400	1.9610	82.	785	782	78.4
1.2725 348 215.56	215.56		ž, M			66.4300	1.5910	r,	7×09.	¥09.	7*09.
1.1438 .43 .58	21.7.08 		<u>ج</u> ۳			56 4:00	1.3440	ç	7295		7235
1.0140 .50 218.57	218.37		9. i			47.8930	1.1352	69.	7963.	00 to	7929
בין אבר גבר מביל	מיט פיט פיט פיט פיט פיט פיט פיט פיט פיט פ		χ. γ. γ. κ			30.60	0600.1	D :	9.76		8/10.
The second of th			e y		_	34.8500	80 m	, ,	100	1 d	40.00 10.00
73.033 GT	55 166 166		S X			300 / 60	(18 E	3, 2	, D4C/	7046	70.45
55.050 MI. B02.93	3 2) - 3			21.57.00	5878	; X	166		
5679 11 227.94	227.94		j			18 75.00	25.6	2 2	9769	5769	5769
, 4357 CB 233 ER	233 68		5.57			3.50.0	83	0	- COO-	1446.	1367.
35.00 .06 250.18	27%.18		6.02			10.01	46.34	= -		1453.	1402.
₹ 2 % ₩. 2£&.	きん		6,67			7.4:20	.3733	20	14:3.	1463.	1413.
89.7.45 00. 7525.	857.83 -		7.23		_	5 5:90	1565	• · 19	1421.	1.33.	1421.
. 1878 05 251.38	33°58		<u>.</u> .			4.1230	6222.	- 15	1+20.	1473.	1420.
16.852 - 21 88.31	16.9%		15.7			3.1016	22.	 	1420.	1473.	1420.
. 1205 16 263 57	263 57		<u>ಕ್ಷ</u> ಪ			≥. 1 5.30	B! 3 .	٠. ت	<u>-</u>	8,5	<u>.</u>
75.835 P 159 SEB. 27	. 256.27		6. 33			1.600C	67.1.	ý.	5	1419.	-
.0796 - 1.19 267. 32	827.78 - 1		ှင်း တ			1.3360	. 6933	£.	1.C2.	1,02.	1402.
.053320 255.95	86.55 28.55		6 6.3			1.3530	£.6.	- 23	1337.	1321.	. 397.
105년 - 119 전시기	25.35		9			3C - 19	.0543	3	1365.	13.8.	1365.
. G 16 25 6	9, 192		£ ;			339	64-3.	ī.	1336.	1,59.	1336.
-30 CK - 80 C - 20 CC	300		د ع			5.3	50√0.	75	1694	1330.	1283.
(19·10) 19·10	đ,		6			3.	8213.	7	17.0	1166.	1140
12 x 2	5.5		8			22.25	86.23	12	942	96	4
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TABLE III-1. MOISTURE RELATED STATISTICAL PARAMETERS

JANUARY

STATION	- 723330	VANOE	ANDRO AFB								
Z	VAPOR P	S.D. VP	SKEH VP	7.7	TV	SKEW TV	DEHPT T	\$.0. DPT	SKEH DPT	NOBS 1+P	NOBS TV
	MEAN			MEAN	5.0.		MEAN				
KM	MB	M9		DEG K	DEG K		DEG K	DEG K			
. C 20	9 6.36	7 144	.23	235.76	4.65	.01	278.86	5.08	-,49	854.	85.
.100	9.435	3.022	. 26	295.41	₩.68	.04	278.58	4.93	52	9 67.	867.
1.000	4.967	2.754	. 92	203. 67	5.19	.23	260.\$7	7.37	.08	877.	89• .
2.000	2 .929	2.003	1.19	276 . 93	5.23	32	261.00	8 36	. 16	871.	894.
3.000	1.802	1.385	1.60	273.62	4.99	73	254.78	8.45	. 2 2	8 52.	884.
4.000	1.126	.928	1.82	267.61	4.79	70	249.10	8.50	.21	860.	894.
5.000	.713	.604	1.72	260.93	4.81	~ .68	243.67	8.69	.03	862.	6 84 ·
6.000	.416	. 366	1.63	253.80	4.75	54	237.69	9.25	15	855.	894
7.000	.278	. 205	1.58	246.29	4.69	36	231.50	9.39	27	e55.	6 83.
8.000	. 127	. 104	1.36	238.62	4.53	25	236.45	8.81	56	680.	883.
9.000	, 084	.061	.68	230.90	4.21	09	18.55	6.90	~.8≷	149.	880.
10.000	. (73	.016	1.17	223.69	3,76	.23	213.51	5.97	-,43	18.	890.
11.000	39.399	99 .933	979.93	218.05	من . م	.70	330 33	99.93	939.99	5.	978
15.000	99.999	99.433	933.93	215.13	5,45	.46	993.39	99.99	999.99	4 ,	9 76.
13.000	99.999	99.939	939.39	214,43	5.46	19	933.99	99.99	999.99	1.	872.
1 → . 60 C	99.999	93.939	9 39.99	213.55	4.32	21	939.99	99.99	999.99	٥.	86 4 .
15.000	99 .939	9 9.933	939.99	211.52	3.97	05	993.93	99.93	933.99	٥.	858.
16.000	99.923	99 .993	939 99	209.52	4.16	04	939.99	99.99	999.99	٥.	6 55.
17.000	53 3 33	99.999	3 33 · 59	208.47	4.22	04	933.99	99.99	993.99	٥.	93 2.
18.000	63 933	99.339	9 ?9.99	208.43	4.07	18	933.93	99.99	999.99	٥.	B27.
19.000	99,999	99.999	939.9 9	203.46	3.68	31	999.99	95.99	993.99	0.	802.
20.000	99.¢∩9	99.993	923.39	210.71	3.51	41	939 93	99.39	333.58	0.	785
21.000	23 9 73	33.933	933.99	212.09	3.49	51	599.39	90.39	939.93	0.	630.
22.00 0	39. ong	93.939	929.99	213.41	3.52	40	999.99	99 99	939.99	0.	6!5.
23.000	93.333	93.933	333.33	214.54	3.54	48	933.29	99.39	933.93	0.	606
24.003	99.933	93,939	9 39.99	215.67	3.52	54	939.99	99.99	999.99	0.	714.
25.000	99.393	99.909	939.99	216.91	3.52	34	999.99	99.33	999.99	0.	714.
25.000	30.333	93.939	979.99	218.09	3.53	40	999.99	99.39	999.99	0.	703.
27.000	93.333	93.933	929.33	₹19.25	3.55	- , 2 9	993.99	99.99	999.99	D.	554.
26 000	9 9.9 99	99.993	979.99	2 ∂0.64	3.55	01	993.93	99.99	999.39	0.	500
23.000	99.333	93.539	939.33	555.11	3.77	.16	993.99	99.99	999.99	0.	483
30.000	99.333	33.399	973.39	223.83	3.96	.25	999.99	99.99	999.99	٥.	473.

TABLE III-2. MOISTURE RELATED STATISTICAL PARAMETERS
FEBRUARY

STATION	- 72 3930	VANDE	HEERS AFB								
Z	VAPOR P	5.D. VP	SKEH VP	IV	77	SKEH TY	DEHPT T	S.D. DPT	SKEH DPT	NOBS T+P	NOBS TV
	MEAN			ME AN	5.D.		HEAN				
101	MB	MB		DEG K	DEG K		DEG K	DEGK			
.000	10.342	2.685	11	265.09	4.24	. 05	290.13	4.20	-1.01	763.	763.
. 100	10.100	2.576	[4	285.70	4.08	. 10	279.83	4.12	-1.05	770.	771.
1.003	5.000	2.329	. 70	293.25	4.69	. 37	₹£3.11	6.45	17	779.	78∙ .
2.000	2.6+5	1.715	1.24	278.23	4.70	05	2 00.02	7.79	. 15	778.	784.
3.000	1.636	1.167	1.47	272.76	4.45	50	253.91	8.00	. 16	775.	7 8 .
4.000	1.003	. 784	1.69	266.71	4.23	73	248.13	8.04	.21	774.	703.
5.000	. 641	. 505	1.52	253.97	4.38	~ . B4	242.97	8 . 32	07	774.	783
6.000	. 378	. 321	2.07	25 2 . 77	4.47	84	237.19	8.61	27	772.	7 94 .
7.000	.203	.177	1.89	245.19	4.45	71	230.71	9.03	- , 444	756.	783.
B. 000	.110	.089	1.93	237.54	4.24	43	225.3 3	8.46	64	5 77.	781.
9.000	.003	. 050	. 77	230.00	3.94	.¢9	221.29	8.39	72	9 9.	780.
10.000	.016	.014	1.64	222.98	3.63	.63	81.015	5.45	. 79	15	779.
11.000	3 0 333	93.979	999,99	2!7.47	4.75	.84	9 39.39	99.99	999.99	1.	777.
12.000	93.939	99 .999	939.99	215.42	6.12	.47	939.9 9	93.99	999.99	1.	פרל.
13.000	99 999	99 .933	939.99	215.60	5.14	45	933.99	99.99	933.99	0.	767.
14.000	99.933	99,939	999.9 9	214.58	3.62	29	9 99.9 9	99.99	9 99. 99	٥.	759.
15.000	99,979	9 9.939	909.93	212.49	3.39	01	933.99	99.99	9 99, 99	0.	758.
16.000	93,530	9 3.9 9 9	939.99	210.43	3.76	15	3 99, 9 9	99.99	333 39	0.	754.
17.000	99,999	93.933	939.99	209.14	3.91	22	939.99	99.99	913.99	0.	7.41.
18.003	37.979	99,939	933.99	209. 96	3.01	~ . 2%	910.99	93.39	933.99	0.	733.
19.000	99,999	93.999	939.99	209.78	3.34	15	993.99	99.93	933.99	0.	731.
20.000	30.573	99.999	939.99	510.38	3.03	.09	999.99	99.99	999.99	0.	725.
21.000	23 339	93.339	933.99	212.19	2.90	.06	993.99	99.99	994.99	0.	583.
82 : 00 0	99.99 3	99.933	999.99	213.29	2.83	03	9 30 (19	93.9 9	909.99	0.	574.
23.000	3 3 53 3	91,999	999.99	214.24	2.93	01	993.99	99.99	9 99 99	0.	563.
24.000	99.999	90.999	909.99	215.47	3.09	.03	999.99	9 9.93	999 33	٥.	€60.
25 000	9 9.933	99.939	99 9 . 99	815.62	3.08	~.16	999,99	99.99	943. 33	٥.	Бчч.
26.000	99,733	93.933	97 3 93	217.80	3.14	26	99 9.99	39 39	9739 39	0.	634.
27 CCC	9 9. 292	99.999	9 29 99	219.28	3.16	38	933.9 9	99.39	933,99	0.	494.
ee.ccs	ā ⊴ a3 3	99 .933	939.99	220.77	3.28	~ .60	993.99	99.39	ā.13 33	0.	449
29 000	99.999	99.999	999.99	222.65	3.1-	~.49	999.99	99.99	333 33	0.	420 .
30.0J0	99.939	99.999	999.9 9	224.76	3.35	~.45	993.9 9	99.99	999 99	0.	411 .

TABLE III-3. MOISTURE RELATED STATISTICAL PARAMETERS

MARCH

STATION	- 723930	VANDE	MERC AFR						5451 POT	NOBS THP	NOBS TY
2	VAPOR P	S.D. VP	SKEH YP	TV	TV	SKEH IV	DEMPT T	5.0. OPT	SKEH DPT	WIRS I'M	AUGS 11
	MEAN			MEAN	5.0.		MEAN OFG K	DEG K			
KM	MB	MB		DEG K	DEG K			3.54	~.85	847.	847.
.000	10.630	2.375	16	285.00	3.67	.05	263.66		85	869.	869
. 100	10.422	2.316	20	235.66	3.74	.04	200.38	3.52	- 34	977.	885.
1.000	5 120	2.302	.62	283.23	5.11	. 30	269.45	6.43		865.	887
2.000	8.608	1.663	1.40	278 . 33	5.29	25	269.92	7.56	. 18	860.	ee7.
3.000	1.538	1.152	1.52	272.96	4.90	56	253.54	8.22	03	9 61.	9 96.
4.000	.9~ 9	.765	1.74	266.36	4.72	78	247.62	8.48		863.	996.
5.330	.593	.485	1.89	260.26	4.57	85	242.05	8.43	11	861.	8∂5.
6,630	. 352	.2 97	1.78	252.97	4.55	82	236.37	B.71	27	849.	896.
7,030	. 185	. 170	1.88	245.32	4.47	72	243.68	9.05	28	6≥3.	885.
8 000	.101	.090	1.95	237. <i>7</i> 4	4.15	32	22+.39	9.59	47	96.	894
9.000	.076	.060	1.03	230.24	3.71	D'+	221.83	B.76	65	90. 17.	884
10.000	.020	.013	. 30	223.29	3.42	. 23	212.63	5.45	17	7.	883
11.000	.009	.004	. 39	217.93	3.92	.92	207.57	2.88	. 10	7.	880
15 000	.008	.002	. 32	215.36	5.42	. 37	205 66	1.89	.23	v.	879
13.000	99.993	99 .939	993.99	215.39	5.29	50	993 99	99.99	999.93	2.	875.
14.000	99,000	99.939	999.93	214.80	3.95	47	999.99	99.99	999.99	2. 1.	872
15.603	93.339	29,339	339.59	212.99	3.38	14	993.99	93.33	933.99	0.	870.
16.000	99.939	99.939	393.59	211.25	3.39	14	999.99	93.99	999.99	0.	8*.8.
17,000	33.533	93.333	929.39	210.32	3.38	21	993.99	99.93	993.93	0. 0.	8 57.
18.000	93,339	9 9.39 9	933.99	210.23	3.19	31	999.99	99.39	959.99	0.	8·3.
19.000	99.939	99.330	999.99	211.04	2.82	24	939.99	93.99	973.99	0.	659.
23.368	93 333	90.729	992 33	211.97	2.73	24	939.99	99.99	939.99	0.	689.
21.000	93.979	99,999	993.93	213.06	2.58	06	999.93	99.93	999.99	σ.	6 72.
22 000	99,929	99.939	999.99	214.42	2.56	- 04	993.93	99.99	939.99	_	658
23.000	99.099	93 933	233,93	215.69	2.53	20	923.39	99.99	969.99		765.
84 000	99.909	99.933	999.99	216.93	2.59	.22	999.99	99.99	909.99	0. 0.	75/4.
25.000	93 999	99,999	999,99	218.26	2.66	.2 7	9119.99		999 99	0.	744.
26.000	99 399	99.999	999.99	219.71	2.93	.31	393.99	99.99	999.99	0.	609.
27.000	99.999	99.933	999.99	221.43	3.11	,47	999.99	99.99	939.99		562
28.000	99.339	99.999	999.99	223.29	3.53	.55	939.99	99.99	993.39		533.
29.000	99,999	99.999	999.99	225.36	3.90	.61	993.99		939.99	1	573. 573.
30.000	99,999	99.999	333.95	227.54	4.11	.52	3 93.99	99.93	939.99	υ.	3, 3,
5-1-1											

TABLE III-4. MOISTURE RELATED STATISTICAL PARAMETERS

APRIL

STATION	• 723930	VANDE	NEIGHC AFE								
2	YAPOR P	5.0. VP	SKEH VP	tv	TV	SKEH TV	DEMPT T	S.D. DPT	SKEH DPT	NODS THP	NOBS TY
	MEAN			MEAN	S.D.		MEAN				
KC4	MB	HB		DEG K	DEG K		DEG K	DEG K			
. 000	10.609	1.793	~.13	296.00	3.74	. 19	280.80	0.60	78	809.	809.
. 100	10.37	1.751	13	285.64	3.62	.15.	? 80 50	2.59	- , 75	829 .	829.
1.000	4.905	2.054	- 38	283.78	5.35	. 16:	269.27	6.05	51	823.	831.
S 000	2.302	1.396	1.53	278.38	5.32	29	<i>25</i> 8 67	6.98	. 18	Ð13.	832.
3.000	1.368	.935	2.00	273.70	5.22	- ,72	258,23	7.15	.21	8 07.	832.
9.000	.833	.656	5 . 68	267.05	5.11	-1.03	Sr£ 39	7.18	. 37	90 8 .	832.
5.000	.515	.422	2.47	261.31	4.89	-1.27	241 01	7.42	.21	BCB.	8 ₺2.
6.000	. <i>2</i> 97	. 252	2.42	254.15	4.66	-1.33	235 2B	7.45	. 10	811.	83 0 .
7.000	. 162	.147	2.32	2 •6.69	4.20	-1.04	538 39	7.93	04	805.	831.
8.003	.096	.073	1.82	239.17	3.58	5≳	553 30	7.80	29	692.	828.
9.000	.058	.049	1.03	231.67	3.04	· . 144	219.35	8.72	-,41	118.	8 2 9.
10.000	.016	.008	. 84	224.56	2 94	. 19	211.53	3.70	.28	14.	ક∂'હ .
11.000	.016	.010	1.11	218.50	3.36	1.11	211.55	3.98	.53	7.	826.
12.000	.014	.010	1.04	214.73	4.73	.83	510.11	5.21	. 05	7.	8.75.
13.000	9 9.97 3	9 9.999	999.99	214.33	5.18	02	999.99	99.99	999.99	5.	8 02.
14.000	9 9.079	99 .999	999.99	214.52	4.00	34	999.99	99.99	999.99	٧.	819.
15.000	33,333	3 3 3 39	999.99	213.49	3.26	.05	9 39. 99	93.99	999.99	3.	818.
16.000	99,933	9 9.339	993.93	212.18	3.29	09	997 39	99.99	999.99	٥.	818.
17 000	99.993	93.939	991.99	211.70	3.16	16	993 SH	93.99	999.99	G.	793.
18.000	9 9.939	99,009	999.93	212.00	3.69	37	990.99	99.99	999. 99	0.	793.
19.000	93.939	99.93 9	999.99	212.73	2.66	18	949.99	99.99	939.99	٥.	782.
20.000	99.9 29	93.973	933.99	213.37	2.41	<i>e</i> 0.	999 99	99.93	333 33	0.	776.
21.000	99 399	6 2 333	3 63 83	214.65	2.58	64	833 88	99.99	939.99	Q.	634.
22.000	99.933	99 .999	927 99	216.04	2.70	18	993.99	99.99	939.99	0.	627.
23.000	99.999	93.999	929.99	217.48	2.65	.03	939 99	99.99	999.99	٥.	6 ∂0.
24.000	99.999	93.939	994 99	218.67	2.66	. 10	999 99	99.99	999.93	٥.	697 .
25.000	90.999	99.933	907.99	220.17	2.75	~.04	943.99	93.99	919.99	٥.	719.
26.000	99.323	93.9 33	999.99	221.83	2.95	~ . 04	999 99	99.99	949.99	0.	712.
27.000	99.999	99.999	923 99	223.81	3.13	.02	993.99	99.99	333 3 3	0.	574.
29.000	99.333	99.999	999.99	25.72	3.21	.03	939.93	99 99	999.99	0.	529.
29.000	99.999	99.993	<u>∂</u> 03`63	27.7 2	3.23	. 05	999 99	99.99	993.93	0.	506.
30.000	99.999	99.999	39 3 . 99	£8.655	3.32	.01	999 . 9 9	99.99	999.99	0.	500.

TABLE III-5. MOISTURE RELATED STATISTICAL PARAMETERS

MAY

STATION	• 723930	+ATCE	SEA DROBE								
Z	VAPOR P	5.0. VP	SPIEW VP	17	TV	SKEH TV	DEHPT T	S.D. DPT	SKEH OPT	N085 T+P	NOBS TV
	HEAN			MEAN	S.D.		MEAN				
KM	MB	MB		DEG K	DEG K		£€6 K	OEG K			
. 330	11.621	1.572	02	287.05	3.5!	. 6 1	262.21	2.06	53	6 59.	859 .
. 100	11.540	1.588	- 25	286 . 89	3 4	. 6~?	282.10	2.10	57	98 0.	99 0 .
1.003	5.773	2.313	. 33	268.06	5. 33	.c <i>2</i>	271. 27	6.10	66	877.	989
2.000	3.158	1.529	.69	293. 9 7	5.25	- ,40	263.02	6.50	28	9 €8.	830.
3.000	1 917	1.122	1.18	278.14	4 50	V-	25.6.42	7.13	14	889.	830.
4 000	1.143	. 749	1.52	271. 97	4.46	"	25.0.16	7.22	03	873.	830.
5.000	.649	.425	1.49	2€5. 3F	7.23	-1.03	<i>2</i> 43.96	6.86	05	874.	83 0.
6.000	. 368	.243	1.50	<i>2</i> 56.2	1.23	-1.0C	237.97	6.8 9	29	874.	963.
7.000	.191	. 134	1.68	250.5 +	1.16	97	271 · 32	7.04	35	872.	889.
8.000	.101	.072	1.47	246.13	6. 9 7	- . 77	225.25	7.20	52	807.	88⊶.
9.000	.052	.040	1.22	235.01	3.53	- , 44 1	219.10	7.86	53	426.	8 83.
10.000	.024	.011	.70	227.46	3.10	32	214.70	3.90	77	20.	8 81.
11.000	.012	.0ან	1.33	220.E9	2.79	.2 2	209 55	3.49	. 19	13.	881.
12.000	.006	.003	1,48	215.58	3.34	1.05	205.07	3.10	-56	13.	8 8).
13 000	93.939	9 9.09 <u>9</u>	939 .39	213.46	<i>- ≥</i> 9	.41	919 99	93.99	999.99	5.	879.
1 4 010	83 J33	99.933	939 . 99	213.49	3.86	01	95.3.99	99 .99	999.99	2.	676.
15,000	33 343	93.933	939, 93	215 62	3.35	.18	933 99	99.99	999.99	₽.	פר9.
16 000	99.333	30, 339	33 0 3 3	211.76	3.42	12	999.39	99.99	999.99	٥.	874.
17 000	93 939	93 939	9 09 23	211.39	3 23	31	97.3 99	93.93	949.99	٥.	. حرو
19 000	99 939	9 9.939	99 0 93	211.76	2.98	24	999.99	99.99	999.99	٥.	845.
19.000	39.133	3 3 993	99 9-93	212.62	2,44	23	3 63 33	9 9.99	939. 99	0.	93⊶.
20.000	99 93 0	3 3 333	53 6 88	513 90	2.13	14	9 ~3.39	99.39	979.99	0.	828
21.000	20 33 3	3 3 3 33	930.39	215.31	5.05	11	9 63- 99	99 99	939.99	0.	677.
55,000	99.1 99	99 997	999, 93	516 63	2.00	11	9 99, 99	99.99	993.99	0.	662.
23.000	93 993	99 9ng	999.99	č19 61	1.98	17	999 79	99 99	993.99	0.	651.
24.000	93 9 39	9 9 599	977, 99	250 35	2.04	12	999 99	99 99	999. 9 9	0.	664 .
25.000	99.539	99.999	939 <i>0</i> 0	252 15	2.15	04	999.99	99.39	999.99	0.	762.
₽ 6 .00 0	9 9-939	9 9.9 99	999 99	223.99	2.26	08	9 99. 99	99.99	999.99	0.	755.
27.000	99 999	9 9.9 99	999. 99	2 25. 96	2.42	.03	909.99	99.99	939.99	٥.	619.
∂8. €00	99 <i>J</i> 93	99 333	3.33 33	227.7 9	₹.48	.13	9 03.99	99.99	999 39	Q.	500.
29.000	9 9 343	99 .909	003 00	289. 5 7	2.49	.19	999.99	99.99	9 99.9 9	0.	544.
30 000	99.33	93.993	9 13 BB	231.40	2.41	. 20	999.93	99.99	939 33	0.	5 27.

TABLE III-6. MOISTURE RELATED STATISTICAL PARAMETERS

JUNE

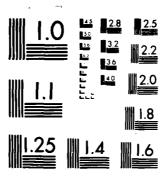
STATION	• 723933	VANDE	NBEHS AFB								
Z	4 ACCIAY	5.0. VP	SAEH VP	TV	īv	SKEH TV	DEHP" T	S.D. DPT	SKEN OPT	NORS THE	MOBS TY
	MEAN			MEAN	5.0.		MEAN				
KM	HB	H8		DEG K	DEG K		DELK	DES K	-		
. 600	12.570	1.681	09	208.18	3.58	.63	283.33	2.07	70	756.	756.
.100	12.624	1.649	14	289.24	3 42	.67	283.45	2.03	75	775.	775.
1.(20	6.110	8:658	.54	<i>≥</i> 92.30	5.94	46	271.35	6.24	22	777.	789.
2.000	3.577	1.662	. 89	209.53	4.55	66	264.82	5.95	.02	77+	790.
3 .000	2.260	1.157	1.23	202 . 7 2	3.99	75	258.94	5.94	بح.	769.	790.
¥.300	1.454	.831	1.45	276,49	3.72	71	253.16	6.27	.29	768.	789.
5.000	.860	.56 9	1.90	<i>2</i> €9. <i>6</i> •	3.57	75	247.22	6.41	.40	771.	790.
6 .00 0	.503	. 377	2.45	2 €2.53 5	3 53	91	2-1.15	6.73	. 32	768.	798.
7.000	.276	.242	8.80	æ5.39	3.43	99	234.54	7.33	. 25	763.	788,
8.000	. (50	. 1 35	2.71	247.58	3.52	79	228.48	7.50	. 10	744.	789.
9.000	.072	.067	₹.52	233.84	3.42	51	221.61	7.89	16	€83.	786
10 000	ə£ 9.	.040	1.82	232.16	3.15	26	214.59	8.92	.21	169.	786.
11.000	.026	.027	2.64	<i>≥2</i> 4.98	2.95	10	214.60	4.71	1.88	13.	782.
15 000	.013	.01:	2.50	219.03	3.01	.07	203.60	3.97	1.94	12.	781.
13.000	.0:0	510.	2.13	214.92	3.41	. 34	207.22	5.14	1.42	10.	778.
14.000	.01≒	.019	1.35	2 12.43	3.51	. 31	207.73	7.10	1,24	6.	777.
15.000	83 333	93.999	939.33	210.43	3.56	.00	933.99	93.99	939.99	3.	774.
16.000	63.939	99.339	993.99	208.96	3.64	03	999. 99	99.99	999.99	Ō.	772.
17.000	99 99 9	99 , 939	999.99	208.70	3.32	09	929.99	99.99	999.99	Ů.	74B.
16 000	39 3.13	97.929	<i>≌</i> ⊛.99	209.81	2.77	.09	999.99	99.99	999.99	Ō.	749.
19 000	99 933	99 .999	993.99	211.95	2.19	.10	999 93	99.99	999.39	0.	743.
20.000	23.923	99 .009	9m.99	214.01	1.80	.03	999.93	99.93	999.99	Ċ.	738.
21.000	99.333	9 9.933	999. 99	215.96	1.61	. 1 1	999.99	99.99	999.99	٥.	574.
55 000	39.999	99,939	993.99	217.89	1.56	.09	993 33	99.99	993 99	٥.	538.
23.000	99,999	99.999	999.99	219.80	1.58	. 31	939.39	93.99	999.99	ũ.	533.
≥+.000	93.39 3	99.999	9 93.75	221.55	1.53	. 37	993.99	99.99	999.99	Ó.	534.
25,000	33 333	99.999	3 €	223.31	1.58	.19	999 99	99.99	993. 99	O.	699.
26.000	3 3.23 9	99,999	ز ر ۲	275.12	1 73	.22	999 93	99.99	999.99	Ö.	669.
27.000	30 333	9 3.359	9.49.99	227.0:	1.82	. 28	999.99	99.99	909.99	Ö.	569.
28.000	93.93 3	99.999	603 60	229.67	1.96	.26	9 59 30	99.99	903 39	o.	505.
29.000	99.993	99.993	921.99	230.32	1.97	25	933 99	99.99	999.99	o.	468
30.000	3 9.999	99.939	913.99	232.17	2.00	25	999.99	99.99	933 99	o.	455.

TABLE III-7. MOISTURE RELATED STATISTICAL PARAMETERS

JULY

STATION	- 723930	VANDE	SERO AFB								
Z	VAPOR P	S.D. VP	SKEH VP	TV	۲V	SKEH TV	DEHPT T	S.D. DPT	SKEH OPT	NORS THE	NOBS TV
	MEAN			MEAN	5.0.		MEAN				11003 11
KM.	MB	MÐ.		DEG K	DEG K		DEG K	DEG K			
.000	13.5+4	1.588	-10	288.85	3.29	.30	₹₩4.53	1.79	~.33	809.	809.
. 123	13 733	1.545	. 04	∂83.0 •	3.13	. 35	ć 84. 75	1.73	~.40	830.	833.
1.000	6.330	2.6+4	1.11	296.60	4.09	65	272.64	5.94	. 13	819.	843
8.000	4.428	2.293	1.32	2 92 . 33	3.04	- 54	267.43	6.34	. 35	824.	847.
3.000	3.075	1.935	1.34	286.01	₹.39	42	262.18	7.18	.52	815.	846.
4.000	2.027	1.473	1.58	279.29	2.10	23	₹ 56.60	7.64	.63	815.	845.
5.000	1.199	.955	1.86	272.39	2.11	.02	250.19	7.67	.71	615.	8∾5.
6 000	.636	.547	2.35	2 05. 59	2.22	15	243.21	7.22	. 80	824.	843.
7.000	.321	.284	2.47	258.46	2.36	27,	236.11	7.10	. 60	804.	344
8.000	. 165	. 148	2.14	251.03	2.50	30	° 229.30	7.50	. 30	797.	843
9.000	.079	.074	2 46	243.53	2.64	33	222.48	7.67	. 97	793.	843.
10.000	.036	.036	1.97	236.06	2.69	4ح	215.35	8.09	.17	429.	84€
11.000	.023	.017	1.84	228.89	2.58	20	£13.78	5.47	32	25.	6 ~2.
12.600	012	.035	1.52	252.35	2.33	27	209.42	2.81	. 92	17.	841.
13.0.0	99 .909	99.99 9	939.39	215.46	2.27	.23	999. 99	99.99	999.99	5.	632
14.010	9 0 909	99.999	9 99.3 3	211.28	2.61	. 75	\$99.9 9	99.99	999.99	0.	83 ≥.
15.000	99 009	99.939	999.99	207.26	2.95	. 63	\$99.9 9	99.99	999.99	٥.	827.
15.000	99.939	99.939	999.99	205.75	2.98	.84	9 93. 93	99.99	999.99	0.	827.
17.003	39 539	99.939	ე შ9 .90	205.68	2.65	.51	939.99	99.99	399.99	0.	795.
19.000	99.393	93.959	999.99	209.88	2.25	. 22	999.9 9	99 .99	999.99	٥.	789.
19.000	99.939	90.999	999.99	211.62	1.78	.09	999 . 99	99.99	939.99	0.	783.
20.000	99.973	99.999	99 3.99	214.14	1.65	.02	\$? 9.99	99.99	999.99	0.	773.
21.000	99.399	93.999	9 33.99	216.44	1.58	.04	999.99	99.93	999.99	٥.	78 2 .
2 2.00 0	97.939	99.979	999.99	218,44	1.49	06	99 9. 99	99.99	939.99	0.	588.
23.000	99.933	99.999	999.99	220.24	1.49	12	9 99.9 9	99.99	999.9 9	٥.	584.
24.000	99 339	33.939	919.99	251.90	1.53	12	939.99	99.99	999 .99	٥.	577.
25 000	99.999	39.993	999.99	223.46	1.56	14	<u>99,99</u>	99.59	999 .93	0.	722.
25.000	99.999	99.939	993.99	225.15	1.66	.10	999.9 9	99.99	9 39 . 9 9	0 .	715.
27,000	99.999	93.939	399.93	226.97	1.79	.09	999. 99	99.99	993.99	O.	6 56.
23.000	99.999	99.999	993.99	<i>22</i> 8.53	1.65	07	99 99	99 .99	999.∋9	c .	5 26.
29 000	99.999	99.999	993.99	230.20	2.03	.08	999.99	99.99	399 .99	0.	496.
30.000	99.999	99.999	993.99	231.81	5.00	.04	£99.99	9 9. 9 9	999.99	0.	484.

AD-A128 125 RANGE REFERENCE ATMOSPHERE 0-70 KM ALTITUDE VANDENBERG AFB CALIFORNIA(U) RANGE COMMANDERS COUNCIL WHITE SANDS MISSILE RANGE RNM METEOROLOGY GROUP G G BOIRE ET AL. UNCLASSIFIED APR 83 RCC/MG-362-83 AD-A128 125 RANGE REFERENCE ATMOSPHERE 0-70 KM ALTITUDE VANDENBERG AFB CALLED AFB CALLE										



MICROCOPY RESOLUTION TEST CHART NATIONAL BUREAU OF STANDARDS-1963-A

TABLE III-8. MOISTURE RELATED STATISTICAL PARAMETERS

AUGUST

STATION	723930	VANDE	NEERG AFB								
Z	VAPOR P	5.D. VP	SKEH VP	tv	TV	SKEH TV	DEMPT T	S.D. DPT	SKEDA DPT	NOBS T-P	NORS TV
	PEAN			MEAN	S.D.		MEAN				
KM	HÐ	M9		DEG K	DEG K		DIG K	DEG K			
. 000	14.336	1.696	03	269.83	3.29	. 15	285.39	1.84	50	823.	823.
- 10 0	14,497	1.629	13	290 . 00	3.11	.17	285.57	1.75	58	953.	853.
1.000	6.874	8ce. S	.86	296 · 58	4.51	56	273.69	5.93	10	826.	854 .
2.000	4.616	2.365	1.20	292 . 92	3.79	72	267.94	6.53	. 15	826.	854.
3.600	3.054	1.863	1.27	28 5 . 67	3.11	62	262.07	7.39	.22	820.	854.
₩.000	1.960	1.337	1.31	278.99	2.69	64	256.26	7.1.8	. 33	821.	854 .
5.000	1.136	.855	1.64	272.22	2 . 60	52	243.72	7.17	. 49	814.	854.
6.C00	.649	.542	2.03	255. 39	2.61	62	243.31	7.!.9	.52	814.	855 .
7.000	. 323	.297	2.51	258.37	2.64	63	235.00	7.44	. 41	BC '.	855.
8.000	. 168	. 151	2.05	251.07	5.80	66	223.35	7.75	.21	809.	855.
9.630	.084	. 079	1.90	.743.50	2.97	51	253.34	8.17	.03	904.	955.
10.COO	.041	.040	1.64	236.04	3.11	37	216.12	8.36	.11	436.	855.
11.000	.029	.017	1.06	228.91	3.02	39	215.80	5.13	69	35.	854.
12.000	.011	.005	.89	222.34	2.56	49	203.73	3.17	.00	14.	852.
13.000	.005	.002	.60	216.57	2.07	07	203.63	2.69	.07	9.	849.
14.000	93 .99 9	99.939	939.39	211.50	2.57	.62	933.99	99.99	993.93	٥.	845.
15.000	99.939	99.999	999.99	207.55	3.36	.96	993.99	99.99	999.99	Ö.	B+1.
15.000	99 .93 9	99.999	999.99	205.87	3.71	.8∿	933.99	99.99	939.99	0.	8 79.
17.000	99.939	9 9.993	999.99	2 06 . 9 7	3.21	.51	993.99	99.99	999.99	0.	819.
19.000	99.933	99 .9 93	999.99	209.25	2.64	. 13	993.99	99.99	999.99	٥.	818.
19.000	99.099	93.933	939.93	211.97	1.98	09	993.99	99.99	999.99	٥.	811.
20.000	99.933	99.939	990.9 9	214.31	1.66	08	993.99	99.99	999.99	D.	802.
21.000	93.933	99 .999	699.93	216.34	1.49	.02	991.99	99.99	999.99	٥.	719.
20.000	93.333	99.533	993.99	218.08	1.49	.01	993.99	99.99	999.99	o.	588.
23.000	93.939	93 .9?3	999.39	219.76	1.51	.00	999.39	93.99	999.99	0.	581.
24.000	93.993	99.999	939.33	221.46	1.58	.08	993.99	99.99	999.99	Ö.	580
25.000	99.999	99.999	993.99	223.05	1.59	.04	993.99	93.99	999.99	٥.	748.
26.000	99.999	99 .993	994,99	224.62	1.65	.03	993.99	99.99	999.99	õ.	735.
27.000	99.999	93.999	993.99	226. 38	1.77	04	997.99	99.99	939.99	٥.	650.
20.000	29.979	93 .993	900.00	227.88	1.91	. 19	931.39	99.93	979.39	Đ.	548.
29.000	99.939	99.000	999, 99	229.39	2.11	.12	393.33	99.93	399.99	õ.	500.
30.000	99.99 9	9 9.99 3	999.99	230.08	2.15	.11	991.99	99.99	999.99	C.	470.

TABLE III-9. MOISTURE RELATED STATISTICAL PARAMETERS

SEPTEMBER

STATION	- 723930	VANOE	NEEDERG AFE								
Z	VAPOR P	5.D. VP	SKEH VP	TV	tv	SKEH TV	CEHPT T	S.D. DPT	SKEH DPT	NOBS TOP	NOBS TV
	MEAN			PEAN	\$.D.		MEAN				
9774	MB	145		DFG K	DEG K		DEG K	DEG K			
.000	14.293	2.301	~.32	290.60	4.02	.64	235.₹	2.74	-1.25	<i>'1</i> 45.	745.
. 100	14.303	2.257	52	290.54	3.80	.63	285.27	2.62	-1.44	818.	818 .
1.000	7.356	3.353	. 98	294 . 18	4.84	26	274.43	6.56	~.22	770.	779.
2.000	4.479	2.510	1.35	289.52	3.69	56	267.31	6.98	.25	767.	783.
3.000	2.683	1.807	1.40	293.20	3.04	59	261.32	7.35	.29	766.	703.
4.000	1.686	1.226	1.97	276.93	2.96	46	254.58	7.20	. 56	761.	783.
5.000	.925	.732	₹.51	270.57	2.64	57	≥ 47. 68	6.79	.87	752.	782.
6.000	.498	.422	3.26	263.83	2.88	76	240.97	6.64	.70	750.	781.
7.003	.257	.243	3.35	256.47	2.93	75	233.90	6.96	.63	752.	780.
B.OCO	. 1 38	. 137	2.89	249.95	2.89	54	2 27. 47	7.54	.42	747.	780.
9.600	.067	.069	2.68	241.13	2.93	22	220. 60	7.95	.20	721.	780.
10.000	.029	.035	2.44	233.69	3.01	.01	212.97	7.99	.65	224.	779.
11.000	.021	.015	2.43	226.83	3.15	.10	213.18	5.04	06	≥4.	<i>77</i> ♥.
12.000	.011	.007	1.84	SS1.03	3.01	.16	208.42	4.10	. 06	20.	774.
13.000	.005	.002	.40	216.08	2.85	.14	203.21	3.11	10	15.	772.
14.000	99 .999	99 .939	9 99.99	211.77	2.73	.49	999.99	99.99	999 .99	٧.	772.
15.000	99.339	99.993	999.99	208.25	2.99	.42	999.99	99.99	99 9.99	1.	76 7.
15.000	99.999	99.939	999.99	2 05 . 30	3.18	.26	999.99	99.99	999.99	0.	762.
17.000	99.939	93.993	999.99	206 . 59	3.00	.32	937. 99	99.99	999.99	0.	751.
18.000	99.999	99.999	99 9 . 99	208.22	2.59	.09	999. 99	93.99	999.99	0.	791.
19.G00	99.999	99.999	999.99	210.72	2.12	.05	999.99	99.99	999.99	٥.	798.
20.000	99.999	93.999	993.99	2:3.20	1.86	. 16	999.99	99.99	999.99	0.	784.
21.000	93.939	93.933	939.99	215.34	1.68	.05	999.99	99.99	999.99	0.	621.
22.000	97.933	99.999	999.39	217.19	1.62	11	993.99	99.99	999.99	0.	591.
23.000	99.993	99.993	999.99	219.00	1.60	01	993.99	99.99	939.99	0.	578.
24.000	99.939	93.999	99 3.99	220.69	1.65	08	939. 99	99.99	999.99	0.	574.
25.000	99.939	93.939	993.99	222 12	1.60	.13	999.99	99.99	999.99	0.	721.
26.000	93.939	99.9 9 9	993.99	223.64	1.69	.00	999.99	99.99	999.99	0.	714.
27.000	99.399	9 9. 999	993.99	225.30	1.84	. 15	999.99	99.99	999.99	0.	568
28.000	92,999	99.999	994.99	226.71	2.08	.08	999.99	99.99	999.99	0.	513.
29.000	99,939	99 .999	999.99	228.04	2.21	10	993.99	99.99	999.99	0.	481.
30.600	99.939	99.993	993.99	229.38	2.26	07	999.99	99.99	999.99	0.	463.

TABLE III-10. MOISTURE RELATED STATISTICAL PARAMETERS

OCTOBER

STATION	- 723730	VANDE	NOOPG AFB								
Z	VAPOR P	5.0, VP	SKEH VP	TV	ΤV	SKEH TY	DEWPT T	5.0. OPT	SKEH DPT	NOBS THP	NOSS TV
	MEAN			HEAN	S.D.		HEAN				
KPI	MB	118		DEG K	DEG K		DEG K	DEG K			
. 003	12.912	3.044	67	283.62	4.14	.09	293.44	4 55	-1.70	926.	626.
. 100	12.761	2.977	75	<i>₽</i> ₽9.√6	3.98	.09	283.27	4.19	-1.74	6 •0.	6 ~0.
1.000	6.120	2 .902	. 82	290.57	5.29	06	271.00	6.48	.04	956.	965.
2.030	3.443	2.006	1.41	285.57	4.59	64	293. 8 3	6.94	.29	8 51.	966.
3.000	2.110	1.358	1.75	279.83	٠.01	9 6	257.54	6.97	. 39	825	966.
4.003	1.275	.882	1.90	273.90	3.87	-1.01	251.45	6.95	.40	625	965.
5.000	.רר.	.568	2.06	267.41	3.02	-1.20	2+5.73	7.08	.26	855.	865.
6.000	.471	. 366	2.04	260.39	3.77	-1.26	5+0.15	7.42	.11	854.	963.
7.000	.263	.212	2.00	25.2.82	3. 69	15.1-	233.93	7.80	11	625.	963 .
8.000	.141	.120	1.72	245.14	3.50	96	227.61	8.22	22	809.	962.
9.000	.069	.060	1.71	237.54	3.06	31	221.03	8.40	35	647.	962.
10.000	.040	.046	1.75	230.29	2.69	. 03	215.41	8.89	. 29	75.	961.
11.000	.013	.003	1.01	253.80	3.21	.51	210.76	l . 35	.69	11.	958 .
12.000	.000	.002	1.04	218.56	3.61	.54	205. 95	1.63	. 89	10.	95 0.
13.000	99.939	99.939	999.99	214.82	3.45	. 39	939.99	99.99	99 9.99	4.	95 8.
19.000	99.999	99.933	99 3.99	211.70	3.23	.14	939.99	93 .99	999 . 99	1.	<i>9</i> 57.
15.600	99.999	99 .999	9 93.99	208.90	3.23	.14	999. 99	99.99	999.99	1.	95 4 .
15.000	99.999	93 .999	999.99	20G.98	3.35	.02	999.99	99.99	999.99	٥.	85 3.
17.000	99. 999	99.939	990.99	206.56	3.31	.08	933.93	99.99	999.99	0.	817
18.000	99.933	93.993	993.99	207.68	5.95	.11	939.99	99 99	999.99	Q.	815.
19.000	99.999	93.999	993.99	2 09.€+	2.42	.06	939.99	99. 99	999.99	Ō.	907.
20.000	99.999	99.939	939.99	211.68	2.19	.10	939.99	99.99	939.99	0.	BCD.
21.000	99.939	99.999	973.99	213.79	2.10	.10	999.99	99.99	939.99	Q.	634.
£2.000	99.933	99.939	939.99	215.59	2.10	09	939.99	99.99	999.99	o.	621.
23.000	99.939	99.339	939.99	217.26	8.18	17	999.99	99.99	999.99	Q.	5 10.
24.000	93.939	99.999	93 3.99	218.80	2.24	19	933.93	99.99	979.99	Q.	646.
25.000	99.939	99.399	939.99	220. 3 6	5.23	24	9 39. 99	99.99	999.99	Ģ.	731.
26.000	99.999	99.939	999.99	231.62	₹.31	32	993.99	99.99	939.99	o.	717.
27.000	99.933	99.999	999.93	222.87	₽.₩	~.36	93 9.99	99.99	903.99	Q.	563.
26.000	99.999	93.303	97) 99	20. €5	≥.66	44	993.99	99.99	999.33	O.	510.
29.000	93.939	99.999	93 3. 99	225.14	2.83	- , 34	939.39	99.99	999. 9 9	0.	479.
30.C00	99.999	93.999	999.99	526.22	79.5	15	939.99	93.99	999.99	0.	460.

TABLE III-11. MOISTURE RELATED STATISTICAL PARAMETERS

NOVEMBER

STATION	• 723930	VANCE:	ADRG AFB								
Z	VAPOR P	S.D. VP	SKEH VP	TV	TV	SKEH TV	DEHPT T	S.D. DPT	SKEH OPT	NOBS TOP	NOSS TV
	MEAN			MEAN	S.D.		MEAN				
KP1	M9	HB		DEG K	DEG K		DEG K	DEG K			
.000	11.137	3.237	02	287.91	4.40	.04	291.09	4.69	~.75	968.	960.
.100	10.979	3.133	06	267.6×	4.24	.07	260 · 29	4.61	79	882 .	665
1.000	5.676	2.892	.63	286.58	5.02	.09	270. 58	7.04	09	890.	894.
2.000	3.143	2.098	1.27	281.92	5.02	3 8	₹€2.07	0.07	. 19	879.	895.
3.000	1.885	1.366	1.72	276.77	4.84	64	255.64	7.95	.21	678.	89 5.
4.000	1.190	.935	1.92	270. 89	₩.67	78	250.00	8.11	.82	977 .	895.
5.000	.774	.636	1.97	264.38	4.56	86	Z+4 . 93	0.42	.05	878.	895.
6.000	.458	.412	₽.08	257.43	4.44	85	₹39.≥	8.70	02	877.	995 .
7.000	.271	.255	2.01	250.10	4.31	6∿	233.28	9.17	13	872.	89 ∙.
8.000	.145	.132	1.67	242.61	4.09	65	227.24	9.26	34	8 20.	89 2.
9.000	.079	.068	1.54	235.11	3.69	27	88.155	8.97	47	476.	889.
10.000	.033	.029	1.29	227.93	3.39	.12	215 26	7.11	.08	43.	8 89.
11.200	.915	.010	1.48	251.39	3.53	.52	210.47	4.43	.78	17.	886 .
12.000	.008	.004	.71	216.15	4.15	.50	206. 59	3.63	.≥€	15.	984.
13.000	99,999	93.999	999.99	212.85	4.39	. 16	999. 99	99.99	999 .99	5.	879.
14.000	99,999	93.999	993.99	210.73	3.80	.08	999. 9 9	99.99	999.99	١.	873.
15.000	99.939	99.939	399.99	208.74	3.53	.27	9 99. 99	99.99	999 . 99	0.	870.
16.030	93.99 9	99.999	99 9.99	207.13	3.67	.23	999.99	99.99	999.99	0.	967.
17.000	99 .939	99.999	999.99	206.72	3.72	.08	939.99	99.99	999 .99	٥.	842.
19.000	99.993	99.993	999.99	207.36	3.47	05	939.99	99.99	99 9.99	0.	8 40.
19.000	99.9%	93.999	933.99	208.75	3.00	.00	939.99	99.99	999.99	٥.	825.
20 .00 0	99.399	99.999	993.9 9	210.13	2.55	01	939.99	99. 9 9	939.99	٥.	815.
21.000	99.999	99.999	993 . 99	211.73	2.19	01	939. 99	99.99	999 .99	٥.	69 1.
22.000	99.939	99.999	999.99	213.21	2.18	05	999. 99	99.99	999.99	o.	676 .
23.000	99.993	99.999	993.99	214.78	2.14	.00	999. 39	99. 99	939.99	0.	668 .
24.000	99.999	99.999	999.99	216.11	2.23	19	999.99	99.99	999.99	٥.	768.
25.000	9 3.999	99.999	99 9 . 99	217.49	2 38	18	9 99. 9 9	99.99	999.99	0.	763.
26.000	9 9. 3 93	99.999	329.99	218.86	2.57	.08	939.99	99.99	999.99	0.	751 .
27.000	99.399	99.939	939 .99	220.01	2.70	. 17	999.99	99.99	939.99	Ç.	589
20.000	99.999	99.99 9	999.99	221.20	2.65	. 17	93 3. 9 9	99.99	99 9.39	Q.	548.
29.000	99.999	99.999	933.99	<i>222</i> . 39	5.92	.05	939 99	99.99	939.99	o.	516.
30.000	99.9 99	99.999	999.99	223. 65	3.01	.01	999.99	99.99	999.99	0.	517.

TABLE III-12. MOISTURE RELATED STATISTICAL PARAMETERS

DECEMBER

STATION	• 723930	VANDE	BORG AFB								
Z	VAPOR P	S.D. VP	skeh vp	14	TV	SKEH TV	DEMPT T	\$.0. DPT	SKEH DPT	NOBS T-P	NOSS TY
	MEAN			HEAN	S.B.		HEAN				
KPI	MB	MB		CEG K	DEG K		DEG K	DEG K			
.000	9.409	3,129	ىح.	205.77	4.87	-,14	278.46	5.23	72	902.	902.
. 100	9.231	3.022	.23	285.44	4.72	12	278.21	5.15	75	918.	919.
1.000	¥.763	2.777	1.17	283.78	5.17	10	267.92	7.47	.18	926.	939.
≥.000	2.792	1,931	1.44	279.17	5.49	48	260.47	8.17	.21	917.	934.
3.000	1.000	1.332	1.54	10 . مروح	5.33	84	254.98	6.07	.27	914.	934.
4.000	1.099	.893	1.89	268 . 33	5.17	-1.05	258.97	8.25	.23	917.	934.
5.000	.672	.595	5.05	261.79	5.02	-1.09	243.09	8.71	. 13	922.	933.
6.000	. 393	. 359	1.93	<i>2</i> 5⊶.69	4.90	97	237.40	8.93	03	919.	931.
7.000	.227	.209	1.66	2-7.37	4.59	66	231.57	9.09	15	913.	931.
9.000	.125	.110	1.55	239.9	4.21	35	226.13	0.89	37	777.	929.
9.000	.082	.037	1.37	232.49	3 85	06	222.52	9.65	58	254.	988.
10.000	.031	. 028	1.96	225.35	3.53	.27	215.38	6.31	.24	34.	926 .
11.000	.014	.004	. 52	219.35	3.65	.68	211.06	2.16	.23	8.	923.
12.000	.009	.003	1.17	215.44	4.98	.48	207.46	2.50	.56	8.	923.
13.000	99.909	99.993	979.99	213.93	5. 19	04	999.99	99.99	999.99	1.	919.
14.000	99.999	9 9.939	999.99	212.55	4.25	.03	999 99	99.99	999.99	0.	917.
15.000	99.999	99.939	9:39.99	210.67	3.91	.24	939.99	99.99	999.99	0.	911.
16.000	99.939	99.939	999.99	2C8.91	3.99	.17	839, 99	99.99	999.99	0.	905.
17.000	99.999	99.939	93 0 99	208.04	4.09	04	939.99	99.99	999.99	0.	868.
18.003	99.9 9 9	93.993	973.99	2C8 .21	3.87	29	999.99	99.99	999.99	O.	96 1.
19.053	99.999	93.939	977.99	209.17	3.36	47	993.93	99.99	999.99	0.	B+2.
20.503	9 9 539	93.999	923.99	210.3	18.5	52	999.99	93.99	999.99	0.	823.
21.000	93.9 79	93.993	993.39	211.76	2.73	S S	999.99	99.99	999.99	0.	674.
22.000	99.999	99.939	999.99	213.10	₽.6	.00	999.99	99.99	999.99	0.	657.
23.000	90.999	93.993	833 39	214.43	2.59	~.04	999.99	99.99	999.99	٥.	641.
2000.	99.999	99. 333	973.99	215.67	2.63	50.	933.99	99.99	999.99	0.	750.
≥5.000	99 .9 99	93.999	939.39	216.82	2.78	.67	993.99	99.99	999.99	D.	733.
26.000	93.999	99.939	923.99	218.00	3.07	.13	999.99	99.99	999.99	0.	729.
27.000	9 9.99 9	99.999	9:9.99	219.01	3.34	. 30	979.99	93.99	939.99	0.	583.
28 . 0 00	99.999	99.999	922.99	2 20. 05	3.48	.37	939.99	99.99	999.99	<u>o</u> .	535.
29 .000	99.999	99.939	999.99	221.17	3.50	.31	999.93	99.99	999.99	0.	495.
30.000	39,399	99.999	993.99	222.35	3.50	.15	993.99	99.99	993.99	٥.	478.

TABLE III-13, MOISTURE RELATED STATISTICAL PARAMETERS

ANNUAL

STATION	- 723930	VANDE	NEERG AFB								
Z	VAPOR P	S.D. VP	SKEH YP	TV	TV	SAIEH TY	DEHPT T	S.D. OPT	SKEH OPT	NOBS THP	NOSS TY
	MEAN			MEAN	S.D.		HEAN				
KIM	118	MB		DEG K	DEG K		DEG K	DEG K			
.000	11.704	2.971	30	287.60	w.36	.01	291.95	4.26	-1.18	9861.	9861.
. 100	11.638	2.981	31	287.45	4.29	01	291.85	4.30	~1.16	10131.	10136.
1.000	5.737	2.806	.89	288.45	7.19	.07	270.83	6.84	18	10096.	10220.
2.000	3.328	2.094	1.37	293.B4	7.06	15	262. 98	7.95	.02	10033.	10246.
3.000	2.105	1.517	1.69	<i>2</i> 78 . 20	6.50	45	256.90	9.21	.11	9986 .	10245.
4.000	1.306	1.048	2.03	272.C9	6.19	53	250. 97	8.32	.10	9987.	10240.
5.000	.784	.662	2.27	265.45	6.11	55	245.12	0.27	.10	9 988.	10239.
5.000	.451	. 399	2.52	256.42	6.19	49	233.10	8.31	04	9969.	10229.
7.000	.242	.224	2.56	251.00	6.22	37,	232.59	8.48	16	9901.	10226.
8.000	. 131	. 121	2.33	243.44	6.14	19	226. 90	8.34	24	6882 .	10210.
9.000	.073	.067	2.17	235.84	5.94	01	221.54	8.26	22	5266.	10198.
10.000	.036	.037	1.96	228.55	5.69	. 12	214.99	8.18	.25	1494.	10190.
11.000	.020	.016	2.73	255.17	5.38	.13	215.67	5.04	. 36	166.	10162.
12.000	.010	.006	3.44	217.54	5.08	08	207.89	3.56	. 83	128.	10148.
13.000	93.999	99.399	939.99	214.86	4.42	29	9 99. 99	99.99	999.99	64.	10106.
14.000	99.99 9	99.999	999.99	212.73	3.8→	.14	999.99	99.99	999.99	20.	10066.
15.000	99.939	99.933	999.99	210.43	4.04	. 18	9 99. 99	99. 9 9	999.99	11.	10025.
15.000	39.939	99.999	999.99	208.76	4.21	.13	999.99	99. 99	939.99	0.	9936.
17.000	99 .999	99.939	99 9 . 9 9	208.45	3.91	.06	933. 93	99.99	999.99	0.	9717.
18.000	99.979	99 .9 99	999.49	209.23	3.49	15	999. 99	9 9. 99	999.99	0.	9724.
19.000	99.999	99.993	9?3. .9	210.78	3.03	45	993. 9 9	99.99	993.99	0.	9 591 .
20.000	99.95 9	99.999	933.93	212.38	2.98	57	939.93	99.99	999.99	0.	9487.
C00.15	99.939	99 . 999	999.99	214.07	2.91	57	999,99	99.99	999.99	0.	7824 .
22.000	99.979	99 , 93 9	939.9 9	215.56	3.04	53	993. 99	99.99	999.99	0.	7909.
23.000	99 .993	99.939	999. 99	217.08	3.20	~.53	999. 99	9 9. 99	999.99	0.	7295.
24.000	93.999	99.993	999.99	218.37	3.40	4444	999.99	99. 99	999.99	0.	7929.
25.000	93 .99 9	99.999	999.29	220.08	3.54	51	999. 99	99.99	999.99	0.	8710.
26 . DDD	99.939	99.999	999.99	221.57	3.76	e#	939.99	99.99	999.99	0.	8 598 .
27.000	99.93 9	99.9 99	999.99	223. 2 4	4.05	46	999.99	99.99	9 93. 93	٥.	7042.
59.000	99. 999	99.999	999.99	224 - 66	4.25	~.41	939. 99	99. 99	933.39	0.	6313.
29.000	99.999	99.999	999.99	23. <i>3</i> 55	4.41	- 36	999.99	99.99	939.99	٥.	5921.
30.000	99.999	93.999	999.99	227.84	4.54	39	999.99	99.99	939.99	0.	5769.

TABLE IV-1. HYDROSTATIC MODEL ATMOSPHERE

JANUARY

	- 723930	VANOE	NEEDRG_AFB	•
2	OEO. HT.	•	0	TV TV
KM and	KM	1018.9300	6/M3 1242.0000	DEG K 205.76
.000	.100	1006.9000	1229.0000	265.41
1.000	.929	903.7500	1110.0000	293.67
2.000	1.997	000.5300	999.9000	278.89
3.000	2.996	707.5600	900.9000	273.62
4.C00	3.994	623.8100	812.1000	267.61
5.000	4.991	548.3300	732.1000	260.93
6.000	5.988	480.3400	659.3000	253.80
7.000	6.985	419.1700	592.9000	245.28
8.000	7.982	364.2500	531.8000	238.62
9.000	8.979	315.0800	475.4000	230.90
10.000	9,975	271.2700	422.5000	223.69
11.000	10.970	232.5500	371.5000	218.05
12.000	11.966	198.7600	321.9000	215.13
13.000	12.961	169.6600	275.6000	214.43
14.000	13.956	144.7500	235.1000	213.55
15.000	14.950	123.3700	203.1000	211.62
15.000	15.944	104.9900	174.6000	200.52
17.000	16.938	89.2490	149.1000	208.47
19.000	17.932	75.8380	126.8000	208.43
19.000	18,925	64.4700	107.2000	209.46
20.000	19.918	54 8580	90.7000	210.71
21.000	20.910	46.7270	76.7500	212.09
22.000	21,903	39.8450	65.0400	213.41 214.54
23.000 24.000	22,835 23,886	34.0080 29.0530	55.2200 46.9300	215.67
25.000	24.878	24.8420	39.9000	216.91
26.C00	₹5.669	21.2610	33.9600	218.09
27.000	26.859	18.2120	28.9400	219.25
28.000	27.650	15.6150	24.6500	220.64
29.000	28.840	13.4020	21.0200	222.11
30.000	29.830	11.5158	17.9200	223.83
32.000	31.806	8.5546	13.0000	230.35
34.000	33.784	6.4005	9.5150	235.52
36.000	35.760	4.8204	7.0120	240.68
38.000	37.735	3.6535	5.1970	246.15
40.000	39.708	2.7861	3.8830	251.19
42.000	41.681	2.1373	2.9080	257.35
44.000	43.652	1.6499		2 62. 9 7
46.000	45.622	1.2795		266.34
48.000	47.590	. 9937		265.70
50.000	49.558	.7705		262.73
52.000	51.524	.5957		259.32
54.000	53.489			257.02
56.000	55,453			255.30
58.000	57.415			253.67 251.11
60.000	59.377 61.337	.2083 1590 .		245.33
62.000 64.000	63.295	. 1208		240.59
66.000	65.253			234.89
68.000	67.209			227.98
70.000	69.165			\$55.88

TABLE IV-2. HYDROSTATIC MODEL ATMOSPHERE

FEBRUARY

	- 723930		NEEDERG AFB	
Z	CEQ. HT.	P	0	TV
KM	KH	MB	G/M3	DEG K
.000	.000	1019.7000	1241.0000	286.09
.100	.100	1006.6000	1227.0000	285.70
1.000	.939 1.997	903.6100	1111.0000	283.25
2.000 3.000	2.996	800.2200 707.05 00	1002.0000	278.23
4.000	3.994	623.1000	903.0000 813.9000	272.76 266.71
5.000	4.991	547.4600	733.6000	259.97
€.300	5.988	479.3300	660.6000	252.77
7.000	6.985	418.0500	594.0000	2-5.19
8.000	7.982	363.0+00	532.4000	237.54
9.000	8.979	313.9500	475.4000	230.C0
10.000	9.975	270.0700	421.9000	255.98
11.000	10.970	231.4100	370.7000	217.47
12.000	11.966	197.7700	319.8000	215.42
13.000	12.961	168.9100	272.9000	215.60
14.000	13.956	144.2200	234.1000	214.58
15.000	14.350	123.0100	201.7000	212.43
16.000	15.944	104.7500	173.4000	2:0.43
17.000	16.938	89.1010	148.4000	209.14
18.000	17.932	75.7470	126.3000	209.96
19.000	18.925	64.4140	107.0000	2 09.78
20.000	19.918	54.8720	90.5200	510.98
21.000	20.910	46.7040	76.6800	515.18
22.000	21.903	39.6240	65.0500	513.58
23.000	22.895	33.9850	55. <i>2</i> 600	214.24
24.000	23.886	29.0280	46.9300	215.47
25.000 26.000	24.878 25.869	24.8160 21.2350	39.9100	216.62
27.000	26.859	18.1880	33.9500 20.9600	217.89
28.000	27.850	15.5960	24.6100	219.29 220.77
29.000	28.840	13.3890	20.9500	222.65
30.000	29.830	11.5104	17.8+00	224.76
32.000	31.806	8.5671	13.0000	232.1.0
34.000	33.704	6.4277	9.5290	237.98
36.000	35.760	4.8590	7.0090	244.57
38.000	37.735	3.7000	5.2090	250.62
40.000	39.708	2.B349	3.9140	255.53
42.000	41.681	2.1827	2.9610	260.08
44.000	43.652	1.6873	2.2630	263.08
46.000	45.622	1.3071	1.7470	264.01
40.COO	47.590	1.0131	1.3550	263.81
50.000	49.558	. 7848	1.0540	2 80.79
52.000	51.524	.6074	.8230	261.31
54.000	53.489	.4695	.6357	260.15
56.000	55.453	. 3623	.4366	257.33
58.000	57.415	.2789	. 3854	255.31
63.890 62.990	59.377 61.337	.2144 1643	7795. 5325.	254.07 249.64
64.000	63.295	. 1251	.1828	بن. وبنے 1.53ء بنج
£5.000	65.253	. 1231	.1413	236.16
58.000	67.209	.0709	.1103	226.56
70.000	69.165	.0525	.0941	220.49
				250.73

TABLE IV-3. HYDROSTATIC MODEL ATMOSPHERE

MARCH

STATION	- 723930	VANDE	NBERG AFB	
Z	GEO. HT.	P	0	TV
KM	KM	M9	G/M3	DEG K
.000	.000	1017.9000	1240.0000	266.00
.100	.100	1005.6000	1227.0000	265.66
1.000	.933	902.0400	1110.0000	283.23
2.000	1.937	799.5500	1001.0000	278.33
3.000	2.996	706.5000	931.7000	272.96
4.000	3.994	655.6900	812.6000	256.96
5.000	4.931	547.1700	732.4000	250.26
6.000	5.988	479.1400	659.8000	252.97
7.000	6.985	417.9100	593.4000	245.32
9.000	7.992	362.9600	531.9000	237.74
9.000	8.979	313.8200	474.8000	230.24
10.000	9.975	270.1000	421.4000	223.29
11.000	10.970	231.5000	370.1000	217.93
13.000	11.956 12.961	197.8700	320.1000	215.36 215.38
14.000	13.956	144.2800	273.3000	
15.000	14.950	123.0900	234.0000	214.80 212.99
16.000	15.944	104.8800		211.25
17.000	16.938	89.2750	172.9000	210.32
18.000	17.932	75.9670	125.9000	210.32
19.000	18.925	64.6650	106.7000	211.04
20.000	19.918	\$5.0820	90.5300	211.97
20.000	20.910	46.9580	76.7800	213.06
22.000	21.903	40.0710	55.1000	214.42
23.000	22.895	34.2290	55.2900	215.68
24.000	23.886	29.2670	46.9900	215.99
25.000	24.878	25.0490	39.9800	218.26
26.000	25.669	21.4610	34.0300	219.71
27.000	26.859	18.4080	28.9600	221.43
28.000	27.850	15.8100	24.6700	223.29
29.000	28.840	13.5970	21.0200	225.36
30.000	29.830	11.7107	17.9300	227.54
32.000	31.806	8.7416	13.1300	234.18
34.000	33.764	6.5698	9.6780	238.74
36.000	35.760	4.9672	7.1500	244.35
38.000	37.735	3.7768	5.3530	248.17
40.000	39.708	2.8871	4.0030	253.65
42.000	41.681	2.2185	3.0230	258.10
44.000	43.652	1.7125	2.2990	262.04
46.000	45.622	1.3262	1.7630	264.53
48.000	47.590	1.0291	1.3630	265.58
50.000	49.558	.7991	1.0570	265.91
52.000	51.524	.6204	.8235	264.97
54.000	53.489	.4811	.6435	262.96
56.000	55.453	. 3726	.5005	261.81
59.000	57.415	.2861	.3900	259.80
60.000	59.377	.2552	.3050	256.21
62.000	61.337	. 1707	.2389	251.36
64.000	63.295	.1305	.1860	2~6.63
66.000	65.253	. 0992 . 0748	.1446	241.20
58.000 70.000	67.209	.0748	.1131	232.49 225.78
70.000	69.165	פנכע.	.0870	£07.78

TABLE IV-4. HYDROSTATIC MODEL ATMOSPHERE

APRIL

STATION	- 723330	VANDE		
Z	OEO. HT.	P	Ō	tv
KM	KM	MB	G/M3	DEG K
.000	.000	1017.4000	1239.0000	286.00
.100	.100	1005.3000	1556.0006	285.64
1.000	.999	902.5 500	1103.0000	293.78
2.000	1.997	799.4800	998.7000	278.98
3.000	8.996	706.6500	8 99.4000	273.70
4.000	3.994	623.0500	810.3000	267.85
5.000	4.991	547.7400	730.2000	261.31
6.000	5.998	479.3000	657.8000	254.15
7.000	6.985	418.8000	591.5000	. +5.69
8.000	7.982	36→ .1coo	530.3000	239.17
9.000	8.979	315.0000	473 .8000	231.67
10.000	9.975	271,4200	421.1000	224.56
11.000	10.970	232.7900	371.1000	218.50
12.000	11.966	198.9700	322.6000	214.73
13.300	18.961	169.8100	276.0000	214.35
14.000	13.956	144.9200	235.3000	214.52
15.000	14.951	153.6400	201.8000	213.49
16.000	15.944	105.4100	173.1000	81.515
17.000	16.938	89.8050	147.8000	211.70
18.000	17.932	76.5100	125.7000	212.00
19.000	18.925	65.2110	106.8000	2:2.73
20.000	19.918	55.6:30	90.6000	213.37
21.000	20.910	47.4640	77.0300	214.65
22.000	21.903	40.5500	65.3900	216.04
23.000	22.895 308.85	31.6810 29.6910	55.5500 47.3000	217.43 218.67
24.000 25.000	24.878	25.4440	40.2600	220.17
26.000	25.869	21.8300	34.2800	221.83
27.000	26.859	18.7540	29.1900	253.81
28.000	27.853	15,1330	29.7500	225.72
29.000	28.840	13.0070	21.7600	227.72
30.000	29.830	11.9072	18.1700	229.83
32.000	31.805	8.9739	13.3100	236.47
74.000	33.784	6.7655	9.0000	241.96
36.000	35.760	5.1319	7.3000	246.57
38.000	37.735	3.9126	5.4700	250.87
40.000	39.708	2.9092	4.1070	256.14
42.000	41.681	2.3:20	3.0960	261.93
44.030	43.652	1.7921	2.35~0	21 G.73
46.030	45,622	1.3:35	1.6223	26.36
48.000	47.590	1.0054	1.4110	267.81
50.000	49.558	.0-57	1.1020	269.10
52.000	51.524	.67.96	.8615	608.13
54.000	53.489	5518.	1978.	80.289
56.000	55.453	. 3975	.5286	263.74
58.000	57.415	. 3078	.4141	260.72
60.100	59.377	.7576	.3240	257.23
62.000	61.337	. 1826	.2551	251.06
€₩.000	63.295	. 1393	.2009	243.21
007.63	65. <i>2</i> 53	. 1053	.1568	235.67
68.000	67.209	.0790	.1215	227.80
70.000	69.165	. 0585	.0941	219.16

TABLE IV-5. HYDROSTATIC MODEL ATMOSPHERE

MAY

	- 723930				
Z	GEO. HT.	P	٥	TV	
101	101	MB	G/M3	DCG K	
.000	.000	1015.9000	1233.0000	297.05	
. 100	.100	1003.9000	1219.0000	296.89	
1.000 2.000	. 999 1.997	800.6900	1091.0000	299.06 293.67	
3.000	2.996	709.1800	988.2000	278.14	
4.000	3.994	626.5100	802.5000	271.97	
5.000	4.991	551.8700	724.5000	265.36	
6.000	5.988	484.5200	653.7000	258.20	
7.000	6.985	423.8000	589.3000	250.54	
B.000	7.982	369.1600	529.7000	242.78	
9.000	8.979	320.1300	474.5000	235.01	
10.000	9.975	276.3300	423.2000	227.46	
11.000	10.970	237.4000	374.8000	220.69	
12.000	11.966	203.1300	328.3000	215.58	
13.000	12,951	173.3600	282.9000	213.46	
14.000	13.956	147.8500	241.3000	213.49	
15.000	14.950	126.0600	206.5000	212.65	
16.000	15.944	107.4100	176.7000	211.76	
17.000	16.938	91.4880	150.8000	211.39	
18.000	17.932	77.9270	128.2000	211.76	
19.000	18.925	66.4110	108.B0C0	212.62	
20.000	19.918	56.6440	92.2500	213.90	
21.000	20.910	48.3650	78.2600	215.31	
22.000	21.903	41.3430	66.4100	216.88	
23.000	22.895	35 . 3840	56 3300	218.61	
24.000	23.896	30.3230	47.9400 HD 0000	220.35	
25.000 26.000	24.878 25.669	26.0190 22.3550	40.8000 34.7700	222.15 223.33	
27.000	26.859	19.2330	29.6530	225.96	
28.000	27.850	16.5680	25.3400	227.79	
29.000	28.840	14.2900	21.6300	229.57	
30.000	29.830	12.3397	18.5900	231.40	
32.000	31.606	9.6512	13.6900	237.27	
34.000	33.784	6.9795	10.1100	242.36	
36.000	35.760	5.2364	7.5340	246.96	
38.000	37.735	4.0419	5.5250	252.33	
40.000	39.708	3.1035	4.2230	259.03	
42.000	41.681	2.3972	3.16?0	263.92	
44.000	43.652	1.9613	2.4360	266.29	
46.000	45.622	1.4501	1.8800	270.88	
48.000	47.590	1.1319	1.4610	271.94	
50.000	49.558	. 8839	1.1420	271.72	
52.000	51.524	. 6896	.8385	263.48	
54.000	53.489	.5369	.7065	266.81	
56.000	55.453	.4169	.5550	263.78	
58.000	57.415	. 3228	.4353	260.39	
62.000 62.000	59.377 61.337	.1912 .1913	.3413	256.26	
64.000	63.295	. 1956	.2685	249.96	
66.000	65.253	. 1936	.2115 .1653	241.78 233.48	
68.000	67.209	. 1099	.1893	222.69	
70.000	69.165	.0603	.0994	213.01	
	JJ. 103	. 0003	.0557	2.3.01	

TABLE IV-6. HYDROSTATIC MODEL ATMOSPHERE

JUNE

XM	STATION	• 723930	VANOE		
1000 1014.7000 1277.0000 243.18	_	GEO. HT.	P		
1.000			_		
1.000					
2.000			_		
3.000			905.0300		
4.000 3.994 630.1300 793.9000 276.49 5.000 4.991 556.2100 718.1000 269.64 6.000 5.989 489.4200 648.7000 262.84 7.000 6.995 429.1400 585.4000 255.33 8.000 7.982 374.8100 527.2000 247.66 9.000 8.979 325.000 473.5000 232.15 10.000 9.975 282.1900 423.4000 232.16 11.030 10.970 243.1700 376.5000 224.96 12.000 11.966 208.6300 331.8000 219.03 13.000 12.961 178.3800 293.1000 219.03 15.000 14.950 129.5600 214.5000 210.43 16.000 15.944 110.1900 183.7000 216.96 17.000 16.938 93.6530 152.2000 210.43 18.000 17.932 79.6300 132.2000 20.901 141.4000 211.95					
5.000 4.991 556.2100 718.1000 269.94 6.000 5.988 489.4200 648.7000 262.84 7.000 6.995 429.1400 585.4000 255.33 8.000 7.982 374.8100 585.4000 247.66 9.000 8.979 325.0000 473.5000 232.16 11.030 10.970 243.1700 376.2000 22.499 12.000 11.966 268.6300 331.8000 219.23 13.000 12.961 178.3800 289.1000 214.92 14.000 13.956 152.1500 299.5000 212.43 15.000 14.950 129.5600 214.500 210.43 16.000 17.932 79.6300 132.2000 209.81 17.000 16.938 93.6530 156.300 209.81 20.000 19.918 57.8130 94.1100 214.95 21.000 21.933 42.2330 67.5200 217.89 23.000 21.933					
6.000 5.988 489.4200 648.7000 262.84 7.000 6.995 429.1400 585.4000 255.33 8.000 7.982 374.8100 527.2000 247.66 9.000 8.979 325.000 423.4000 232.16 11.030 10.970 243.1700 376.5000 224.98 12.000 11.966 208.6300 331.8000 219.03 13.000 12.961 178.3800 283.1000 219.03 14.000 13.956 152.1500 249.5000 212.43 15.000 14.950 129.5600 214.5000 210.43 16.000 15.944 110.1900 183.7000 208.96 17.000 16.938 93.6530 156.3000 209.96 19.000 16.938 93.6530 156.3000 209.96 20.000 19.918 57.8130 94.1100 214.01 21.000 20.910 49.3770 79.6500 215.96 22.000 21.903					
7.000 6.995 429.1400 585.4000 255.39 8.000 7.982 374.8100 507.2000 247.66 9.000 8.979 325.000 473.5000 232.16 11.030 10.970 243.1700 376.5000 232.16 11.030 10.970 243.1700 376.5000 224.98 12.000 11.966 208.6300 331.8000 219.03 13.000 12.961 178.3000 289.1000 214.90 14.000 13.956 152.1500 249.5000 212.43 15.000 14.950 129.5600 214.5000 212.43 15.000 14.950 129.5600 214.5000 20.143 15.000 14.950 129.5600 214.5000 20.16.33 15.000 14.950 129.5600 152.2000 20.915 17.000 16.938 93.6530 152.2000 20.910 19.000 16.938 93.6530 152.2000 20.910 19.000 17.932 79.6300 132.2000 20.910 19.000 18.925 67.7940 111.4000 214.95 20.000 19.918 57.8130 94.1100 214.01 21.000 20.910 49.3770 79.6500 215.96 22.000 21.903 42.2330 67.5000 217.69 23.000 22.895 35.1740 57.3300 219.80 24.000 23.8865 31.0260 48.7900 22.17.69 25.000 24.878 26.6440 41.5700 22.31.55 25.000 24.878 26.6440 41.5700 22.31.62 27.000 26.859 19.7240 30.2700 22.01 28.000 27.850 17.0020 25.9000 232.17 28.000 29.830 12.6757 19.0200 233.12 29.000 29.840 14.6720 22.1900 230.32 30.000 29.830 12.6757 19.0200 230.32 30.000 29.830 12.6757 19.0200 230.32 30.000 39.890 14.6760 22.1900 230.32 30.000 39.890 14.6760 22.1900 230.32 30.000 39.890 14.6760 22.1900 230.32 30.000 39.890 14.6760 22.1900 230.32 30.000 39.890 14.6750 22.1900 230.32 30.000 39.890 14.6750 22.1900 230.32 30.000 39.890 14.6750 22.1900 230.32 30.000 39.890 14.6750 22.1900 230.32 30.000 39.890 14.691 3.7820 247.79 46.000 47.590 11.654 15.5050 271 84 40.000 39.708 31.1968 4.3410 22.844 40.000 47.590 1.1654 1.5050 271 84 50.000 57.415 3.332 4.493 560.05 54.000 59.377 .2571 3.524 22.00 56.000 59.377 .2571 3.524 22.00 56.000 59.377 .2571 3.524 22.00 56.000 59.377 .2571 3.524 22.00 56.000 59.377 .2571 3.524 22.00 56.000 59.377 .2571 3.524 22.00 56.000 59.377 .2571 3.259 24.53 56.000 59.377 .2571 3.259 24.53 56.000 59.377 .2571 3.259 24.53 56.000 59.377 .2571 3.259 24.53 56.000 59.377 .2571 3.259 24.53 56.000 59.377 .2571 3.259 24.53					
8.000 7.982 374.8100 5.77.2000 247.66 9.000 8.979 325.0000 473.50000 232.94 10.000 9.975 282.1900 423.4000 232.15 11.030 10.970 243.1700 376.5000 22.4.90 12.000 11.966 208.6300 331.8000 219.03 13.000 12.961 178.3000 283.1000 219.03 14.000 13.956 152.1500 249.5000 212.43 15.000 14.950 129.5600 214.5000 210.43 16.000 15.944 110.1900 183.7000 209.10 17.000 16.938 93.6530 155.3000 209.81 18.000 17.932 79.6300 132.2000 209.81 18.000 17.932 79.6300 132.2000 209.81 18.000 19.918 57.8130 94.1100 214.01 21.000 20.910 49.3770 79.6500 215.96 22.000 21.903 42.2330 67.5000 217.89 23.000 24.903 42.2330 67.5000 217.89 23.000 23.886 31.0260 48.7900 217.59 25.000 23.886 31.0260 48.7900 217.59 25.000 25.869 22.9090 35.4500 225.15 25.000 26.859 19.7040 41.5700 223.31 26.000 27.850 17.0020 25.9000 228.57 29.000 29.840 14.6720 22.1900 230.32 29.000 31.806 9.5115 14.0300 237.94 74.000 33.784 7.1802 10.7300 237.74 74.000 33.784 7.1802 10.7300 237.74 74.000 33.784 7.1802 10.7300 237.74 74.000 33.789 7.1802 10.7300 237.74 74.000 33.789 7.1803 1.9370 270.58 48.000 37.735 4.1611 5.7910 252.75 49.000 49.558 .9103 1.9590 22.70.58 49.000 35.760 5.4513 7.7350 247.39 38.000 37.735 4.1611 5.7910 252.75 50.000 49.558 .9103 1.9590 227.05 50.000 57.415 3332 .9493 250.05 50.000 57.415 3332 .9493 250.05 56.000 57.415 3332 .9493 250.05 56.000 57.415 3332 .9493 250.07 66.000 57.415 3332 .9493 250.07 66.000 57.415 3332 .9493 250.07 66.000 57.415 3332 .9493 250.07 66.000 57.415 3332 .9493 250.07 66.000 57.415 3332 .9493 250.07 66.000 57.415 3332 .9493 250.07 66.000 67.209 .0045 .11329 223.29					
9 000					
10.000					
11.030					
12.000					
13.000					
14.000					
15.000					
16.000					
17.000 16.938 93.6530 156.300 208.70 18.000 17.932 79.6300 132.2000 203.81 19.000 18.925 67.7940 111.4000 211.95 20.000 19.918 57.8130 94.1100 214.01 21.000 20.910 49.3770 79.6500 215.96 22.000 21.903 42.2330 67.5200 217.69 23.000 22.895 35.1740 57.3300 219.80 24.000 23.886 31.0260 48.7900 221.55 25.000 24.878 26.6440 41.5700 223.31 26.000 25.869 22.9090 35.4500 225.12 27.000 26.859 19.7040 30.2700 226.17 28.000 27.850 17.0020 29.9000 230.32 29.000 29.840 14.6720 22.1900 230.32 30.000 29.830 12.6757 19.0200 232.17 32.000 31.806 <td< td=""><td></td><td></td><td></td><td></td><td></td></td<>					
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28.000 27.850 17.0020 25.9000 228.57 29.000 28.840 14.6720 22.1900 230.32 30.000 29.830 12.6757 19.0200 232.17 32.000 31.806 9.5115 14.0300 237.74 74.000 33.784 7.1802 10.3000 247.73 36.000 35.760 5.4513 7.7300 247.39 38.000 37.735 4.1611 5.7910 252.25 40.000 39.708 3.1998 4.3410 258.49 42.000 41.681 2.4691 3.7820 264.09 44.030 43.652 1.9171 2.5100 268.17 46.000 45.622 1.4933 1.9370 270.58 48.000 47.590 1.1654 1.5050 271.84 50.000 49.598 .9103 1.1740 272.24 50.000 51.524 .7106 .9227 240.36 56.000 57.453 .4303 .	26.000	25.869	22.9090	35.4500	225.12
29.000 29.840 14.6720 22.1900 230.32 30.000 29.830 12.6757 19.0200 232.17 32.000 31.806 9.5115 14.0300 237.94 34.000 33.784 7.1802 10.3000 247.73 36.000 35.760 5.4513 7.7300 247.39 38.000 37.735 4.1611 5.7910 25.25 40.000 39.708 3.1958 4.3410 264.49 42.000 41.681 2.4691 3.7820 264.09 44.000 43.652 1.9171 2.5100 268.17 46.030 45.622 1.4933 1.9370 270.58 49.000 47.590 1.1654 1.5050 271.84 50.000 51.524 7106 .9227 270.36 54.000 53.489 .5537 .7259 267.78 56.000 57.415 .3332 .4493 260.35 60.000 59.377 .571 .2765 <td>27.000</td> <td>26.859</td> <td>19.7240</td> <td>30.2700</td> <td>227.01</td>	27.000	2 6.859	19.7240	30.2700	227.01
30.000 29.830 12.6757 19.0200 232.17 32.000 31.806 9.5115 14.0300 237.94 74.000 33.794 7.1802 10.7000 247.71 36.000 35.760 5.4513 7.7360 247.73 38.000 37.735 4.1611 5.7910 252.75 40.000 39.708 3.1958 4.3410 258.49 42.000 41.681 2.4691 3.7820 264.09 44.000 43.652 1.9171 2.5100 268.17 46.000 47.590 1.1654 1.5050 271.84 50.000 47.590 1.1654 1.5050 271.84 50.000 51.524 .7106 .9227 270.36 54.000 53.489 .9537 .7259 267.78 56.000 57.415 .3332 .4493 260.35 56.000 57.415 .3332 .4493 260.35 60.000 59.377 .2571 .2789		27.850	17.0020	25.9000	22 8. 57
32.000 31.806 9.5115 14.0300 237.94 34.000 33.784 7.1802 10.3000 247.71 36.000 35.760 5.4513 7.7300 247.39 38.000 37.735 4.1611 5.7910 252.75 40.000 39.708 3.1958 4.3410 25.849 42.000 41.681 2.4691 3.7820 264.09 44.000 43.652 1.9171 2.5100 268.17 46.000 45.622 1.4933 1.9370 270.58 48.000 47.590 1.1654 1.5050 271 84 68.000 47.590 1.1654 1.5050 271 84 50.000 51.504 7.106 9227 210.36 54.000 51.504 7.106 9227 210.36 55.000 51.504 7.106 9227 210.36 56.000 57.415 3332 4493 260.35 56.000 57.415 3332 4493 260.35 56.000 59.377 2571 3524 256.07 62.000 61.337 1971 2705 249.53 66.000 65.253 1.132 1.697 234.09 68.000 67.209 0.045 1.1329 223.09				22.1900	230.32
₹¥.000 33.784 7.1802 10.3000 247.71 36.000 35.760 5.4513 7.7360 247.39 36.000 37.735 4.1611 5.7910 252.75 40.000 39.708 3.1998 4.3910 258.44 42.000 41.681 2.4691 3.7820 264.09 44.030 43.652 1.9171 2.5100 208.17 46.030 45.622 1.4933 1.9370 270.58 48.000 47.590 1.1654 1.5050 271.84 50.000 49.558 9103 1.1740 272.24 52.000 51.524 .7106 .9227 270.36 56.000 53.483 .5537 .7039 260.37 56.000 57.415 .3332 .4493 260.35 60.000 59.377 .2571 .3524 286.07 64.000 61.337 .1971 .2795 249.53 64.000 65.253 .1500 .2165					
36.000 35.760 5.4513 7.7360 247.39 38.000 37.735 4.1611 5.7910 252.25 40.000 39.708 3.1958 4.3410 258.44 42.000 41.681 2.4691 3.7820 264.09 44.000 43.652 1.9171 2.5100 268.17 46.000 45.622 1.4933 1.9370 276.58 48.000 47.590 1.1654 1.5050 271 84 50.000 51.524 7.106 9227 270.36 54.000 53.489 .5537 .7259 267.78 56.000 57.453 1.4303 5.717 264.20 56.000 57.415 3.332 4493 266.35 60.000 59.377 .2571 3524 256.07 62.000 61.337 .1971 .2765 246.53 64.000 65.253 .1132 1.697 2.54.09 68.000 67.209 .0845 .1329 223.29					
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56.000 55.453 .4303 .5717 264.00 58.000 57.415 .3332 .4493 260.35 60.000 59.377 .2571 .3524 256.07 62.000 61.337 .1971 .2795 248.53 64.000 63.295 .1500 .2185 240.97 66.000 65.253 .1132 .1697 .234.08 68.000 67.209 .0045 .1329 .223.09					
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64.000 63.295 .1500 .2185 240.97 66.000 65.253 .1132 .1697 23.4.08 68.000 67.209 .0045 .1329 223.09					
66.000 65.253 .1132 .1697 234.08 68.000 67.209 .0045 .1329 223.29					
68,000 67,209 .0845 .1329 823.03	66.C00				
70,000 69,165 .0003 .1015 215,46	68.000				
	70.000	69.165	.0523	.1015	215.46

TABLE IV-7. HYDROSTATIC MODEL ATMOSPHERE

JULY

Z GEO. MT. P D TV MH MH G/H3 DEG K .000 .000 1015.0000 1224.0000 269.65 .100 .100 1003.0000 1209.0000 269.65 .1000 .999 903.1600 1061.0000 296.60 2.000 1.997 804.3000 979.6000 292.33 3.000 2.996 714.8000 870.7000 266.01 4.000 3.994 633.6500 790.4000 279.28 5.000 4.991 560.0000 716.2000 272.39 6.000 5.988 493.3800 647.2000 265.98 7.000 5.998 493.3800 584.000 261.08 8.000 7.982 379.0400 525.900 251.08 9.000 6.979 330.3100 472.5000 236.08 10.000 9.975 286.6100 423.0000 236.08 11.000 10.970 247.5900 376.8000 228.88
.000 .000 1015.0000 1224.0000 289.05 .100 .100 1003.0000 1209.0000 289.04 1.000 .999 903.1600 1061.0000 286.60 2.000 1.997 804.3000 958.6000 293.33 3.000 2.936 714.8600 870.7000 266.00 4.000 3.994 633.6500 790.4000 279.29 5.000 4.991 560.0000 716.2000 275.39 5.000 5.988 493.3800 647.2000 265.59 7.000 5.988 493.3800 647.2000 265.59 8.000 7.982 379.0400 525.9000 251.03 8.000 7.982 379.0400 525.9000 251.03 9.000 8.979 330.3100 472.5000 236.06 10.000 9.975 286.6100 423.0000 236.06 11.000 10.970 247.5900 376.6000 228.08
.100 .100 1003.0000 1209.0000 289.04 1.000 .999 903.1600 1061.0000 286.60 2.000 1.997 804.300 958.6000 293.33 3.000 2.936 714.88000 870.7000 266.60 4.000 3.994 633.6500 790.4000 279.29 5.000 4.991 560.0000 716.2000 272.33 6.000 5.988 493.3800 647.2000 265.59 7.000 5.988 493.3800 647.2000 258.46 8.000 7.982 379.0400 525.9000 2581.09 9.000 8.979 330.3100 472.5000 258.56 10.000 9.975 286.6100 423.0000 236.06 11.000 10.970 247.5900 376.8000 228.88 12.000 11.966 212.9500 333.6000 228.88
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3.000 2.996 714.8000 870.7000 266.01 4.000 3.994 633.6500 790.4000 279.29 5.000 4.991 560.0000 716.2000 275.39 6.000 5.988 493.3800 647.2000 265.39 7.000 6.985 433.200 584.000 258.46 8.000 7.982 379.0400 525.9000 251.03 9.000 8.979 330.3100 472.5000 235.08 10.000 9.975 266.6100 423.0000 236.08 11.000 10.970 247.5900 376.8000 228.88 12.000 11.966 212.9500 333.6000 222.35
4.000 3.994 633.6500 790.4020 279.29 5.000 4.991 560.0000 716.2000 272.39 6.000 5.988 493.3800 647.2000 265.59 7.000 5.985 433.2400 584.0000 258.46 8.000 7.992 379.0400 525.9000 251.09 9.000 8.979 330.3100 472.5000 243.53 10.000 9.975 286.6100 423.0000 236.06 11.000 10.970 247.5900 376.8000 228.88 12.000 11.966 212.9500 333.6000 222.38
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6.000 5.988 493.3800 647.2000 265.59 7.000 6.965 433.2400 584.000 258.46 8.000 7.982 379.0400 525.9000 251.09 9.000 8.979 330.3100 472.5000 243.53 10.000 9.975 286.6100 423.0000 236.08 11.000 10.970 247.5900 376.8000 228.98 12.000 11.966 212.9500 333.6000 222.38
7.000 5.995 433.2400 584.000 258.46 8.000 7.982 379.0400 525.9000 251.03 9.000 8.979 330.3100 472.5000 243.53 10.000 9.975 286.6100 423.0000 236.08 11.000 10.970 247.5900 376.8000 228.68 12.000 11.966 212.9500 333.6000 222.35
8.000 7.982 379.0400 525.9000 251.05 9.000 8.979 330.3100 472.5000 243.53 10.000 9.975 286.6100 423.0000 266.05 11.000 10.970 247.5900 376.8000 228.95 12.000 11.966 212.9500 333.6000 222.35
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12.000 11.966 212.9500 333.6000 222.35
13.000 12.961 182.3800 293.5000 216.46
14.000 13.956 155.5900 256.5000 211.29
15.000 14.950 132.2700 228.3000 207.25
15.000 15.944 112.2100 190.0000 205.75
17.000 16.938 95.1780 160.4000 206.68
18.000 17.932 80.8330 134.8000 208.88
19.000 18.925 68.7860 113.2000 211.62
20.000 19.918 58.6540 95.4200 214.14
21.000 20.910 50.1060 80.6500 216.44
22.000 21.903 42.8730 68.3700 218.44
23.000 22.895 36.7350 58.1100 220.24 24.000 23.886 31.5160 49.4800 221.90
- 24.000 - 23.895 - 31.5150 - 49.4900 - 221.90 - 25.000 - 24.878 - 27.0890 - 42.2000 - 223.46
26.000 25.869 23.2770 36.0100 225.15
27.000 26.859 20.0400 30.7600 226.97
29.000 27.850 17.2730 26.3300 228.53
29.000 28.840 14.9050 22.5800 230.20
30.000 29.830 12.8750 19.3500 231.81
32.000 31.806 9.6516 14.2900 236.70
34.000 33.784 7.2731 10.5500 240.94
36.000 35.760 5.5095 7.8730 2-5.20
38.000 37.735 4.1952 5.8810 249.96
40,000 39,708 3,2135 4,4040 255,66
42.000 41.681 2.4754 3.3250 260.89
44.000 43.652 1.9157 2.5380 264.50
46.000 45.622 1.4870 1.9530 266.80
48.000 47.590 1.1564 1.5110 269.05
50.000 49.558 .8997 1.1780 267.67 52.000 51.524 .6995 .9318 265.87
56.000 53.489 .5456 .7e36 202.69 56.000 55.453 .4195 .5673 269.11
58.000 53.455 .4155 .5675 253.11
60.000 59.377 .2475 .3479 249.24
62.000 61.337 .1684 .2735 241.31
64.000 63.295 .1422 .2125 234.39
66.000 65.253 .1064 .16+0 227.33
60.000 67.209 .0789 .1264 218.65
70.000 69.165 .0579 .0952 212.89

TABLE IV-8. HYDROSTATIC MODEI ATMOSPHERE

AUGUST

STATION	- 723930	YANZY	NOCES AFB	
Z	ŒO. HT.	P	D	TV
KC4	KM	MB	G/#3	DEG K
.000	.000	1014.4000	1219.0000	283.83
. 100	.100	1002.5000	1204.0000	≥30.50
1.000	.933	902.8500	1061.0000	296.58
S.000	1.997	B04.0300	959.2000	535 . 05
3.000	2.936	714.4330	871.3000	285 67
4.000	3.994	633, 2000	790.7000	576 00
5.000	4.331	559.5600	716.1000	272 22
000 3	5.708 6.985	432,9500 432,8300	647.1000	265.39
7.000 8.000	7.962	378.6700	503 6000	2-8.37
9.000	8.979	329.9830	\$25,4000 472,1000	ಪ1.07 243-50
10.000	9.975	296.3200	422.5000	236.04
11.000	10.970	247.3400	376.4000	220.91
12.000	11.966	212.7400	333.3000	222.34
13.000	12.961	185 -5100	293.1000	216.57
14.000	13.956	155.4600	256.1000	211.50
15.000	14.950	132.1900	231.900	207.55
16.000	15.944	112.1600	189.8000	205.87
17.000	16.938	35.1470	160.1000	206.97
18.000	17.932	80.6780	134.6000	209.25
19 000	18.925	68.8010	113.1000	211.97
20.000	19.918	58.6783	95.3800	214.31
21.000	20.919	50.1280	80.7.00	216.74
22.000	21.903	42.6840	68.5:00	218.C8
23.000	22.995	36.7340	58.2300	219.76
2 ⊶ 000	23.886	31.5050	49.5500	221.46
25.000	24.878	27.0520	42 2500	223.05
26.000	25.863	23.2540	36.0700	22° €3
2 1. 000	ટલ ૯૭	23 0133	30.8000	236.38
56 000	27.850	17 2430	∂6:30:00	237 BB
29.000	58 649	14 8720	\$2,5900	\$59,23
30.000	29.830	12.8394	19.3700	230.98
32.000	31.806	9.6141	14.2500	235.€€
₹000	33.764	7.2331	10.5700	539.15
36.000	35.760	5.4658	7.8700	242.78
38.000 40.000	37.735 39.708	4.1507	5.8620	247.52
42.000	41.681	3.1710 2.4360	4.3780 3.3010	253.19 257.99
44.000	43.652	1.8809	2.5030	257.99 262.71
46.000	45.622	1.4573	1.9230	254.94
48.000	47.590	1.1306	1.4920	c54.91
50.000	49.558	.8773	1.1570	265.12
52.000	51.524	6836	.9003	204.06
54.000	53.499	.5272	.7049	261 38
56.000	55.453	.4071	.5518	257.69
50.000	57.415	.3134	.4306	254.58
60.000	59.377	50+5.	. 336-6	249 35
64,000	61.337	. 1830	.2633	2 42 91
64.000	63 233	. 1303	.2056	212 12
86, 700	65.33	.1037	.1579	503.50
643 500	67.239	.0770	.122	600,00
70.000	69.165	. 0%66	₹£3.	513.76

TABLE IV-9. HYDROSTATIC MODEL ATMOSPHERE

SEPTEMBER

STATION	- 723930	VANDE	NBORS AFO	
Z	ŒO. HT.	P	o	TV
K0 4	KP1	HB	G/M3	DEG K
. 000	.000	1013.5000	1215.0000	290.60
. 100	. 100	1001.9000	1201.0000	290.54
1.000	. 99 9	901.9100	1008.0000	294.18
2.000	1.997	802.4200	965.5000	209.52
3.000	2.996	712.3330	976,2000	283.20
4.COO	3.99+	630.6900	793.4000	276.93
5.000	4.991	556.8600	717.0000	270.57
6.000	5.988	490.1920	647.3000	263.83
7.000	6.995	430.0400	584.1000	256.47
8.000	7.982	375.8200	526 1000	2-6.85
9.000	8.979	327.0700	472.5000	241.13
10.000	9.975	283.3700	422.5000	233.69
11.000	10.970 11.966	244.4700 210.0300	375.5000	226.83
12.000			331.0000	221.03
13.000	12.961	179.7700	289.6000	216.08
14.600		153.3700	252.3000	211.77
15.000 15.000	14.950	133.4630	218.2000	208.25
	15.944 16.938	93.9470	187.0000	206.30 20 6.59
17.000			158.4000	
18.000 19.000	17.932	79.7640 67.8350	133.5000	208.22 210.72
			112.1000	
20.000	19.518	57.8030	\$4.4500	213.20
21.000 22.000	20.910 21.903	49.3430 42.1840	79.8300	215.34
23.000	22.595	36.1130	57.6 600 57.4400	217.19 219.00
24.COO	23.886	30.9550	48.8600	220.69
25.000	24.878	26.5650	41.6600	225 12
26.000	25.869	55.8510	35.5500	223.64
27.000	26.859	19.6270	30.3500	225.30
56.000	27.850	16 8980	25.9700	225.71
29.000	28.540	14 5620	22.25.00	209.04
30.000	29 830	12.5603	19.0800	229.36
32.000	31.806	9.3879	14.0800	23+.37
₹4.000	33.704	7.0479	10.4500	237.02
35.000	35.760	5.3147	7.7410	241.31
38.000	37 735	4.0287	5.7610	2+5.79
40.000	39.708	3 0712	9.3010	250.97
42 000	41.681	2 35.52	3.2230	256 65
44.000	43.652	1.8163	2.4370	202.05
45.000	45.622	1.4070	1.6760	2C+.49
48.000	47.530	1.0322	1.4410	265 30
50.000	49.558	.8495	1.1190	265.41
52,000	51.524	.6591	.0731	265.30
54 CCO	53.489	.5113	.5625	263.28
56.000	55.453	. 3359	.5320	261.58
58.000	57.415	. 3060	.4160	258.48
63.000	59.377	.2355	. 3267	253.29
62.000	61.337	. 1903	بلواراح.	248.02
64.000	63 233	- 1370	3 225.	2 40.13
6 6 . 000	65.253	. 1033	. 1553	233.91
68.000	67.209	.0772	.1209	224.50
70.COQ	69.165	- 0571	.0919	218.33

TABLE IV-10. HYDROSTATIC MODEL ATMOSPHERE

OCTOBER

	- 723930	VANCE	ะหละวันย	•
Z KM	GEO. HT.	•	ρ,	TV ~~
_		HB 1015.7000	G- P3	DEG K
.000	.100	1003.8000	1222.0000	287.52
1.000	.100	902.9000	1208.0000	299.46 290.57
2.000	1.937	832.0700	1082.0000	
3.000	2.996	710.9200	979.5000 885.1000	285.57 279.83
9.000 9.000	3.994	628.5500	793.4000	273.90
5.000	4.931	554.1800		267.41
6.000	5.988	487.0600	721.9000	
7.000	6.985	426.5200	65 1.6000 58 7.7000	260.39 252.82
8.000	7.982	372.0000	528.7000	295.14
9.000	8.979	323.0700	473.8CC0	237.54
10.000	9.975	273.3300	473.8000	230.29
11.000	10.970	240.4600		225 80
12.000	11.966	206.1900	374.3000 328.7000	219.55
13.000	12.961	176.2500	265.8000	214.82
14.000	13.956	150.2300		
15.000	14.950	127.8700	247.3000	211.70
16.000	15.944	108.6000	213.2000	208.93 206. 98
17.000	16.938			
19.000		92.1470	155.4000	236.56
19.000	17.932 18.925	78.2190	131.2000	237.58
		66.4790	110.5000	203.64
20.000	19.918	56.5370	93.1400	211.68
21.000	20.910	48.25.30	78.6333	213.79
22.000	21.903	41.2050	66.5800	215.59
23.000	55.632	35.2330	56.4900	217.25
25.000	23.896	30 . 1620	49.0200	218.80
25.000	24.879	25.8510	40.8750	220.36
26.000	25,969	22.1790	34.8600	551 65
27.000	26.859	19.0-60	29.7730	227.87 227.87
29.000	27.850	16 3700	25.4500	224.06
29.000	28.840	14.0810	21.7900	225.14
30.000	29.930	12.1213	19.6700	250.22
32.000	31.806	9.0244	13.7500	231.38
₹ . 000 200	33.784	6.7533	10.1400	234.80
36.000	35.760	5.0790	7.4890	233.05
38.000 40.000	37.735	3.8+10	5.5500	243 93
	39.7CB	2.9235	4.1220	2-9.25
42.000	41.681	2.2393	3.0870	255.69 270.03
44.000	43.652	1.7254	2.3310	260.97
46.000 48.000	45. <i>C22</i> 47.590	1.3359	1.7760	265.09
50.000		1.0375	1.3700	266 . 85
52.000	49.558 51.524	. 6064	1.0650	256.85
54.000	53.489	6208	.6331	265.03
56.000	55.453	. 4865 . 3770	. 6 493 .5057	204.09
56.000	57.415	. 2916	.3357	202.22 203.71
60.000	\$9.377	. 2248	.3037 301 8 .	200.74 19.59
62.000	61.337	.1725	.3102 85 45 .	250.43
64.000	63.295	.1723	.1905	243.30
66.000	65.253	.0395	.1905	235.37
68.000	67.209	. 0744	.1164	225.47
70.000	69.165	. 0552	.0803	220.13
70.000	64.163	. 0336	. 0003	E 20.13

TABLE IV-11. HYDROSTATIC MODEL ATMOSPHERE

NOVEMBER

STATION	- 723930			
Z	OEQ. HT.	P	0	Ťγ
KH	KM	MB	G/M3	DEC K
.000	.000	1017.7000	1235.0000	297.91
.100	.100	1005.7000	1218.0000	297.64
1.000	.999	903.6400	1098.0000	296 . 59
5.000	1.997	801.4500	930.4000	591.92
3.000	2.936 3.994	709.3×00	892.8000 805.4020	276.77 270.89
4.000 5.000	4.991	551.4200	726.6000	264.38
6.000	5.988	483.9100	654.9C0C	257.43
7.000	6.985	423.1300	509.4000	250.10
8.co0	7.982	368.5100	529.2000	242.51
9.000	8.979	319.5700	473.5000	235.11
10.C00	9.975	275.8930	421.7000	227.93
11.000	10.970	237.1200	373.1000	221.39
12.000	11.966	232.9800	327.1000	216.15
13.000	12.961	173.2300	283.5000	212.85
14.000	13.956	147.5500	243.9000	210.73
15.000	14.950	125.4800	209.4000	208.74
16.000	15.944	106.5700	179.2000	207.13
17.000	16.938	90.4460	152,4000	206.72
18.000	17.932	76.7700	129.0000	207.36
19,000	18.925	65.2173	108.8000	200.75
50 ′ 000	19.918	55.4650	91.9500	210.13
21.000	20.910	47.2280	77.7100	211.73
22.000	21.903	40.2630	65.7900	213.21
23.000	22.895	34.3660	55.7400	214.78
24.000	23.906	29.3650	47.3-00	216.11
25.000	24.878	25.1183	40.2300	217.49
26.000	25.869		34.2300	218.66
27,000 28,000	26.859 27.850	18.4340 15.8120	29.1900 24.9000	220.01 221.20
29.000	28.840	13.5763	21.2700	222.38
30.600	29.830	11.5057	18.1700	223.65
32.000	31.806	8 6553	13.3500	228.78
₹4.000	33.784	6.4595	9.78+0	232.95
35.000	35.760	¥ .8×80	7.2030	237.49
38,000	37.735	3.5573	5.3430	₹41.56
40.000	39.708	2.7763	3.9610	247.29
42.000	41.681	2.1200	2.9030	252.48
44.000	43.652	1.6291	2.2230	257.69
46.000	45.622	1.2563	1.6950	261.52
48.CCO	47.590	.9729	1.2960	264.45
50.000	49.558		1.0050	264.92
52.00g	51.524	. 5857	.7873	₹64 . 80
54.000	53.489		.6087	263.26
56.000	55.453			261.83
58,003	57.415		.37.89	250.23
60.000	59.377			257.09
62.000	61.337			252.49 243.05
64.003 65.000	63.295 65.253			235.97
68.000	67.209			225.93
70.000	69.165			218.76
,0.000	US. 103		.0033	C 10.70

TABLE IV-12. HYDROSTATIC MODEL ATMOSPHERE

DECEMBER

Z	STATION	• 723930	VANDENEERG AT 8		
.000	Z		•		TV
1.000					
1.000					
2.000 1.997 800.8100 999.1000 279.17 3.000 3.996 707.7500 899.5000 274.10 4.000 3.996 624.1500 810.3000 258.33 5.600 4.991 548.8400 730.4600 251.79 6.000 5.998 481.0100 657.9000 247.37 6.000 6.995 419.9800 511.4000 247.37 8.000 7.982 365.2000 530.2000 230.94 9.000 8.979 316.1900 473.8000 230.49 10.000 9.975 272.5000 421.3000 230.49 11.000 10.970 233.8600 371.4000 219.35 12.000 11.966 200.0000 343.4000 215.44 13.000 12.361 170.7000 278.1000 213.83 14.000 13.956 145.5500 239.5000 210.67 15.000 14.950 123.9600 205.0000 210.67 16.000 15.944 105.4300 175.8000 209.17 17.000 16.938 89.3650 150.0000 209.17 17.000 18.925 64.6840 167.7000 209.17 20.000 19.918 55.0250 91.1400 210.34 21.000 20.910 46.8580 77.0900 211.76 22.000 21.903 39.960 65.3000 211.75 22.000 21.903 39.960 65.3000 211.76 22.000 21.903 39.960 65.3000 211.76 22.000 23.8866 29.1210 47.4400 215.67 25.000 24.878 24.6990 40.0100 21.176 25.000 25.869 21.3080 34.0500 219.01 26.000 27.850 15.5440 24.77400 215.67 25.000 26.899 18.2510 24.0100 211.76 25.000 27.890 15.5440 24.77400 215.67 25.000 27.890 15.5440 24.7740 220.05 26.000 27.890 15.5440 24.7740 215.67 26.000 39.930 11.5217 18.6500 222.33 32.000 29.830 11.5217 18.6500 222.33 32.000 29.830 11.5217 18.6500 222.33 32.000 29.830 11.5217 18.6500 222.33 32.000 39.830 11.5217 18.6500 222.33 32.000 39.830 11.5217 18.6500 222.33 32.000 39.830 11.5217 18.6500 222.33 32.000 39.830 11.5217 18.6500 222.33 32.000 39.830 11.5217 18.6500 222.33 32.000 39.830 11.5217 18.6500 222.33 32.000 39.830 11.5217 18.6500 222.33 32.000 39.830 11.5217 18.6500 222.33 32.000 39.830 11.5217 18.6500 227.70 36.000 37.735 3.5971 5.2900 242.00 36.000 37.735 3.5971 5.2900 242.00 36.000 37.735 3.5971 5.2900 242.00 36.000 37.735 3.5971 5.2900 242.00 37.750 35.760 4.7692 7.1790 222.05 38.000 37.735 3.5971 5.2900 242.00 38.000 37.735 3.5971 5.2900 242.00 38.000 37.735 3.5971 5.2900 242.00 39.000 39.559 1.5097 7.7865 266.33 39.4000 59.377 2697 2915 255.93 30.000 59.377 2697 2915 255.93 30.000 59.377 2697 2915 255.93 30.000 59.377 2697 2915 255.93					
3.000 2.996 707.7500 899.5000 274.10 4.000 3.994 624.1500 810.3000 268.33 5.000 4.991 548.8400 730.4000 261.79 6.000 5.998 481.0100 657.9300 254.63 7.000 6.995 419.9000 501.4000 247.37 8.000 7.982 365.2000 530.2000 230.94 9.000 8.979 316.1900 473.8000 230.49 10.000 9.975 272.5000 421.3000 225.49 11.000 10.970 233.8600 371.4000 219.35 12.000 11.966 200.0000 323.4000 215.44 13.009 12.961 170.7000 278.1000 213.83 14.000 13.956 145.5500 239.5000 212.55 15.000 14.950 123.9600 205.0000 210.67 16.000 15.944 105.4300 175.8000 209.91 17.000 16.938 893.550 150.0000 209.91 17.000 16.938 893.550 150.0000 209.91 17.000 19.918 55.050 91.1400 210.34 21.000 20.910 46.8580 77.0900 211.76 22.000 21.903 39.9460 65.300 211.76 22.000 21.903 39.9460 65.300 211.76 22.000 21.903 39.9460 65.3000 211.76 22.000 21.903 39.9460 65.3000 211.76 22.000 21.903 39.9460 65.3000 211.70 23.000 22.895 31.0900 55.3800 211.43 23.000 22.895 31.0900 55.3800 211.70 24.000 25.869 21.3080 34.0500 216.60 25.000 26.869 21.3080 34.0500 216.60 27.000 26.869 21.3080 34.0500 218.00 27.000 28.869 21.3080 34.0500 218.00 27.000 28.869 28.2510 29.0300 219.01 28.000 29.800 15.6400 21.1400 221.17 30.600 29.800 15.6400 21.1400 221.17 30.600 39.735 35.540 99.0300 219.01 32.000 49.550 47.692 71.790 220.05 29.000 39.735 35.971 5.2900 227.70 36.000 39.735 35.971 5.2900 227.70 36.000 49.550 47.692 71.790 226.55 50.000 49.550 47.692 71.790 226.55 50.000 55.453 35.21 47.97 236.50 44.000 41.681 2.0875 2.9223 254.25 44.000 41.681 2.0875 2.9223 254.25 44.000 45.652 1.5074 2.1910 261.04 42.000 41.681 2.0875 2.9223 254.25 54.000 55.453 3521 47.97 261.04 56.000 59.577 2697 22915 255.53 56.000 55.453 3521 47.97 261.04 56.000 59.577 2697 22915 255.59 56.000 59.577 2697 22915 255.59 56.000 59.577 2697 22915 255.59 56.000 59.577 2697 22915 255.59 56.000 59.577 2697 22915 255.59 56.000 59.577 2697 22915 255.59 56.000 59.577 2697 22915 255.59 56.000 59.577 2697 22915 255.59 56.000 59.577 2697 22915 255.59 56.000 59.577 2697 22915 255.59					
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5.000 4.991 548.840 730.4000 261.79 6.000 5.998 481.0100 657.900 254.63 7.000 6.995 419.900 571.4000 247.37 8.000 7.982 365.2000 530.2000 230.49 9.000 8.979 316.1900 473.8000 235.49 10.000 19.975 272.500 421.3000 225.36 11.000 10.970 233.850 371.4000 219.35 12.001 11.986 200.0000 323.4000 215.45 13.001 12.961 170.7000 278.1000 213.83 14.000 13.956 145.5500 239.5000 210.67 16.000 13.956 145.5500 239.5000 210.67 16.000 15.944 105.4300 127.3000 210.67 16.000 17.932 76.1040 127.3000 208.21 20.000 19.918 55.050 91.140 20.317 20.000 29.910					
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42.000 41.681 2.0875 2.0223 254.25 44.000 43.652 1.6074 2.1910 261.04 46.000 45.622 1.2451 1.6600 265.04 48.000 47.590 .9679 1.2650 26.07.98 50.000 49.559 .7531 1.0003 267.97 52.000 51.524 .5857 .7826 266.33 54.000 53.489 .4547 .8135 263.71 56.000 57.415 .2721 .3742 228.63 50.000 59.377 .2697 .2915 255.93 62.000 59.377 .1610 .2282 .251.01 64.000 63.295 .1278 .1797 .243.10 66.000 65.253 .0931 .1394 .239.29 68.000 67.209 .0701 .1076 .231.61					
44.000 43.652 1.6074 2.1910 261.04 46.000 45.622 1.3451 1.6660 265.04 48.000 47.590 .9679 1.2650 265.08 50.000 49.559 .7531 1.0000 267.97 52.000 51.524 .8657 .7826 266.33 54.000 53.489 .4547 .8135 263.71 56.000 57.415 .2721 .3742 .28.653 .28 50.000 59.377 .2697 .2915 .255.93 .93 62.000 61.337 .1610 .2282 .251.01 .2721 .2721 .2721 .2721 .2721 .2721 .2721 .2721 .2721 .2721 .2721 .2721 .2721 .2721 .2722 .271.01 .2722 .271.01 .2722 .271.01 .2722 .271.01 .2722 .271.01 .2722 .271.01 .2722 .272.01 .2722 .272.01 .2722 .272.01 .272	-				
N6.000 N5.622 1.391 1.6600 265.04 N8.000 47.590 .9679 1.2660 267.88 50.000 49.558 .7531 1.0000 267.97 52.000 51.524 .8657 .7826 26.337 54.000 53.489 .4547 .6135 263.71 58.000 57.413 .2721 .3742 258.63 50.000 59.377 .2697 .2915 .255.93 62.000 51.337 .1610 .2282 .251.01 64.000 63.295 .1228 .1797 283.10 66.000 65.253 .0931 .1384 .239.08 69.000 67.209 .0701 .1076 .231.61					
48.000 47.590 .9679 1.2650 267.88 50.000 49.558 .7531 1.0000 267.97 52.000 51.524 .5657 .7826 266.33 54.000 51.524 .4957 .6135 263.71 56.000 55.489 .4547 .6135 263.71 56.000 57.415 .2721 .3742 258.69 60.000 59.377 .2697 .2915 255.93 62.000 61.337 .1610 .2282 .251.01 64.000 63.259 .1278 .1797 243.10 66.000 65.253 .0931 .1364 .23.28 66.000 67.299 .0701 .1076 231.61					
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\$\frac{50}{56.000}\$ \$\frac{53.489}{55.453}\$ \$\frac{.561.71}{.56.000}\$ \$\frac{55.453}{55.21}\$ \$\frac{.4797}{.4797}\$ \$\frac{.561.18}{.58.000}\$ \$\frac{57.415}{57.415}\$ \$\frac{.2721}{.2791}\$ \$\frac{.2781}{.2791}\$ \$\frac{.2781}{.275.553}\$ \$\frac{.282}{.2751.01}\$ \$\frac{.282}{.2751.01}\$ \$\frac{.2782}{.2751}\$ \$\frac{.2795}{.2751}\$ \$\fr					
56.000 55.453 .3521 .4797 261 18 58.000 57.415 .2721 .3742 .258.63 60.000 59.377 .2097 .2915 .255.93 62.000 61.337 .1610 .2282 .251.01 64.000 65.295 .128 .1797 .43.10 66.000 65.253 .0931 .1384 .239.28 68.000 67.209 .0701 .1076 .231.61					
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	66.000	65.253	. 0931	. 1 384	239.09
70.000 69.165 .0523 .0825 ?25.68	6A . QUD	67.209	.0701	.1076	
	70.000	69.165	.0523	.08≥5	225 68

TABLE IV-13. HYDROSTATIC MODEL ATMOSPHERE

ANNUAL

	- 723930		HEER OFFE	
Z	OEO. HT.	•	C	TV
- 101	KH	16	0.43	DEC K
.000	.000	1016.6000	10 sc . c c n 0	297.EC
. 100	.100	1004.6300	1210.0.0	207.45
1.000	.999	805 3800	1.01.0000	∂88. •5
2.003	1.937	801 40CU		.493. 6 4
3.000	5 736	709.9000	809.9.	.78.20
W.000	3.934	627.1700	803.0CL.	272.08
5.000	4.991	552.4700	725.0000	265 45
5.000	5.998	485.0900	653.9000	258.42
7.000 8.000	6.985 7.982	424.3700 369.7700	569.0000 529.2000	टा. 00 ४४. इस्ट
9.000	8.979	320.8300	473.9C00	235.84
10.000	9.975	277.0700	422.3000	228.55
11.000	10.970	238.2500	373.6000	222.17
12.000	11.966	204.1100	376.9000	217.54
13.000	12.961	174.4100	282.8000	214.86
14.000	13.956	148.7800	243.6000	212.73
15.C00	14.950	126.7100	209.8000	210.43
15.000	15.944	107.7500	179.8000	208.76
17.000	16.938	91.5570	153.0000	₹68.45
18.000	17.932	77.0310	129.6303	503.53
19.000	18.925	66.2190	109.4000	210.78
20.000	19.918	56.4100	92.5300	212.38
21.000	20.910	48.1160	78.3000	214.07
22.000	£1.903	41.0910	65.4100	215.56
23.000	22.895	35.1330	56.3800	217.08
₽.000	23.886	30.0700	47.9700	218.37
25.000	24.878	25.7660	40.7800	820.08
26.000	25.869	22.1030	34.7500	221.57
000 . 27	25.859	18.9⊌30	29.62 00	223.24
28.000	27.850	16.3210	25.3100	224 . 66
29.000	28.840	14.9470	21.6300	22 6 . 2 2
33.000	29.830	12.1028	18.5100	227.84
32.000	31.806	9.03 <i>3</i> 2	13.5700	233.68
₹+.000	33.784	6.7936	9.9350	238.18
36.000	35.760	5.1238	7.4020	242.94
39.000	37.735	3.8922	5.5100	247.88
40.000	39.708	2.9744	4.1190	253.38
42.000	41.681	2.2062	3.0990	258.91
44.000	43.652	1.7668	2.3520	263.57
45.000 49.000	45.622	1.3704	1.8060 1.3980	266.27
50.000	47.530 49.558		1.0990	267.34
52.000	51.524	. 8291 . 64 34	.0510	265.31 265.31
54.000	53.489	.4990	.6657	263.06
56.000	55.453	.3862	.5200	260.54
58.000	57.415	.2962	.4053	257.84
60.003	59.377	.2296	.3168	25. 27
62.000	61.337	. 1759	2464	248.47
64.000	63.295	.1338	19-9	2.0 %
66.000	65.253	.1010	.15:2	271.41
58.000	67 209	.0755	.1176	125 21
70.000	69.165	. 0559	.0897	218.45

APPENDIX A

EXAMPLES OF WIND STATISTICS FOR VANDENBERG AFB, CALIFORNIA (Data base 32-70 km altitude from Point Mugu, CA)

Appendix A gives some examples of graphical displays of wind statistics that can be derived from the statistical parameters presented in table I. These illustrations should aid the user of the RRA to understand the functional relationships of the probability wind models and, thus, to develop an appreciation of the powerful properties of the bivariate normal probability distribution function.

All illustrations for this appendix are derived from the five wind component statistical parameters from table I.1 for January and table I.7 for July for eight selected altitudes. These selected altitudes are 4, 12, 20, 30, 40, 50, 60, and 70 km.

1. Windspeed (Figures A-1 through A-4)

The five wind components from table I are used as inputs to the generalized Rayleigh probability density function, equation (29), and then integrated as indicated by equation (30) to obtain the probability distribution function for windspeed. The derived distribution functions for windspeed are shown in figures A-1 through A-4 on the normal probability scale.

2. Frequency of Wind Direction (Figures A-5 through A-20)

The derived frequencies for wind direction shown in figures A-5 through A-20 were obtained using the five wind component parameters from tables I.1 and I.7 as input values in equation (35). The limits of integration (performed numerically) are over the 22.5-degree interval for each of the 16 compass points. These graphs give the percentage frequency that the wind will blow from the direction intervals.

3. Mean Wind Components and 80th Interpercentile Range of Wind Components (Figures A-21 through A-36)

The wind component means with respect to any orthogonal axes are obtained by using the zonal and meridional mean wind components in equations (44) and (45). These component means form the circles shown in figures A-21 through A-36. Further, the zonal and meridonal wind component variances and correlation coefficients are used in equations (46) and (47) to obtain the variances with respect to any orthogonal axes. These rotated component variances and the rotated component means are used in equation (8) to obtain the 80th interpercentile range of wind components and are then illustrated in figures A-21 through A-36.

4. Probability Ellipses (Figures A-37 through A-52)

Using the five wind component parameters from tables I.1 and I.7 and p = 0.50, p = 0.95, and p = 0.99 as input values to equation (13), the wind

probability ellipses shown in figures A-37 through A-52 were obtained by computer graphics. The statistical inferences are, for example, that 50 percent of the wind vectors lie within the smaller ellipse and 99 percent of the wind vectors lie within the outer ellipse. These probability ellipses are illustrated using the standard meteorological coordinate system explained in section I.B.1.

5. Conditional Windspeed Given the Wind Direction (Figures A-53 through A-68)

The five wind component parameters from table I.1 and table I.7 are used to evaluate the conditional probability distribution function, equation (41). Figures A-53 through A-68 show interpolations of the conditional function made to obtain the 5th, 15th, 50th (median), 85th, 95th, and 99th conditional percentile values of windspeed, given the wind directions. The conditional mean windspeed, given the wind direction, is obtained from equation (40). The conditional mode (most probable) windspeed, given the wind direction, is obtained from equation (38). The conditional mean windspeed and the conditional windspeed modal value, given the wind direction, are also shown in these figures. For some figures, the conditional windspeed values are invalid for the given wind direction near 270° (from the west). This is caused by the lack of computational precision in evaluating equations (40) and (41) when the arguments for the Gaussian probability distribution have large negative values, i.e., when the coefficients (b/a) become less than -4 in these equations.

This appendix contains only a few of the many options in presenting wind statistics illustrations.

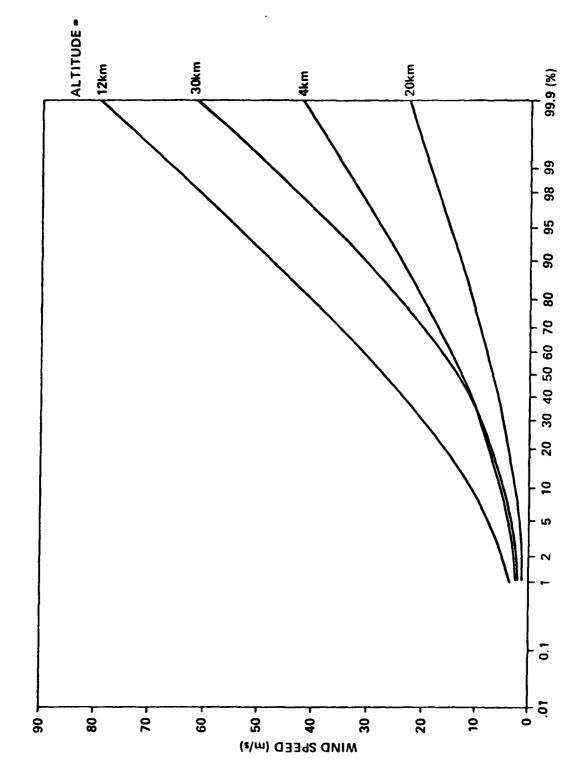


Fig. A-1. Rayleigh PDF of wind speed, Vandenberg AFB, January.

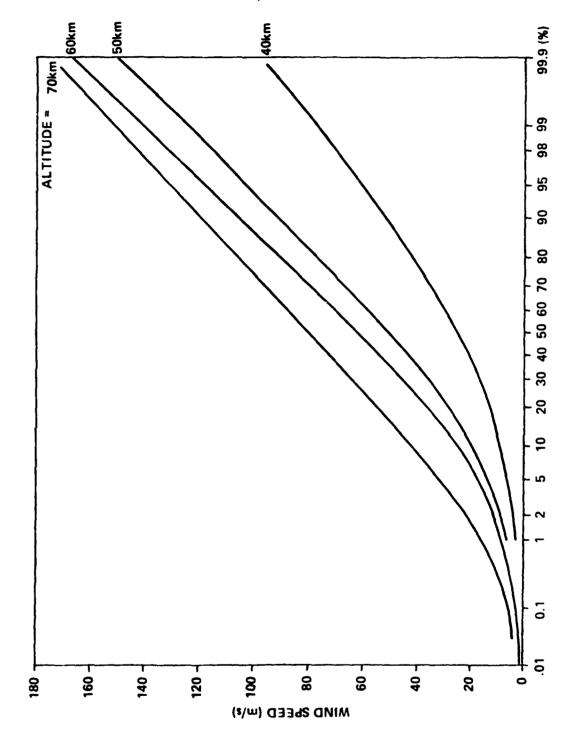


Fig. A-2. Rayleigh PDF of wind speed, Vandenberg AFB, January.

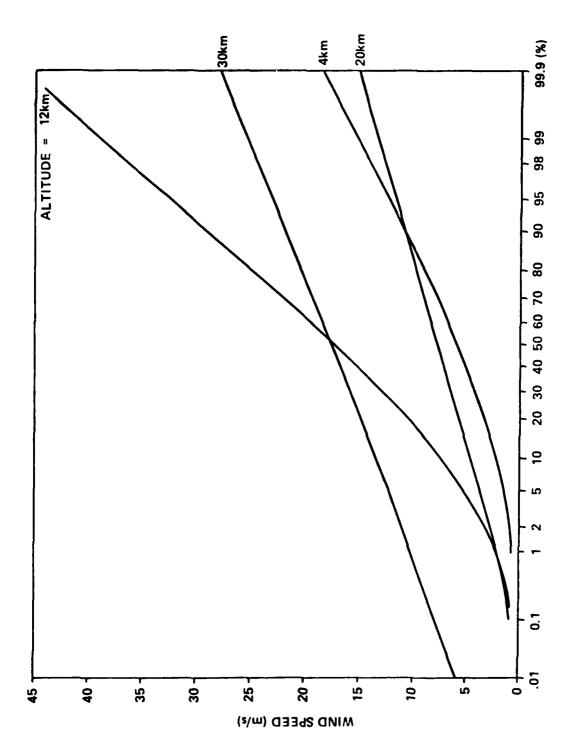


Fig. A-3. Rayleigh PDF of wind speed, Vandenberg AFB, July.

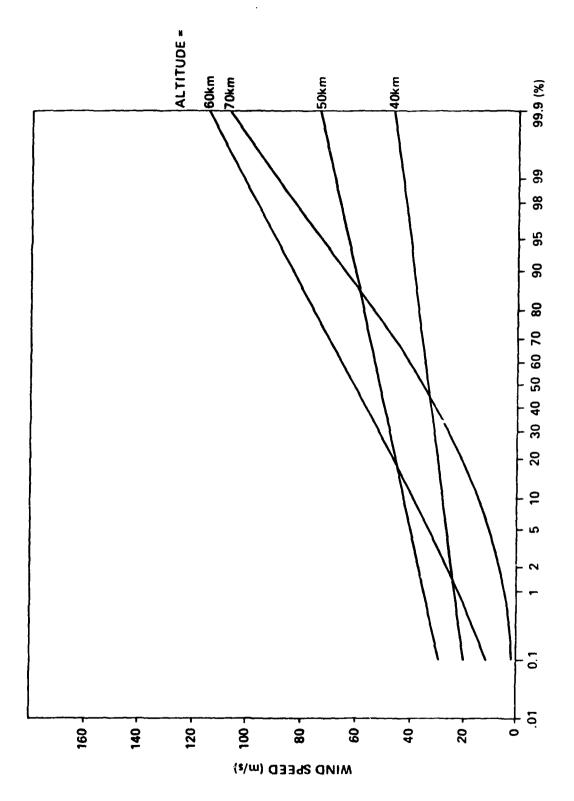


Fig. A-4. Rayleigh PDF of wind speed, Vandenberg AFB, July.

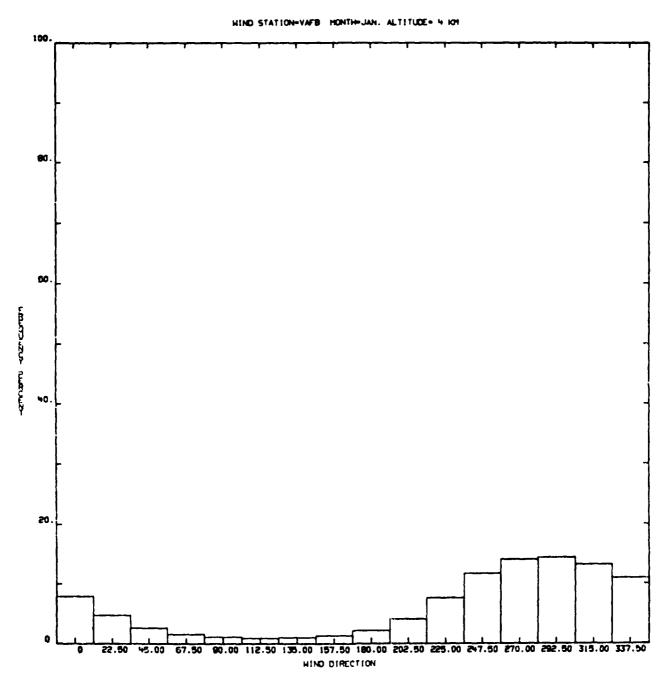


Fig. A-5

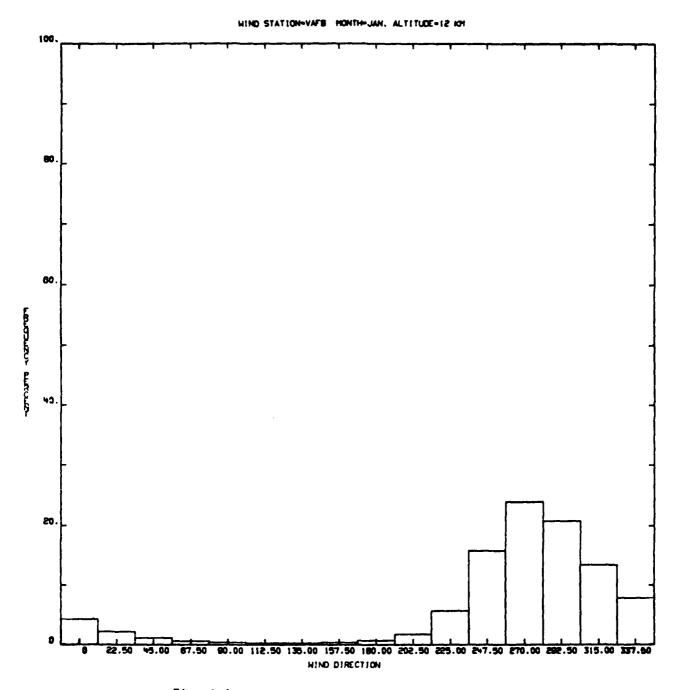


Fig. A-6

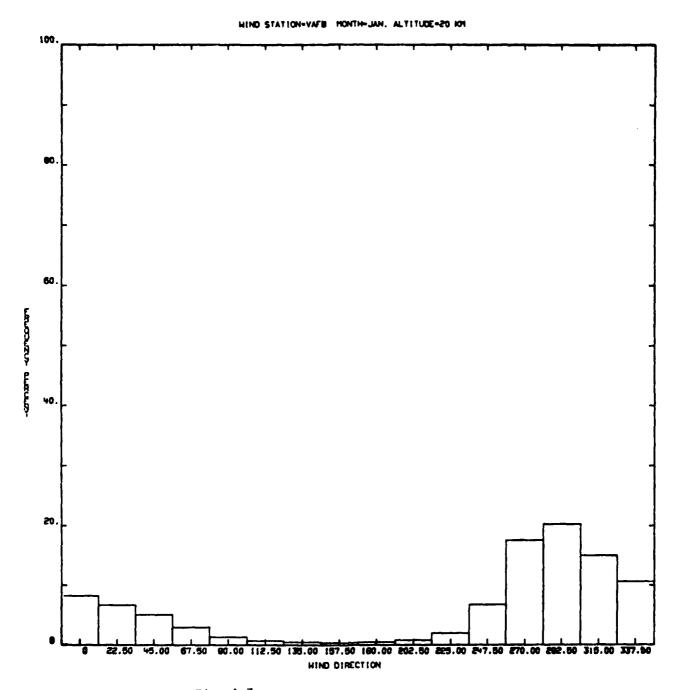


Fig. A-7

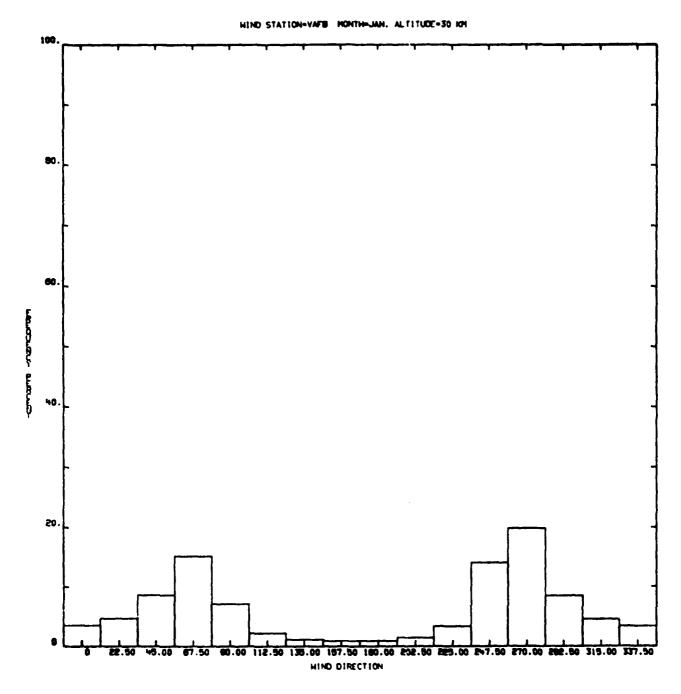


Fig. A-3

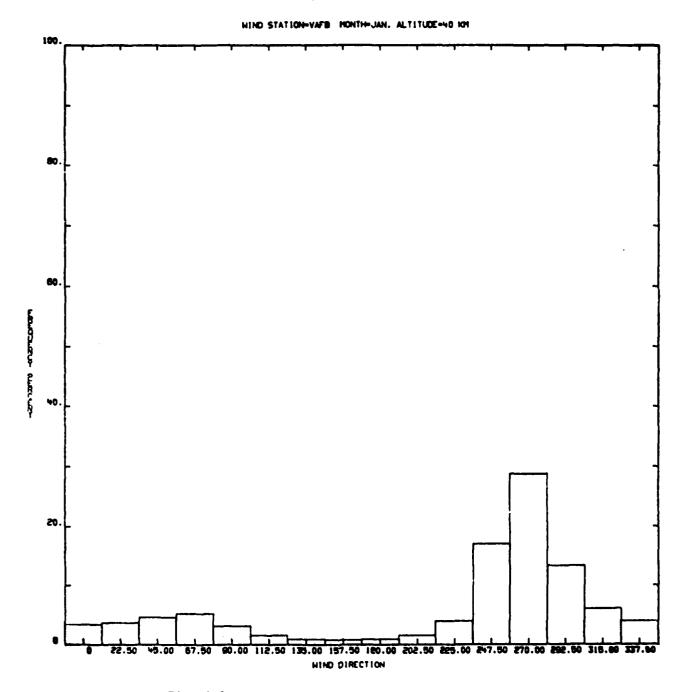


Fig. A-9

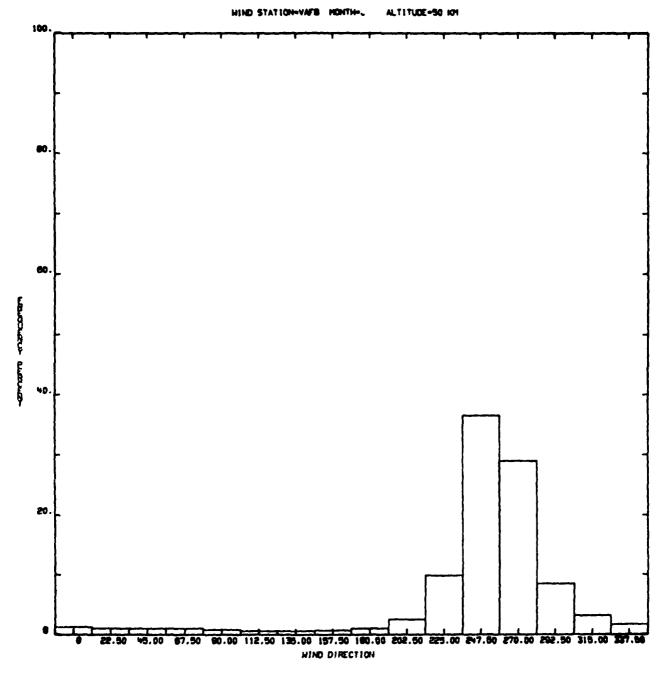


Fig. A-10

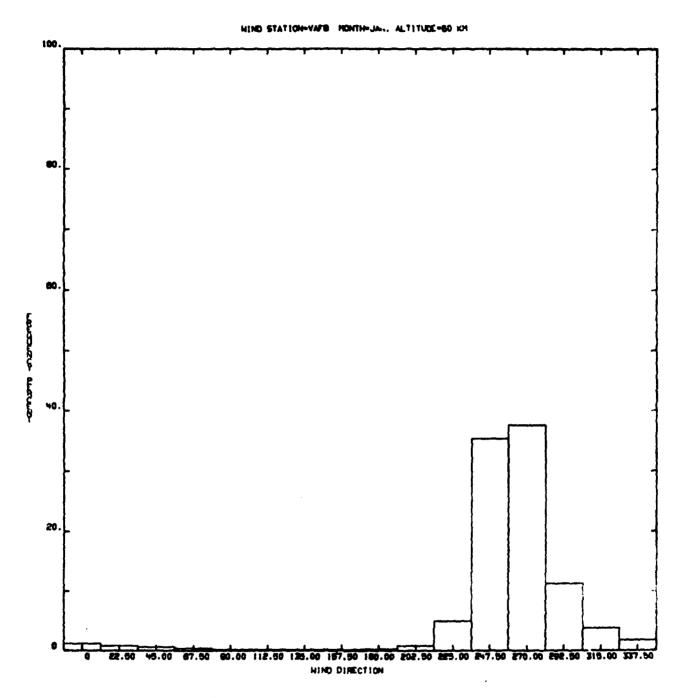


Fig. A-11

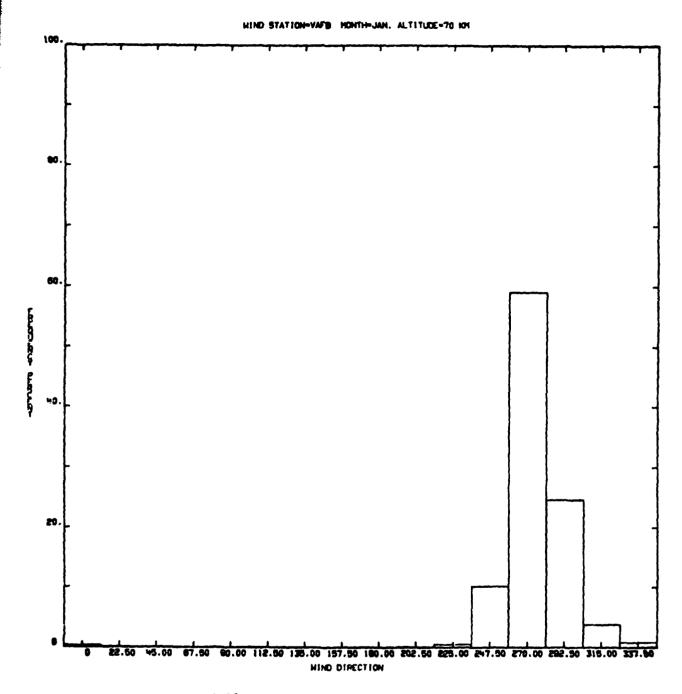


Fig. A-12

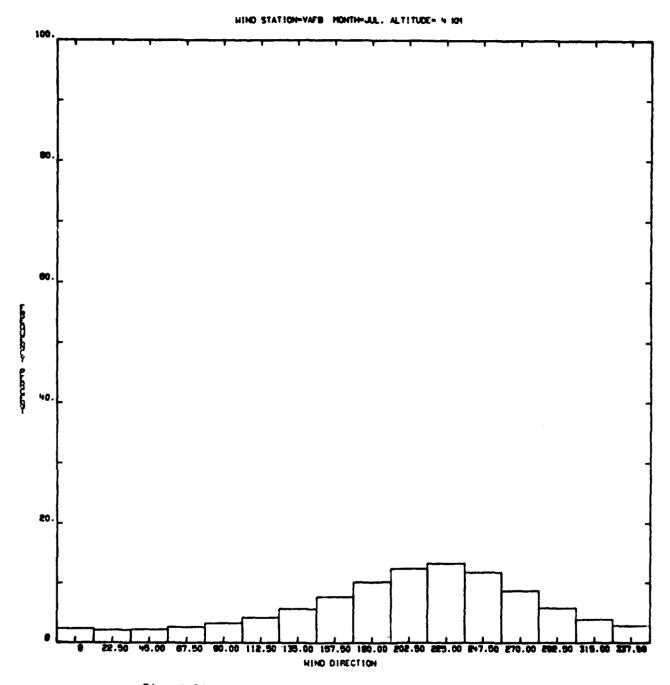


Fig. A-13

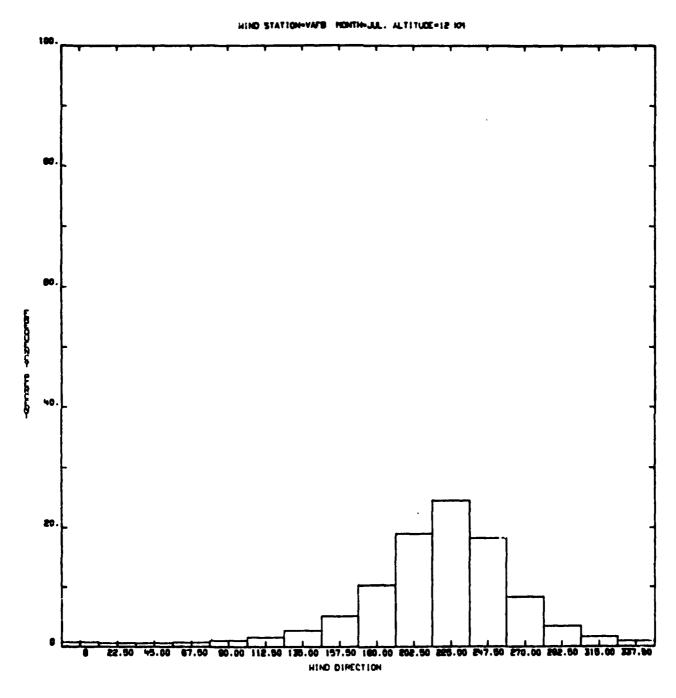


Fig. A-14

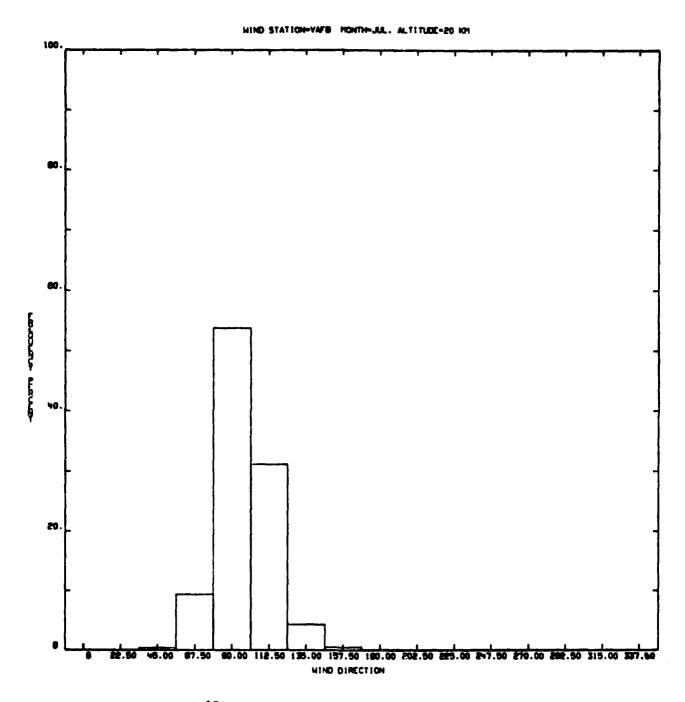


Fig. A-15

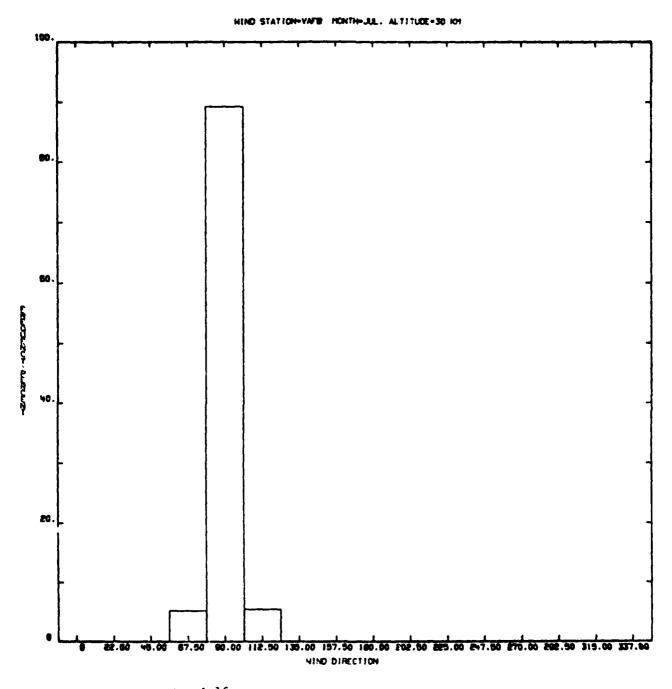


Fig. A-16

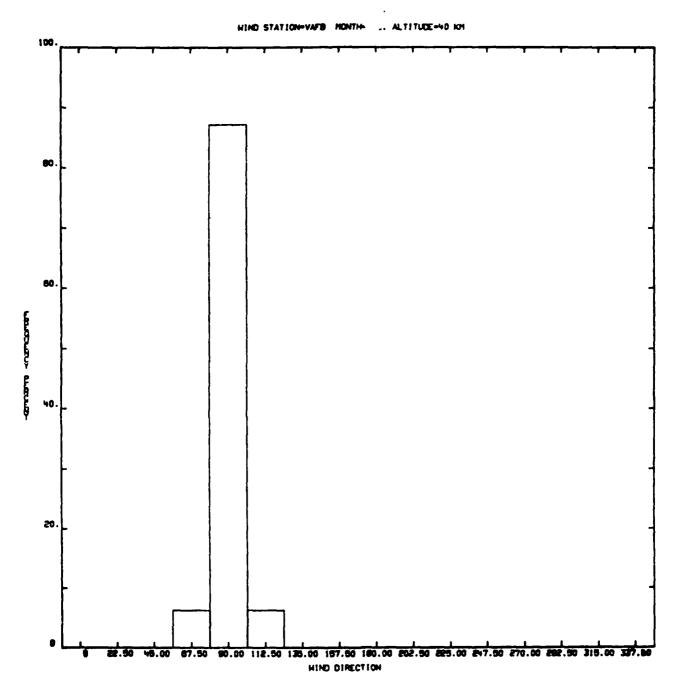


Fig. A-17

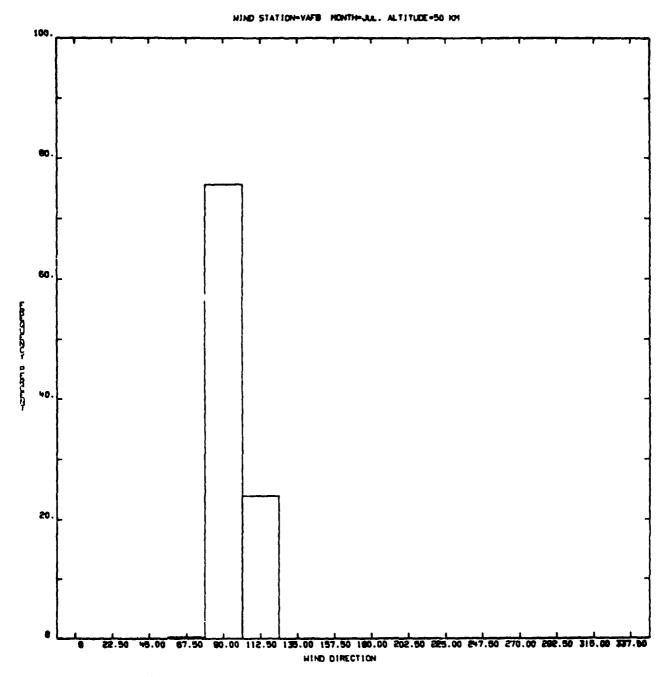


Fig. A-18

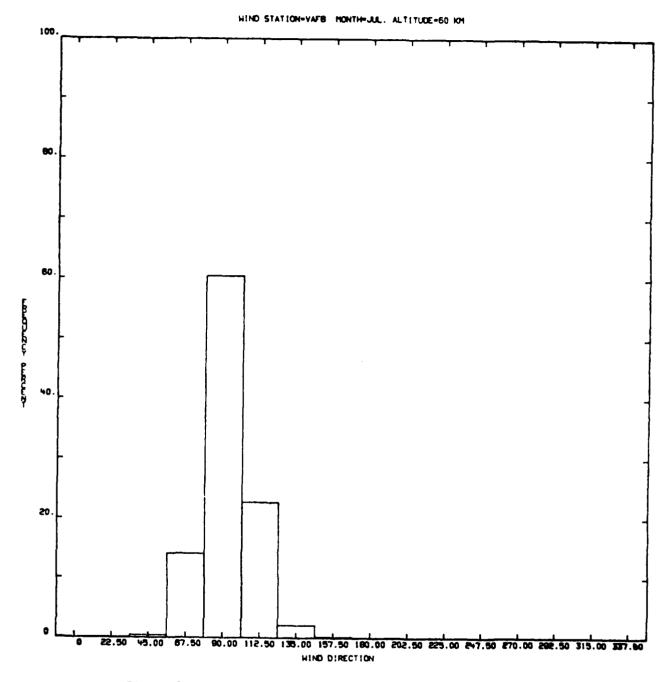


Fig. A-19

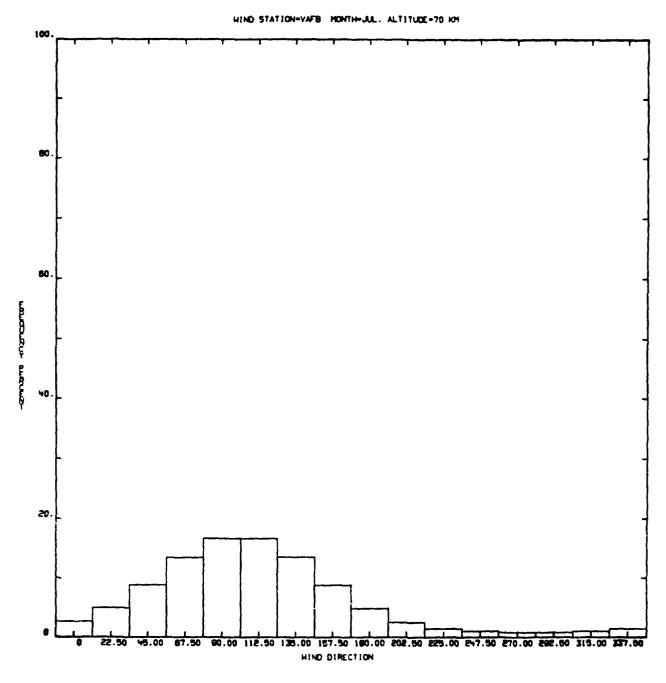


Fig. A-20

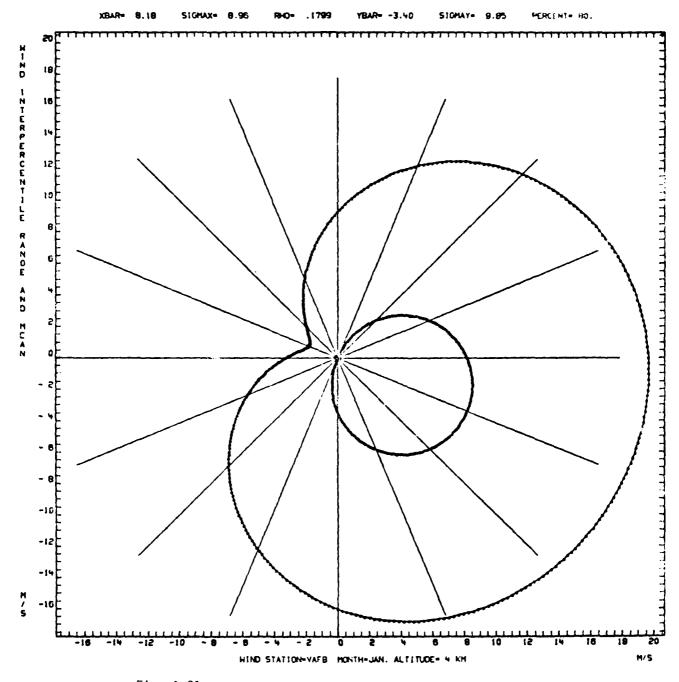


Fig. A-21

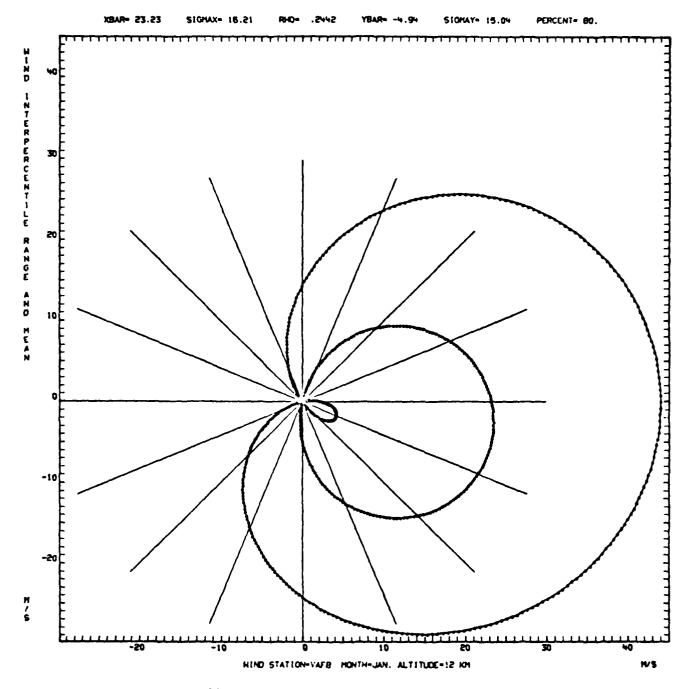


Fig. A-22

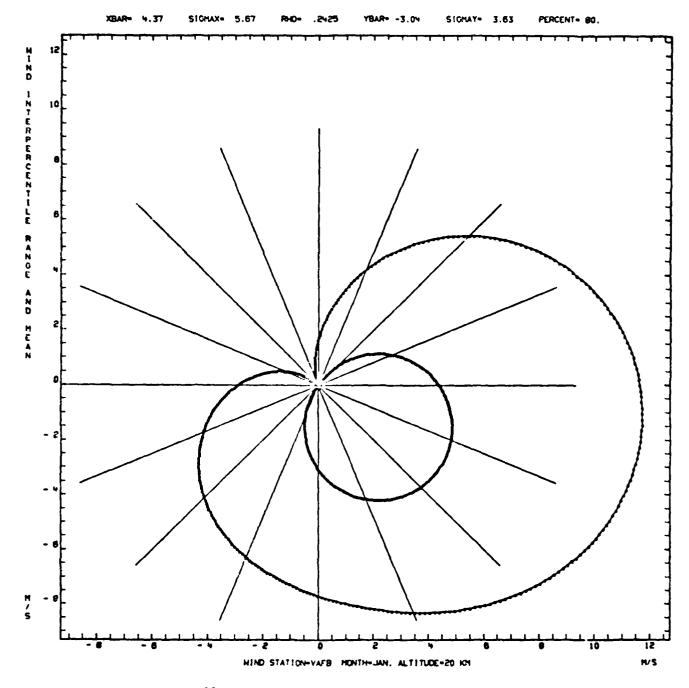


Fig. A-23

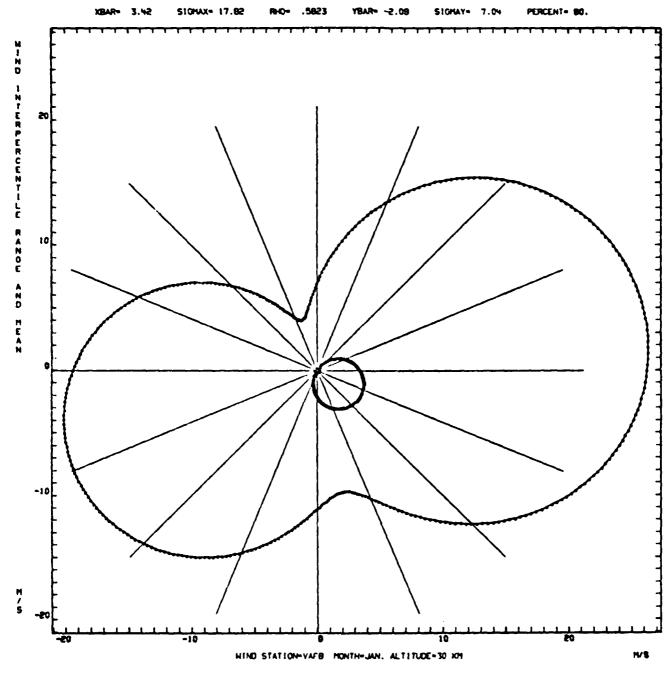


Fig. A-24

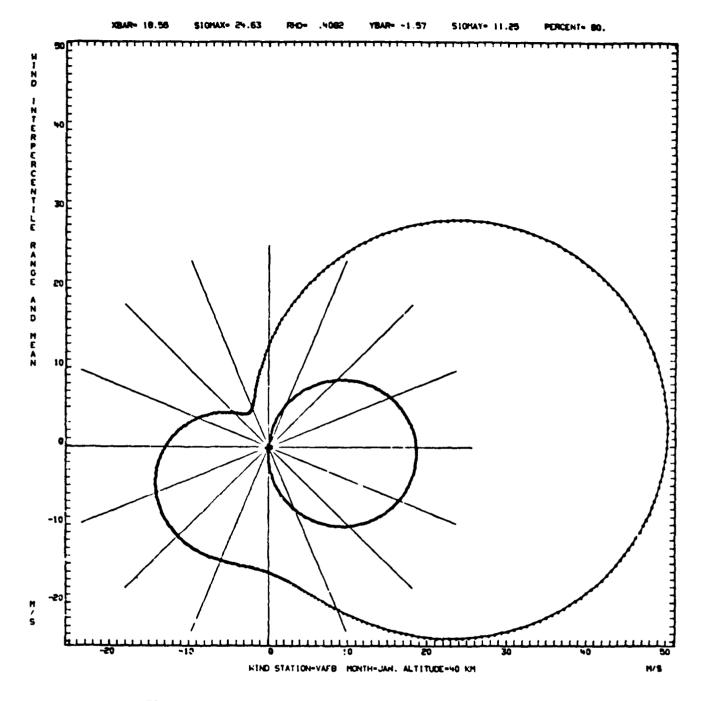


Fig. A-25

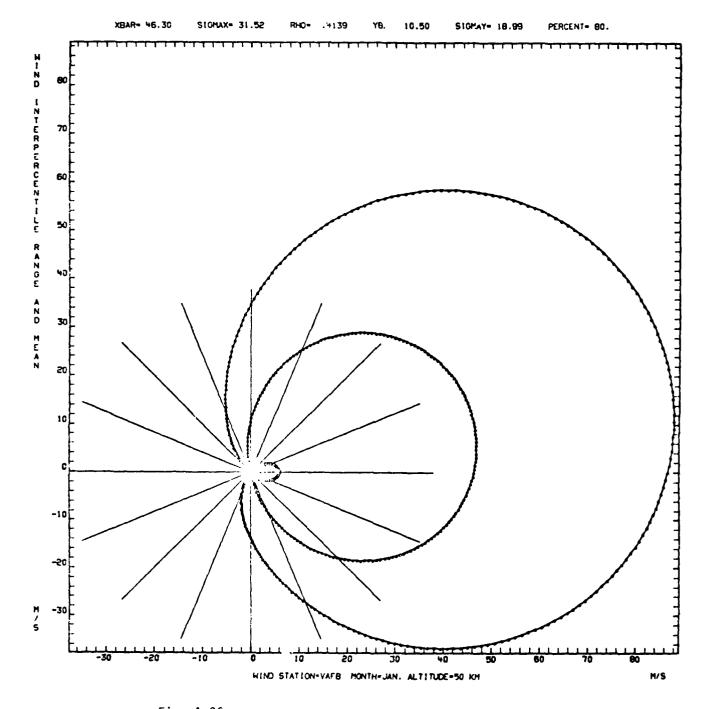


Fig. A-26

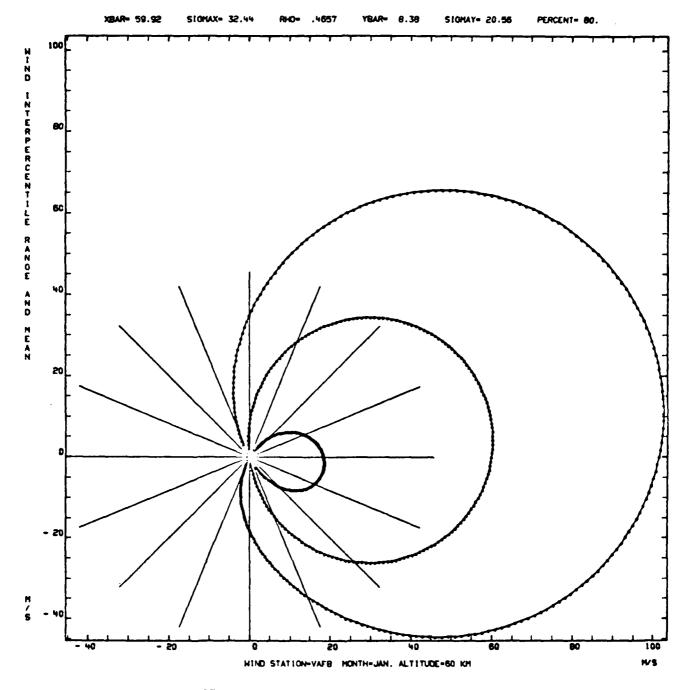


Fig. A-27

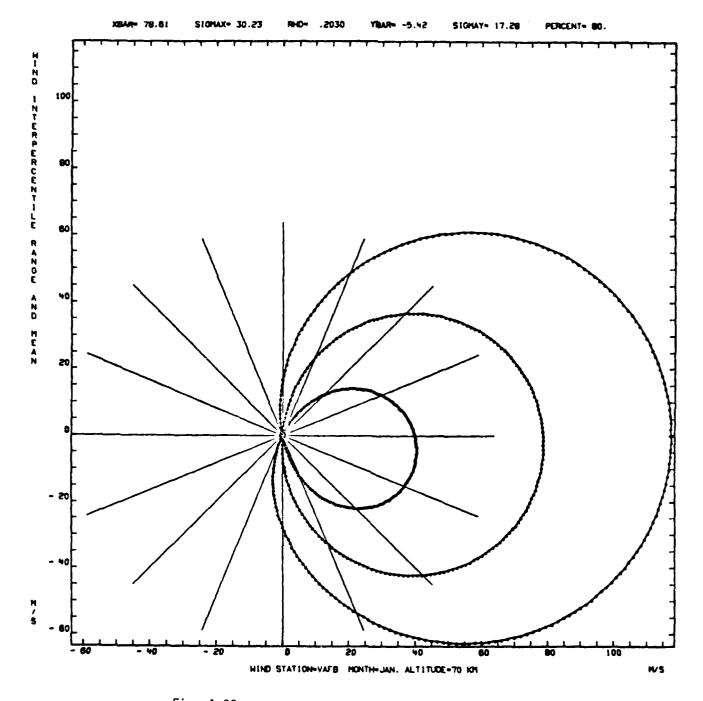


Fig. A-28

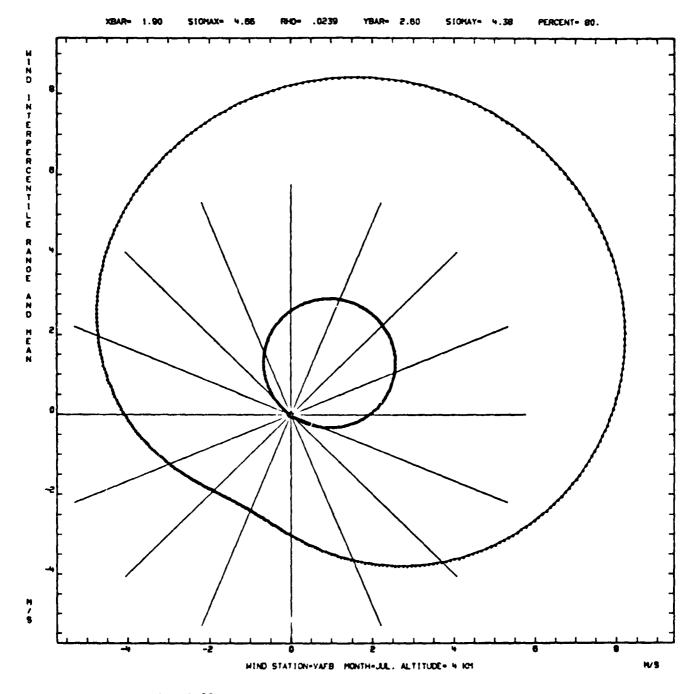


Fig. A-29

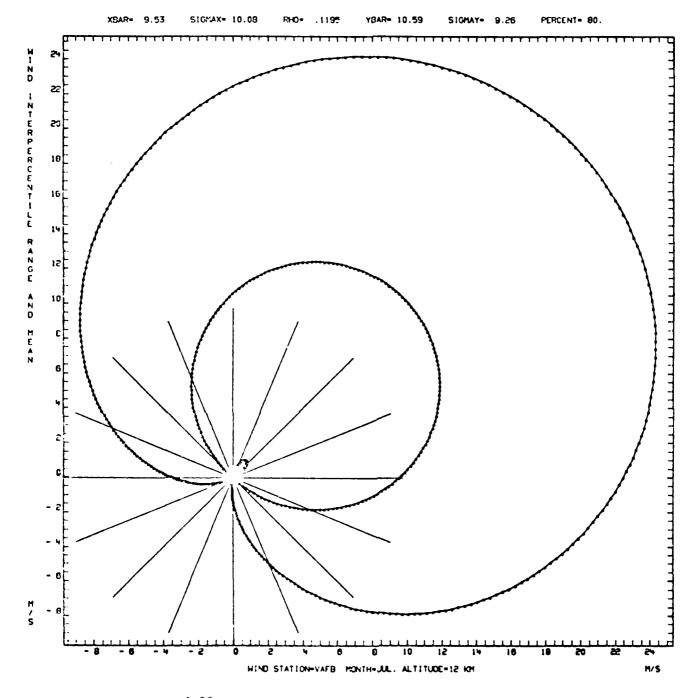


Fig. A-30

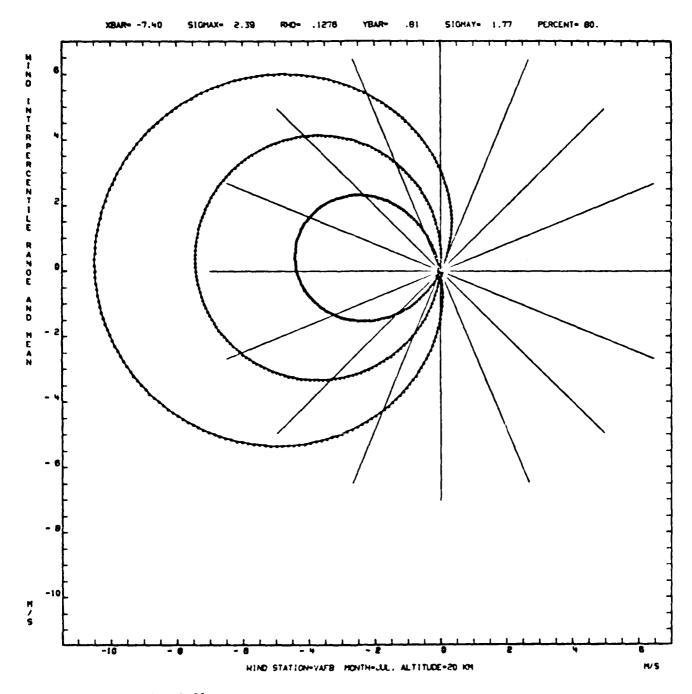


Fig. A-31

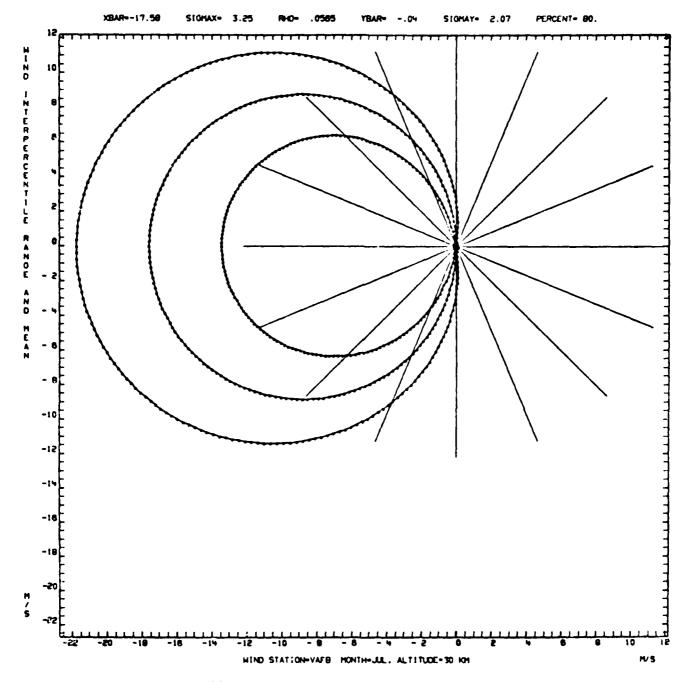


Fig. A-32

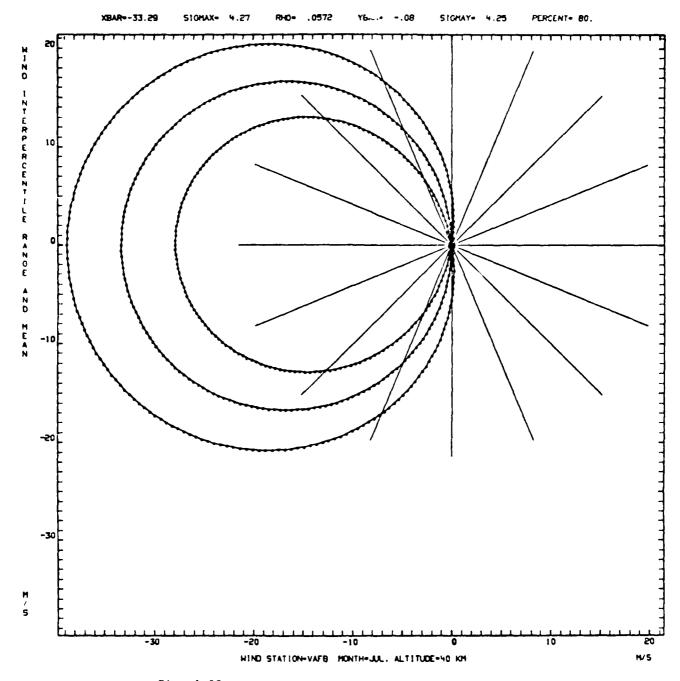


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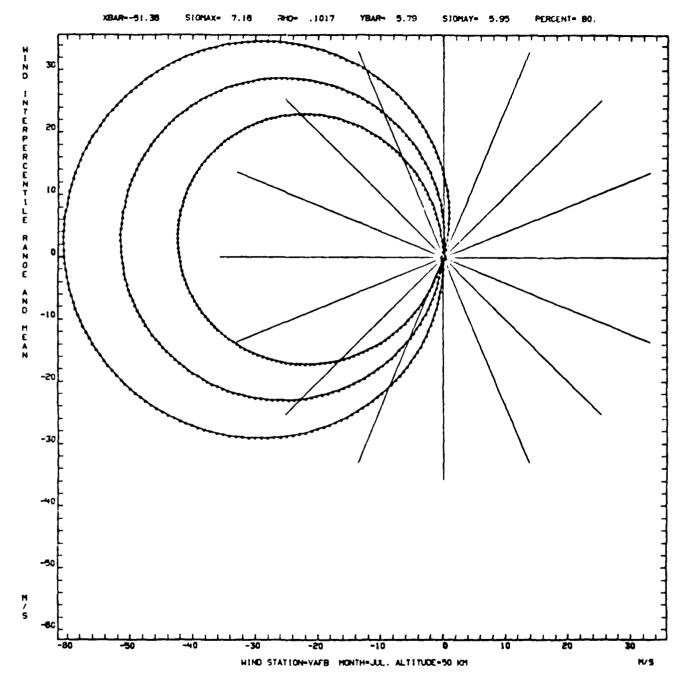


Fig. A-34

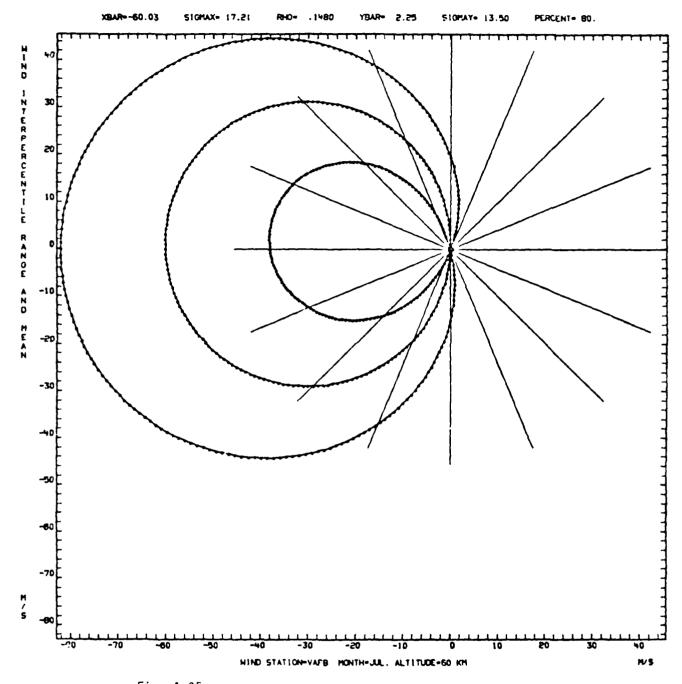


Fig. A-35

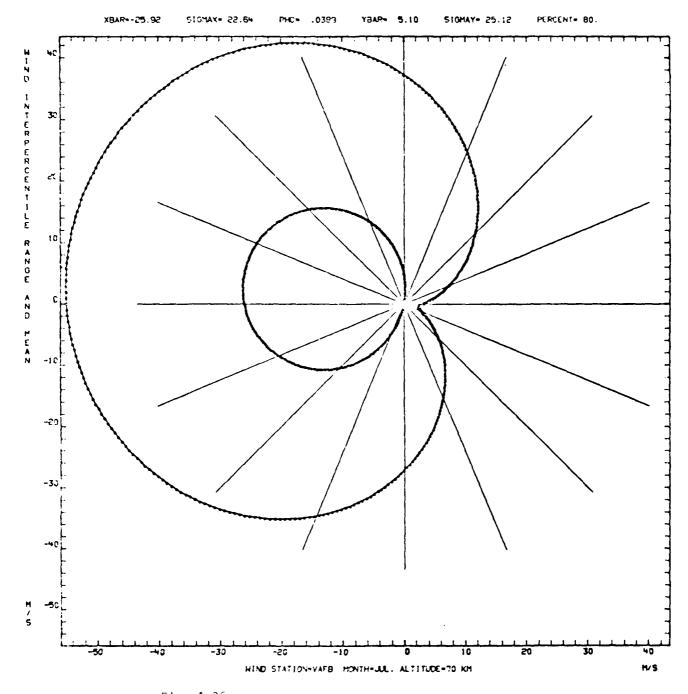


Fig. A-36

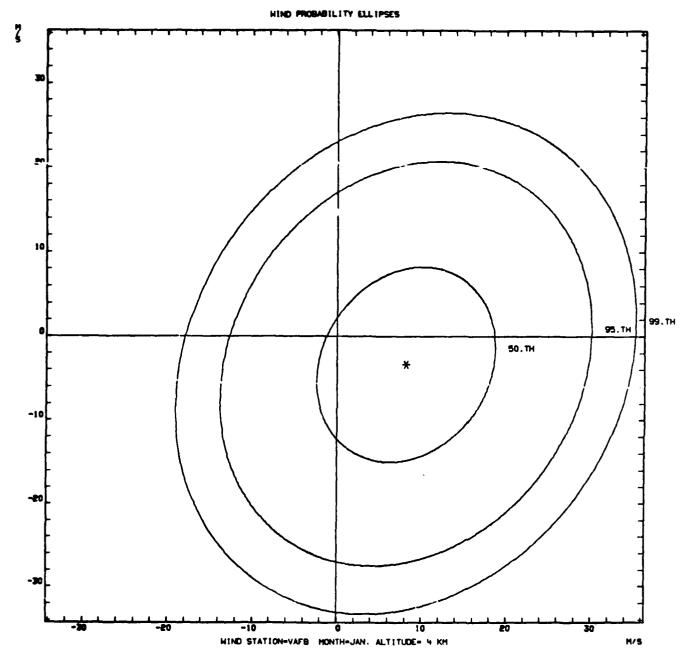


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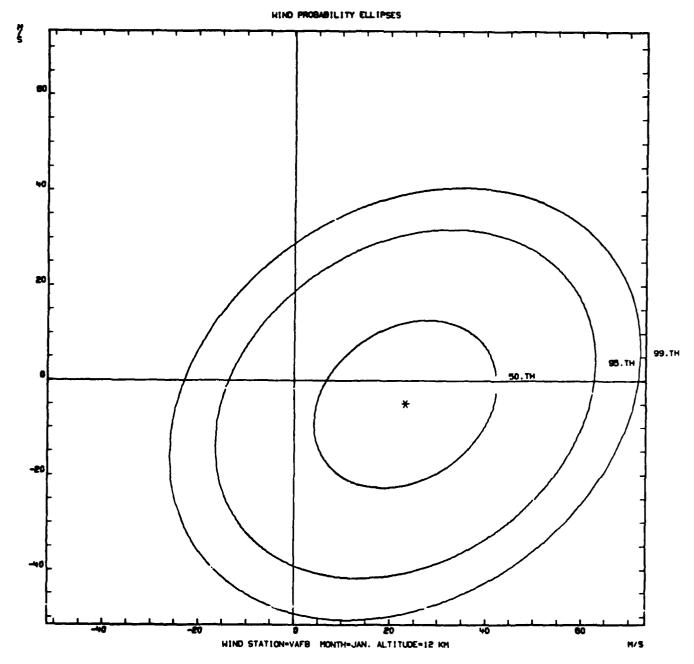


Fig. A-38

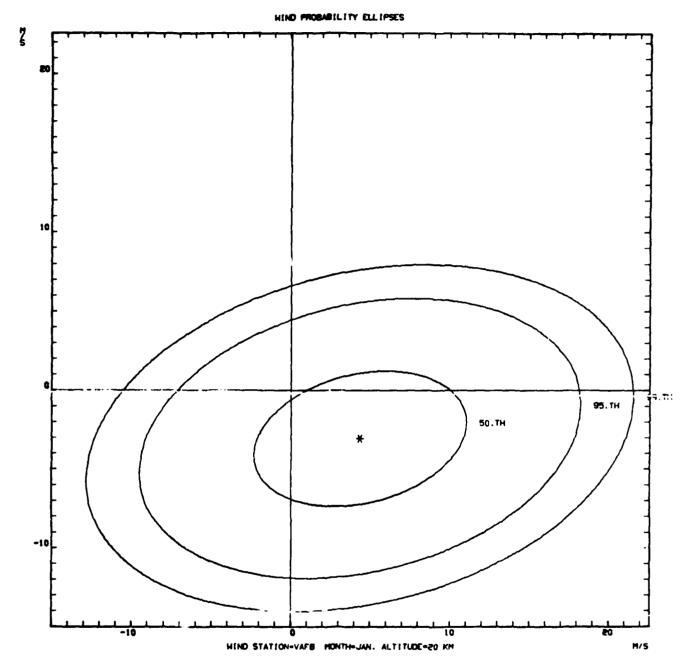


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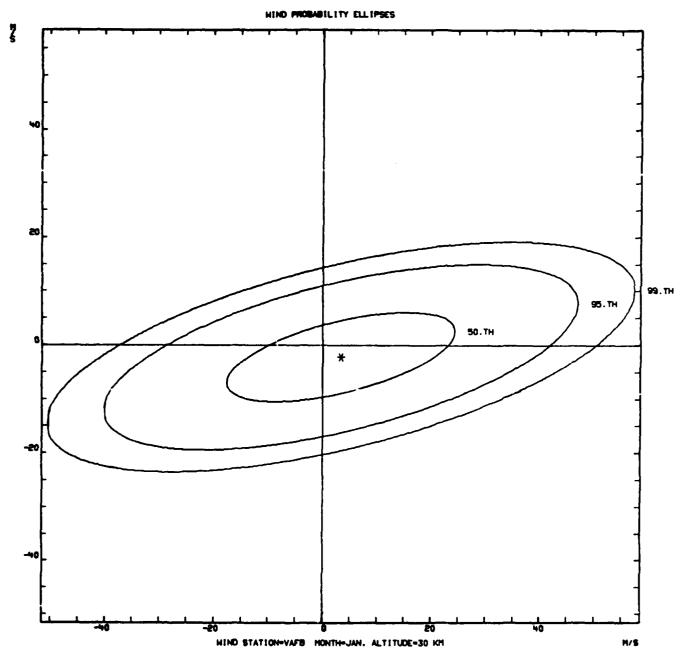


Fig. A-40

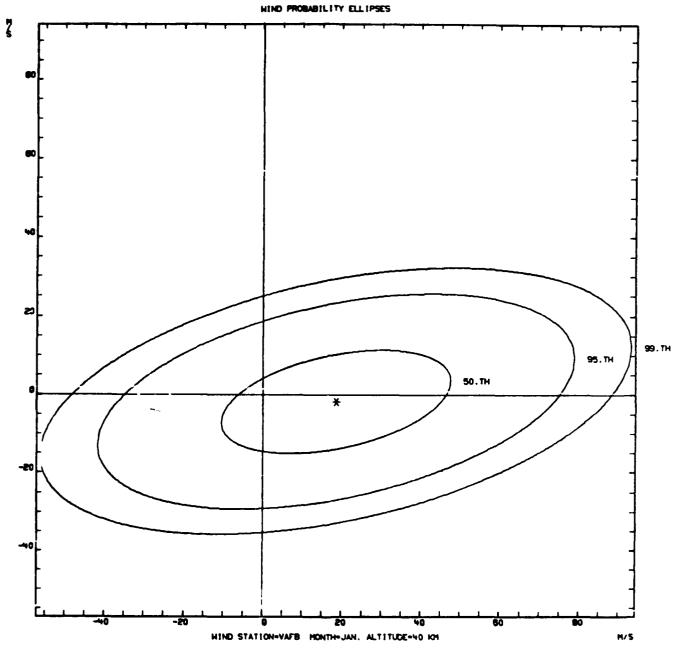


Fig. A-41



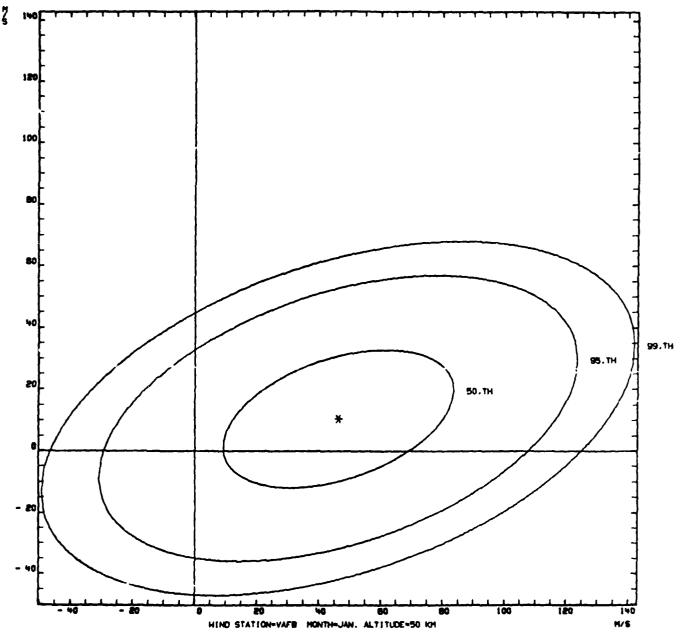


Fig. A-42

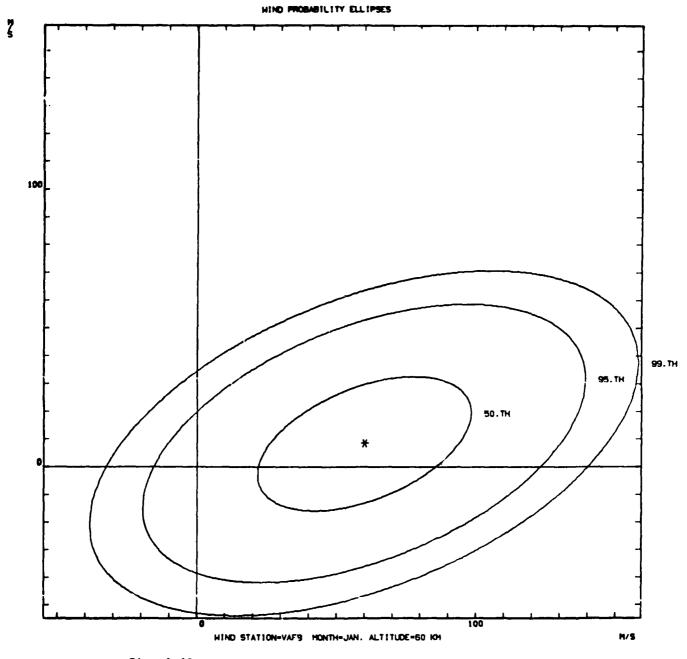


Fig. A-43

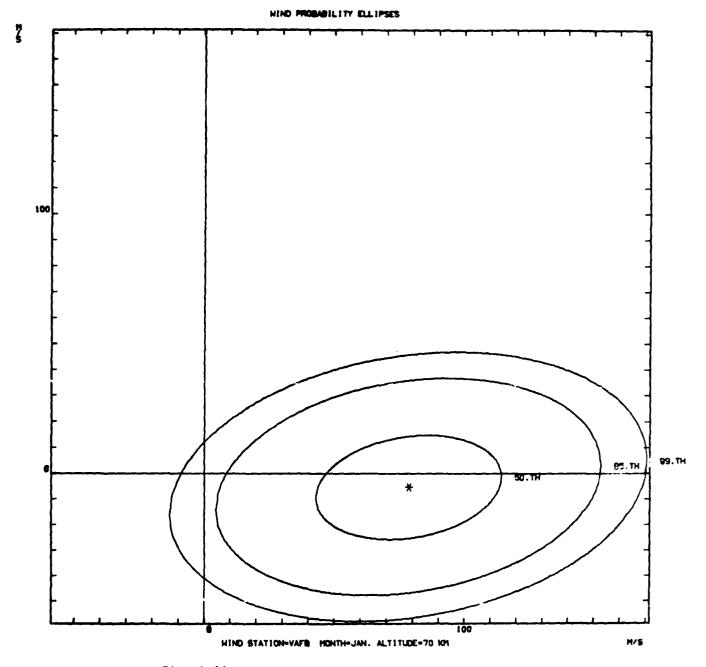


Fig. A-44

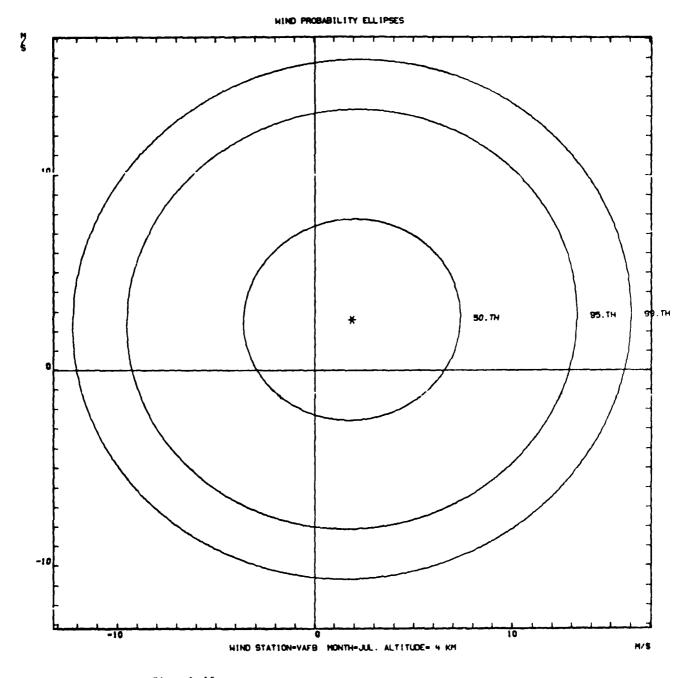


Fig. A-45

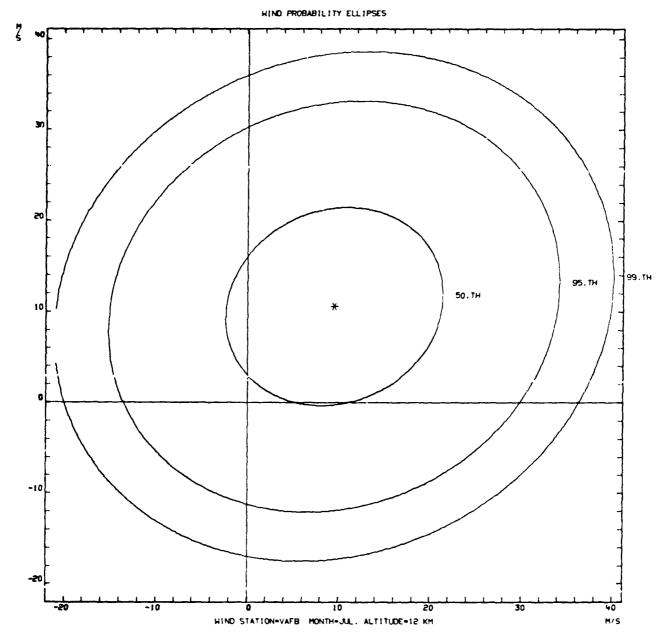


Fig. A-46

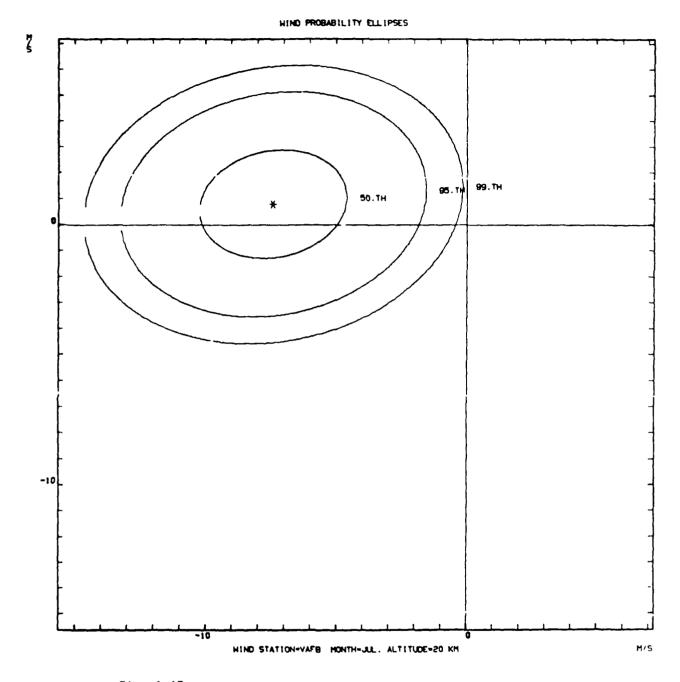


Fig. A-47

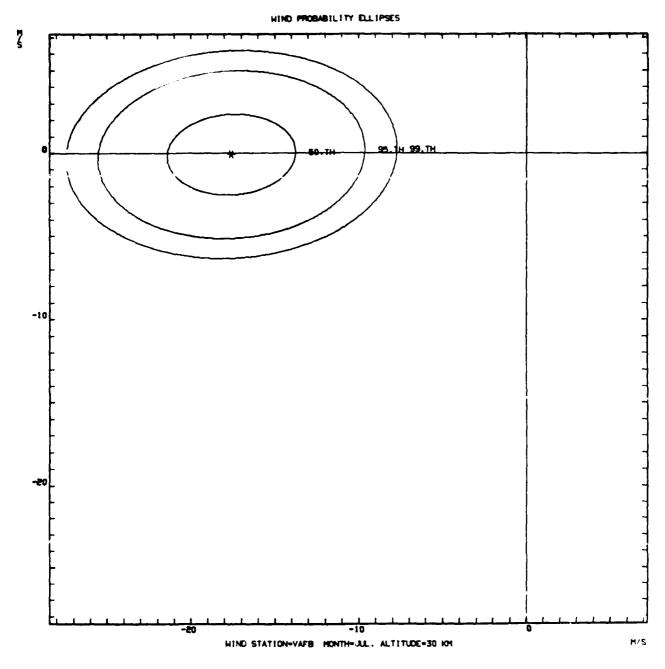


Fig. A-48

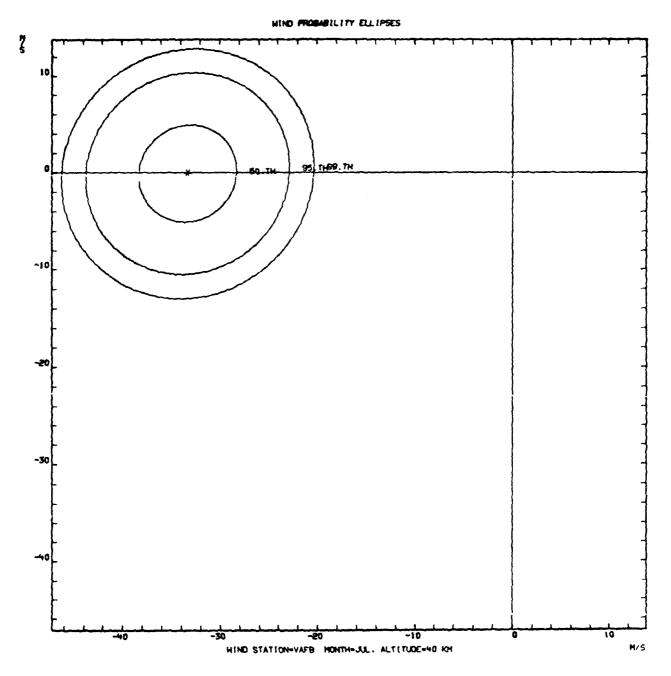


Fig. A-49

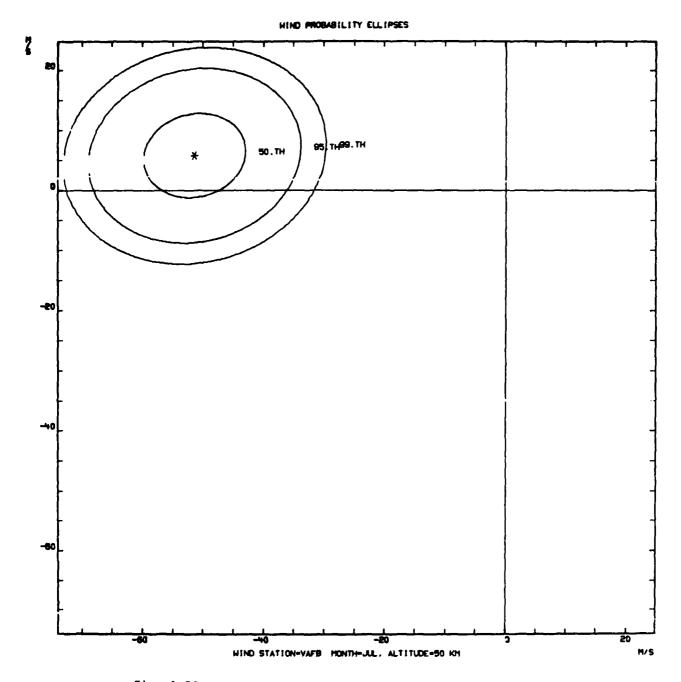


Fig. A-50

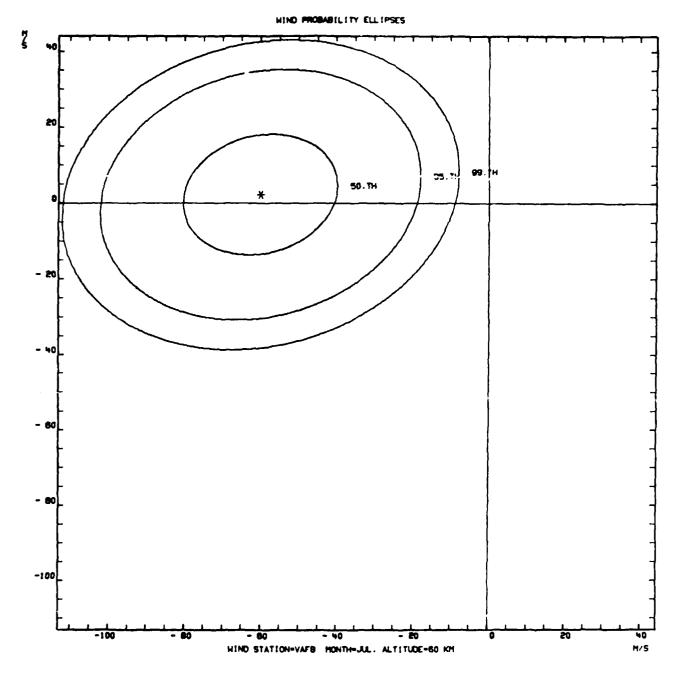


Fig. A-51

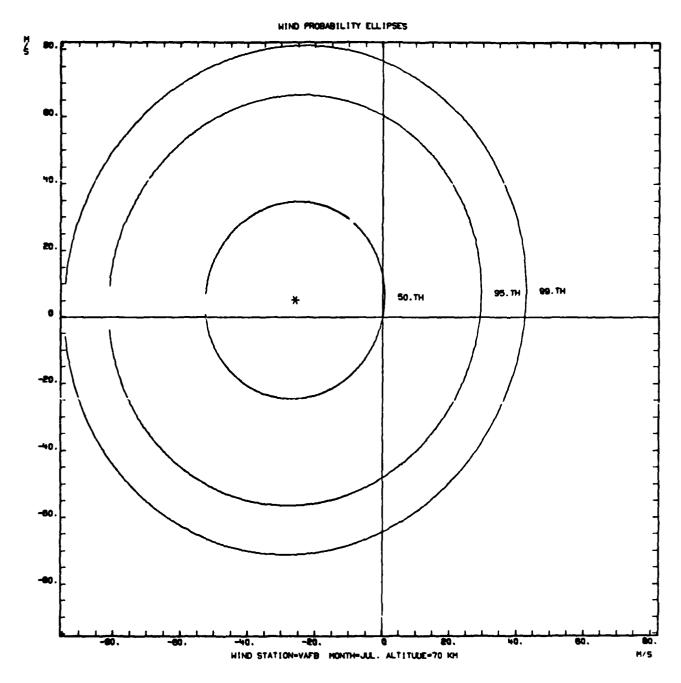
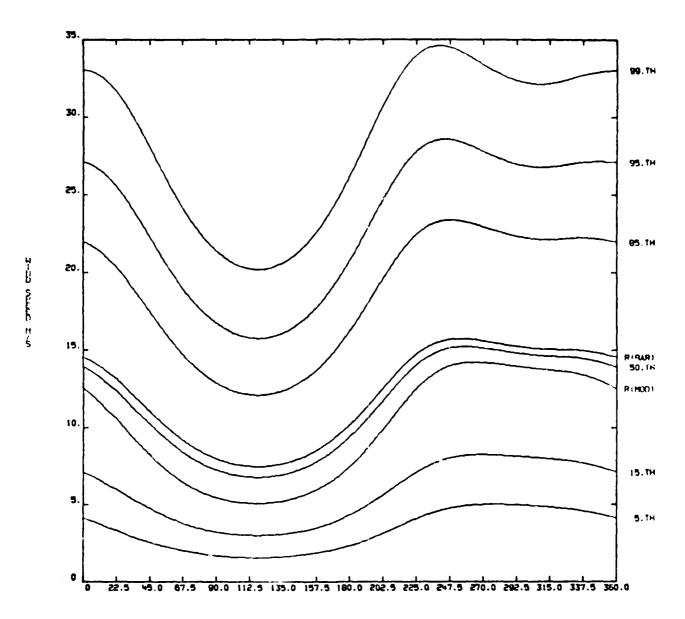


Fig. A-52

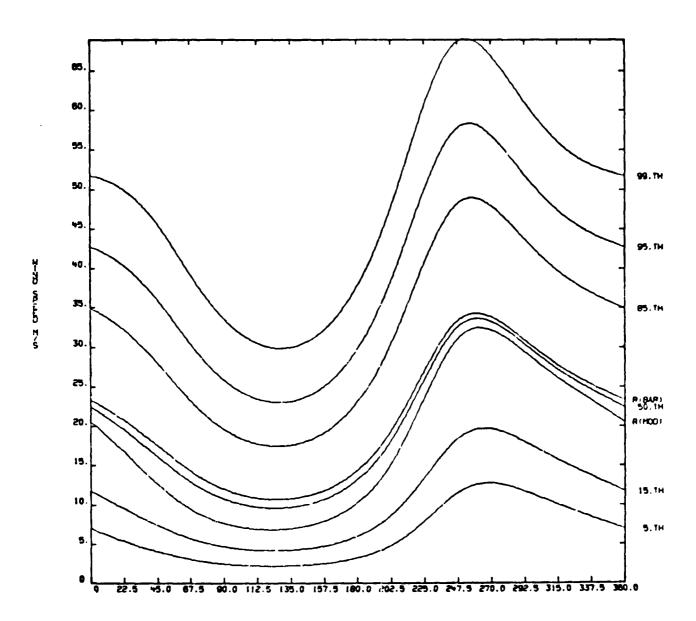
HIND STATION-VAFB HONTH-JAN, ALTITUDE+ 4 KM



CONGITIONAL HIND SPEED GIVEN HIND DIRECTION

Fig. A-53

HIND STATION-VAFB HONTH-LAN. ALTITUDE-12 KH



CONDITIONAL WIND SPEED GIVEN HIND DIRECTION

Fig. A-54

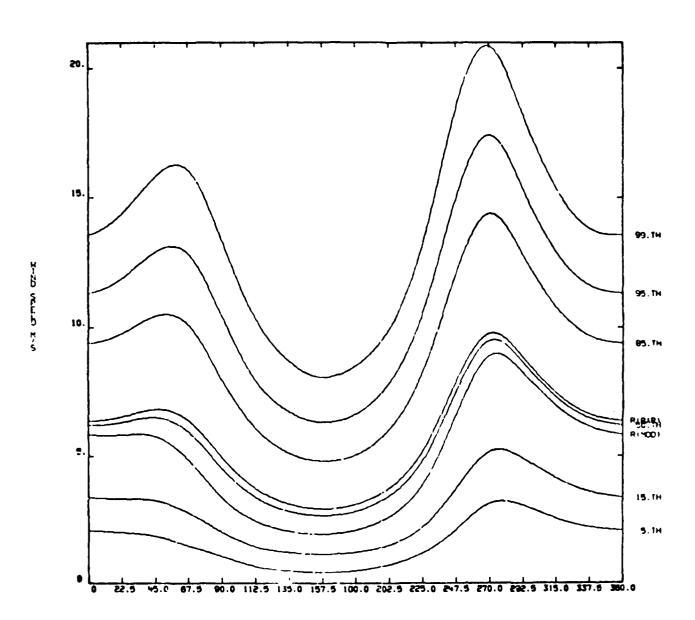
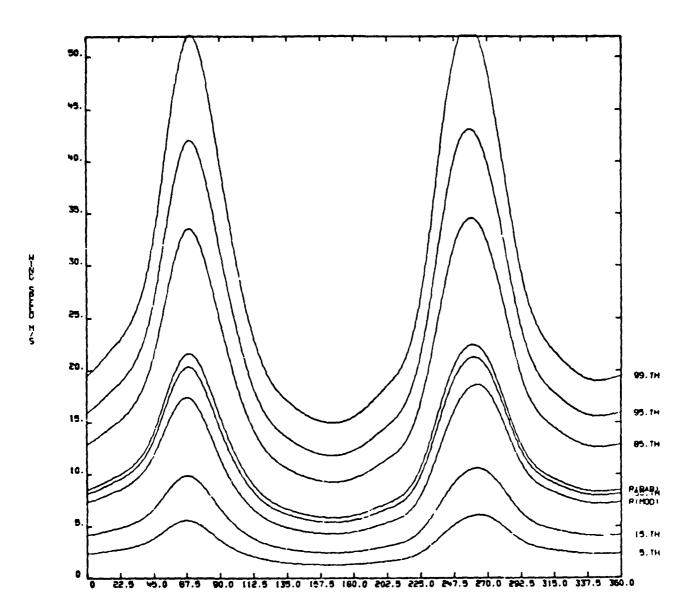


Fig. A-55

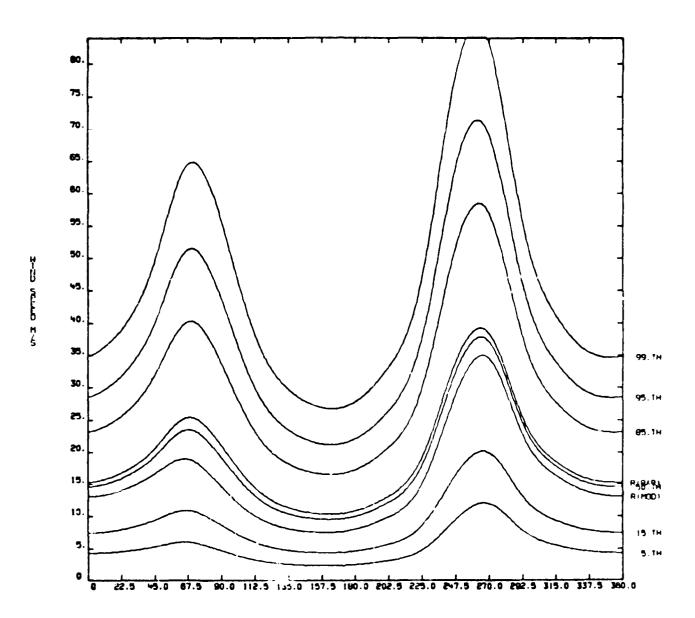
CONDITIONAL HIND SPEED GIVEN HIND DIRECTION



CONDITIONAL HIND SPEED GIVEN HIND DIRECTION

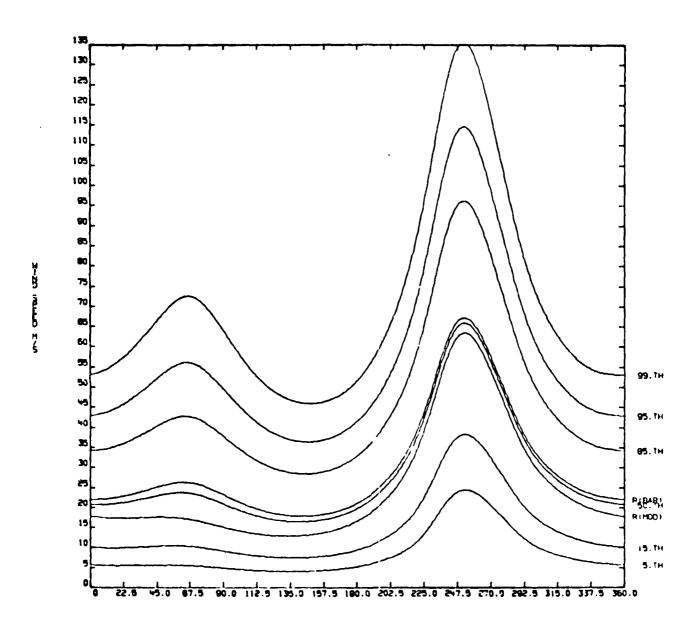
Fig. A-56

HIND STATION-VAFB HONTH-JAN. ALTITUDE-40 KM



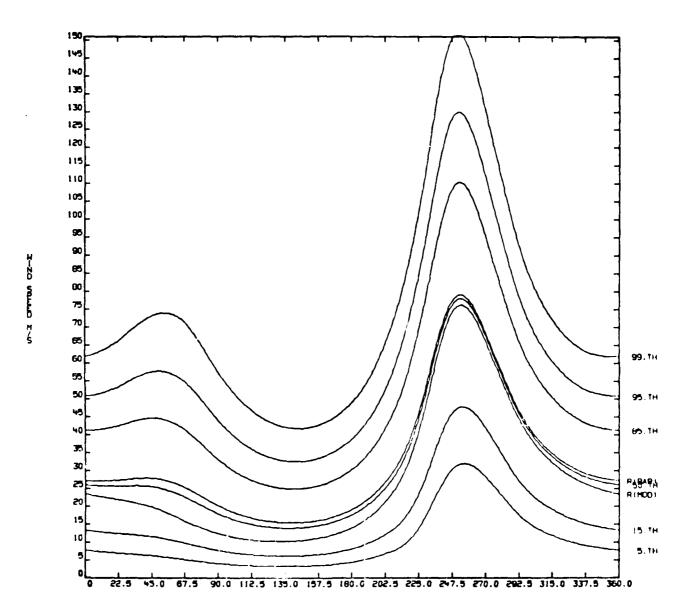
CONDITIONAL HIND SPEED GIVEN HIND DIRECTION

Fig. A-57



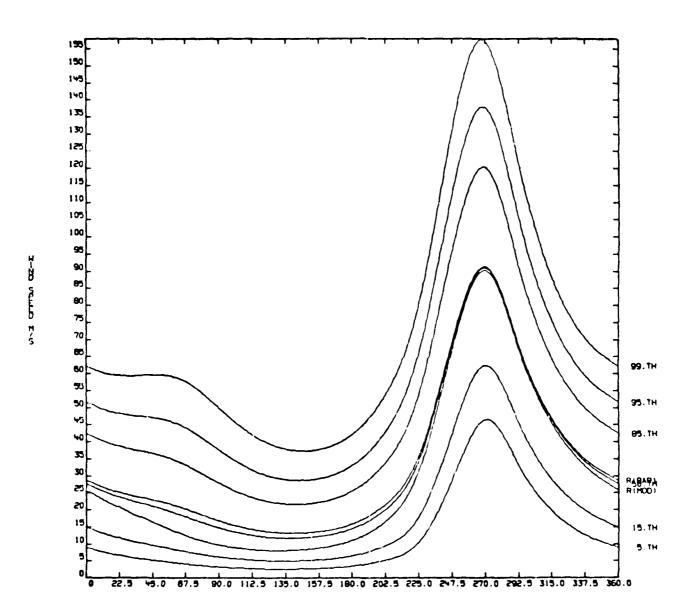
CONDITIONAL HIND SPEED GIVEN HIND DIRECTION

Fig. A-58



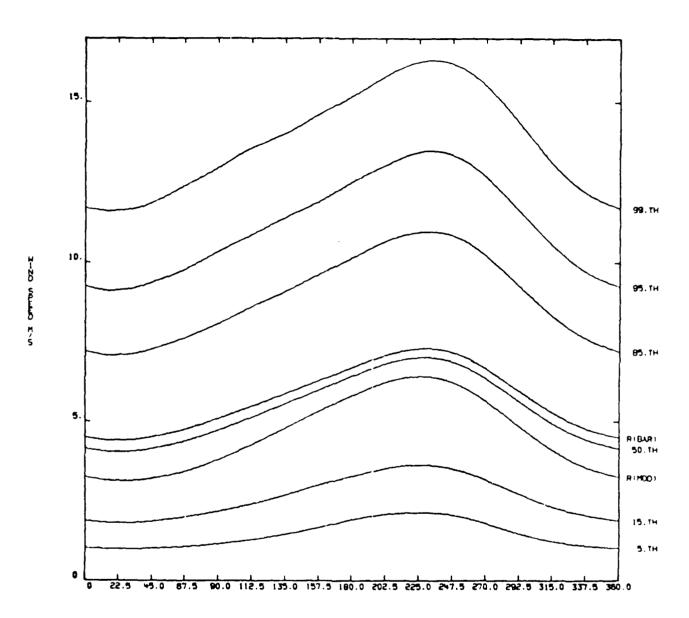
CONDITIONAL HIND SPEED GIVEN HIND DIRECTION

Fig. A-59



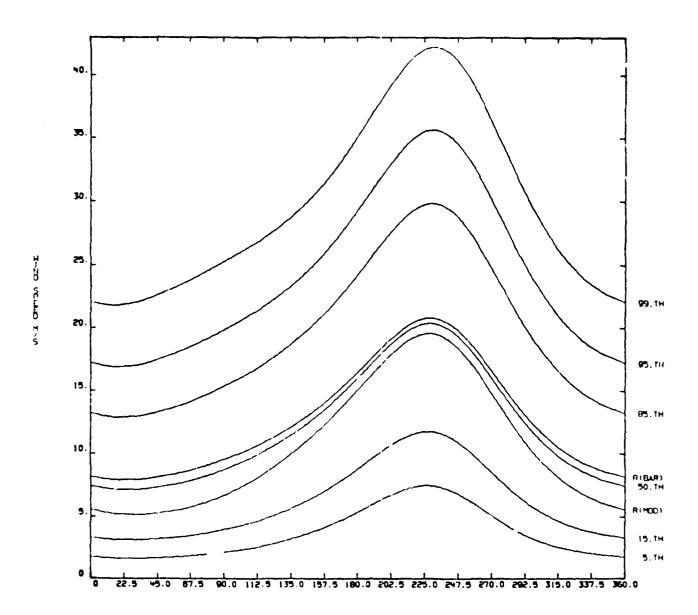
CONDITIONAL HIND SPEED GIVEN HIND DIRECTION

Fig. A-60



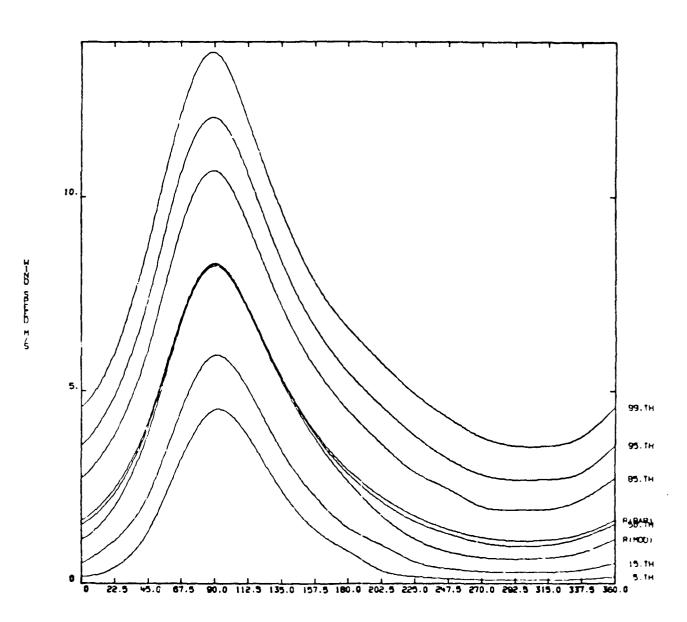
CONCITIONAL HIND SPEED GIVEN HIND DIRECTION

Fig. A-61



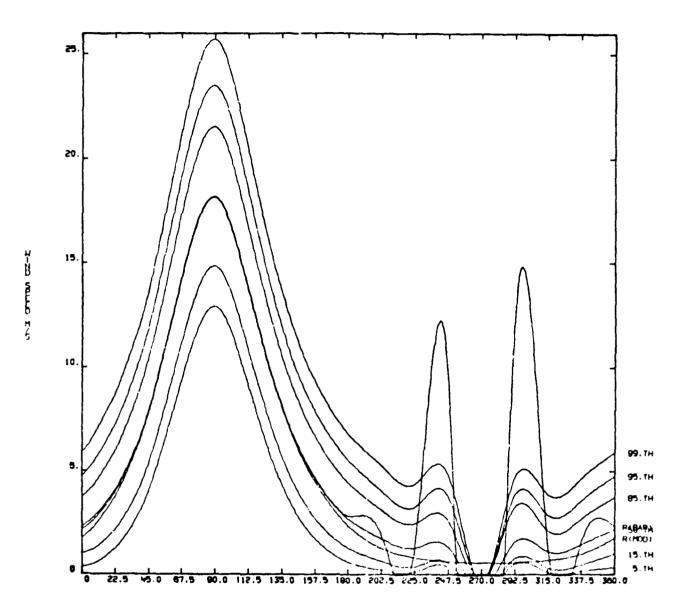
CONDITIONAL HIND SPEED GIVEN HIND DIRECTION

Fig. A-62



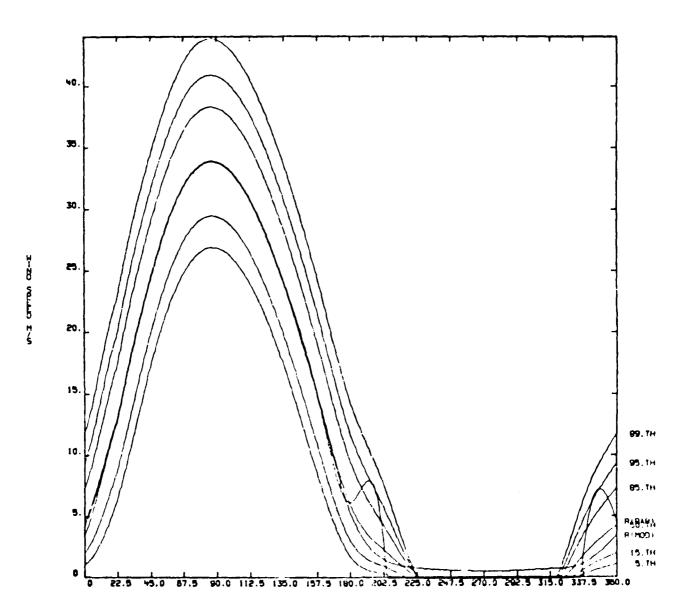
CONDITIONAL HIND SPEED GIVEN HIND DIRECTION

Fig. A-63



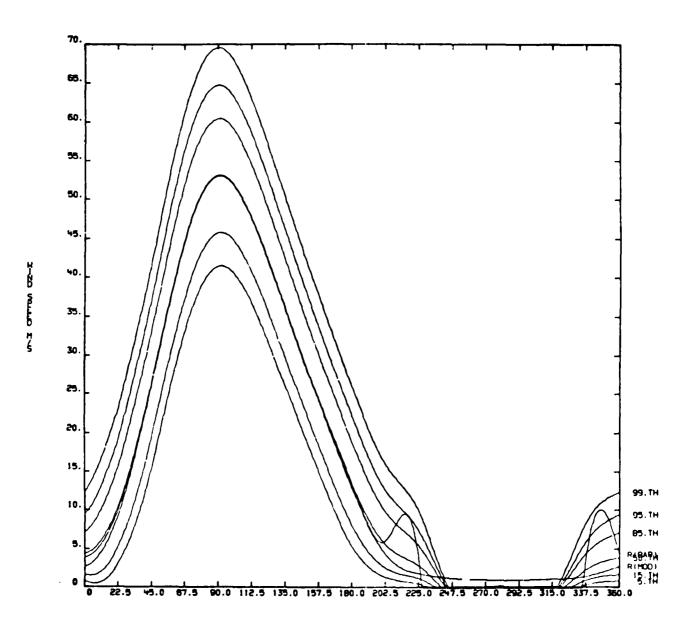
CONDITIONAL HIND SPEED GIVEN HIND DIRECTION

Fig. A-64



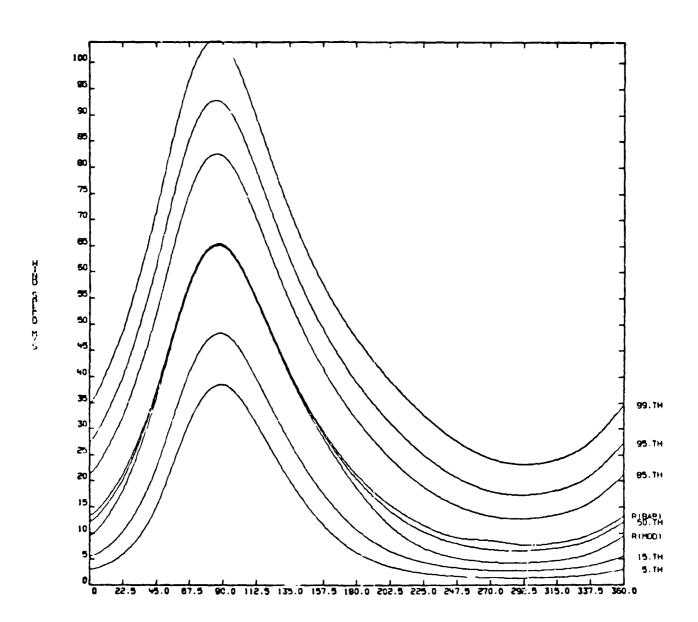
CONDITIONAL HIND SPEED OIVEN HIND DIRECTION

ig. A-65



CONDITIONAL HIND SPEED GIVEN HIND DIRECTION

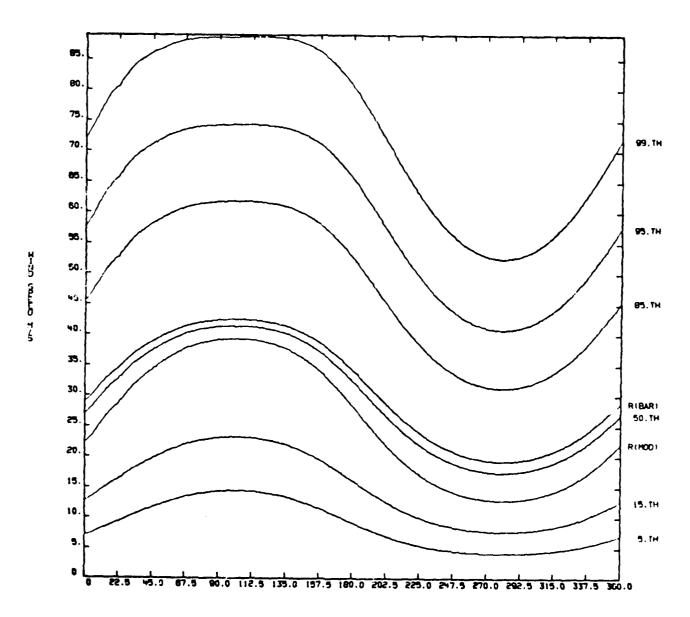
Fig. A-66



CONDITIONS. HIND SPEED GIVEN HIND DIRECTION

ig. A-67

HIND STATION-VA'S HONTH-JUL, ALTITUDE-70 KM



CONDITIONAL HIND SPEED GIVEN HIND DIRECTION

Fig. A-68

APPENDIX B

RANGE SPECIFIC INFORMATION AND THERMODYNAMIC QUANTITIES FOR VANDENBERG AFB, CALIFORNIA

(Data base 32-70 km altitude from Point Mugu, CA)

1. Range Specific Information

To prevent further character size reduction for tables I through IV, certain range-specific information has been omitted. This important information is given in table B-1.

TABLE B-1

Header Record 0-30 Km	Header Record 32-70 Km
Table Number0	Table Number0
Data Source	Data Source
(1 = DATSAV, 2 = WDC-A)1	(1 = DATSAV, 2 = WDC-A)2
Call LettersVBG	Call LettersNTD
WMO Number723930	WMO Number723910
Latitude34°,45'	Latitude34°,07'
Direction (N or S)N	Direction (N or S)N
Longitude120°,34'	Longitude119°,07'
Direction (E or W)W	Direction (E or W)W
Elevation in Meters100	Elevation in Meters4
Start Period of Record	Start Period of Record
(Mo-Yr)160	(Mo-Yr)169
End Period of Record	End Period of Record
(Mo-Yr)1279	(Mo-Yr)1278
No. of Time Windows	No. of Time Windows
(0, 1 or 2)2	(0, 1 or 2)1
Start Time Window	Start Time Window
#1 (Hr-MNZ)2200	#1 (Hr-MNZ)1200
End Time Window #1200	End Time Window #12200
Start Time Window #21000	Start Time Window #20
End Time Window #21400	End Time Window #20
Date of RRA980	Date of RRA1080
Altitude Range of RRA	Altitude Range of RRA
Low Level (km)0	Low Level (km)30
Altitude Range of RRA	Altitude Range of RRA
High Level (km)	High Level (km)70
Standard Deviation of	Standard Deviation of
Thermodynamic Limits6.0	Thermodynamic Limits6.0
Wind 'imits6.0	Wind Limits6.0

2. cmodynamic Quantities

is section presents examples of further computations and graphical displays of pressure, density, and virtual temperature statistics that can be derived from the data given in tables II, III, and IV. No attempt is made to

present complete nor exhaustive illustrations that can be made to aid in visualizing the relationships that can be made from the data in tables II and IV. The choices are those that aided the committee to verify the reasonableness of the tabulations.

2.1 Monthly Means from the Annual Mean

The hydrostatic model values in table IV are used to compute (1) the monthly mean differences relative to the annual mean values of pressure, density, and virtual temperature expressed in percent and (2) the monthly mean difference in virtual temperature for the annual mean virtual temperature expressed in degrees Kelvin. Examples of these four statistics are given in table B-2 for January and table B-3 for July. Graphical displays of the four statistics contained in tables B-2 and B-3 are shown in figures B-1 through B-8. Also, the relative differences between the monthly mean values from table IV-1 through IV-12 for all months from the annual mean values (table IV-13) are illustrated in figure B-9 for pressure, in figure B-10 for density, and in figure B-ll for virtual temperature. The monthly mean virtual temperature differences from the annual mean virtual temperature for all months are given in figure B-12. The simple sum of the monthly mean differences from the annual mean values of these quantities is not zero. This is because the annual mean statistical parameters are computed (see section C of text) by weighting the monthly means by the number of observations in each month.

2.2 Coefficients of Variation and Derived Correlation Coefficients

The coefficient of variation, C_V , is defined by the standard deviation with respect to the mean divided by the mean. The coefficients of variation for pressure, C_VP , and density, C_VD , were computed using the standard deviations from table II and the hydrostatic mean values from table IV. The coefficient of variation for temperature uses the standard deviations of virtual temperature from table III to the altitude where virtual temperature exists. Above this altitude, the standard deviations of temperature are from table II. The mean values for comperature (virtual temperature to the altitude where it exists) are taken from table IV. No distinction is made in the table headings in table B-4 (Jan) and table B-5 (July) and all related figures between virtual temperature and temperature.

From the coefficients of variation for pressure, density, and temperature (virtual temperature to the altitude where it exists), the correlation coefficients between these quantities are derived using Buell's method (see reference in text). The equations for these derived correlation coefficients are

$$r(P,T) = \frac{(C_V T)^2 + (C_V P)^2 - (C_V D)^2}{2[C_V T \cdot C_V P]},$$
 (B-1)

$$r(P,D) = \frac{(C_V D)^2 - (C_V T)^2 + (C_{V'} P)^2}{2[C_V D \cdot C_V P]}$$
 (B-2)

$$r(T,D) = \frac{(C_V P)^2 - (C_V D)^2 - (C_V T)^2}{2[C_V T \cdot C_V D]} .$$
 (B-3)

The correlation coefficients in tables B-4 and B-5 are derived from the above equations.

A test for the validity of the derived correlation coefficients is that all three of the following inequalitites be satisfied.

$$C_{V}P - (C_{V}D + C_{V}T) < 0$$

$$C_{V}D - [C_{V}T + C_{V}P] < 0$$

$$C_{V}T - [C_{V}P + C_{V}D] < 0$$
(B-4)

In these examples (tables B-4 and B-5) the numerical values from equation (B-4) are all negative; hence, the derived correlation test is considered valid. The rare exceptions to this test for several RRAs occur at the extreme highest altitudes, where sample sizes for the statistical sample are small.

The statistical parameters from table B-4 (January) and table B-5 (July) are illustrated in figures B-13 through B-16.

For all months the $\mathrm{C_VP}$ values are shown in figure B-17, the $\mathrm{C_VD}$ values are shown in figure B-18, and $\mathrm{C_VT}$ values are shown in figure B-19. If the abscissa on the figures for the coefficient of variation were multiplied by 100, these figures would show the percentage of the random dispersion of these quantities over the month with respect to the monthly mean for these thermodynamic quantities.

The derived correlation coefficients for all months are illustrated in the following figures:

Figure B-20 gives r(P,D).

- figure B-21 gives r(P,T).
- c) Figure B-22 gives r(T,D).

Table B-2

	T23930 IN PEPCENT	MONTH I	D ANTUAL	
LEVEL	PRESSURE	DENSITY	TEMP.	TMT-TAINIGEC.K)
.000	.23	.81	- 6→	-1.84
.100	.22	. 9 0	71	-2.5+
1.000	.09	1.7→	-1.68	-4.72
2.000	12	1.65	-1.74	-4.95
3.000	33	1.35	-1.65	-4.58
4.000	54	1.13	-1.64	-4,47
5.000	75	. 98	-1.70	-4.52
E.000	93	. 83	-1.79	چن. به۔
7.000	-1.23	.65	-1.811	+4.72 -4.83
9.000	-1.49 -1.78	. 49 . 32	-1.99 -2.09	-4 (% -4 (%)
9.000	-2.09	. 35	-2.13	-4.96
11.000	-5.33	5 6	-1.65	-4.12
12.000	-2.62	-1.53	-1.11	-2.41
13.000	-2.73	-2.55	~ .20	-, w3
17.000	-2.71	-3.08	.39	9.7
15.000	-2.64	-3.19	.57	1.13
15.000	-2.56	-2.89	. 36	.76
17.000	-2.53	-2.55	. 01	50.
18.000	-2.56	-2.16	38	- 63
19.030	-2.64	-2.61	83	-1.52
20.000	-2.75	-1.98	79	-1.67
21.000	-2.69	-1.98	دو	-1.98
25.000	~3.03	-2.05	-1.00	-2.15
23.000	-3.20	-2.06	-1.17	-2.5+
24.000	-3.30	-2.17	-1.24	-2.70
25.000	~3.59 ~3.81	-2.15 -2.27	-1.44 -1.57	-3.17 -3.48
25.000 25.000	-3.04 -4.06	-2.30	-;.57 -;.79	-3.99
28.000	-4.33	-2.61	-1.73	-4.02
20.000	-4,59	-5 85	- : .82	-4.11
30.000	-4,85	-3.19	-:.76	-4.21
30 000	-5.30	-4.20	-1.43	-3 33
34.000	-5.65	-4.80	-1.13	-2.66
36.000	+5.92	-5.27	93	er. 5-
39.000	~6.13	-5 69	7c	-1.73
40.000	~8.33	-5.73	8-5	-5.19
42.000	-6.51	-6.18	80	~1.56
44.000	-6.61	-6.59	23	50
46.000	-6.64	-6.87	.03	. 07
48.000	-5.71	-6.37	61	-1.54
50.000	-6.96	-5.69	-1.55	-4.13
\$2.000	-7.42	-5.50	-2.56	-5.99
54.000 55.000	-7.96 9. 49	-6.0≥ -8.79	-2.33 -2.05	~8,04 ~5,34
56.000	8	7.66	-1.62	۳۰, ۱۳ ۱۲, ۲۰
60.000	-9 241.,	Cincil 65	1.54	~3.16
€2.000	737 58	-8.56	-: 26	-3.14
64.000	-9.75	-9.25	12	- 30
.66.000	-9.74	-10.19	.55	.46
68.000	-9.56	-16.88	1.23	E.77
70.000	-9.1 <i>2</i>	~11.13	2.03	4.43

Table 5-3

STATION DELTAS		MONTH 7 RELATIVE T	O ANTRUAL	
LEVEL	PRESSURE	DENSITY	TEMP.	THO-TARMODEG.K)
DELTAS	IN PERCENT	RELATIVE T	TEMP. 43 .555 2.83 2.99 2.81 2.65 2.61 2.77 3.14 3.26 3.29 3.02 2.21 .7468 -1.51 -1.446517 .40 .83 1.11 1.34 1.46 1.62 1.67 1.72 1.76 1.79 1.16 1.79 1.16 1.79 1.16 1.79 1.16 1.79 1.70 1.70 1.70 1.70 1.70 1.70 1.70 1.70	TMO-TANENOEG.KI 1.25 11.59 8.159 7.81 7.21 6.94 7.17 7.46 7.65 7.65 7.51 6.72 4.81 1.60 -1.45 -3.17 -3.01 -1.77 -3.01 -1.77 -3.93 3.16 3.53 3.39 3.58 3.73 3.98 3.97 3.08 3.97
44.000 48.033	8.43 9.50	7.91 8.14	. 35	.93 53
68.000 69.000 69.000 70.000	7.11 5.28 5.40 4.47 3.59	9.30 9.03 9.47 7.48 6.13	-2.70 -3.02 -3.02 -2.55	-5.03 -7.15 -6.50 -7.09 -6.56 -6.56

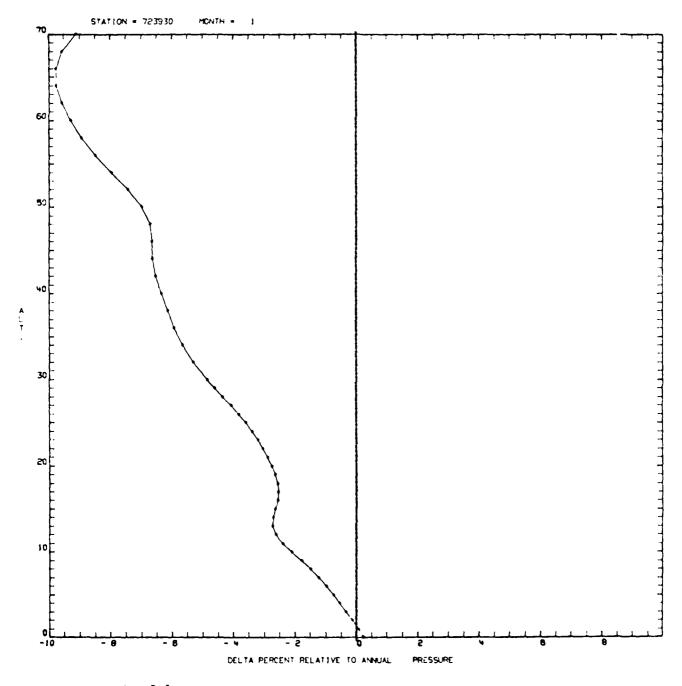


Fig. B-1

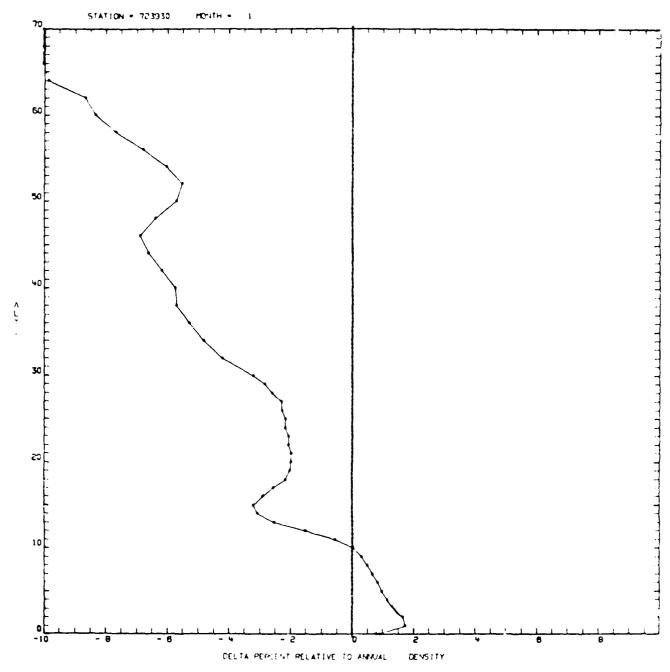
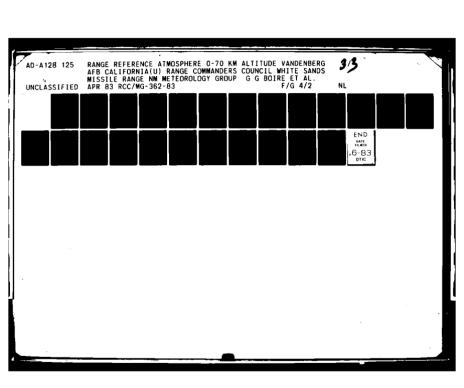
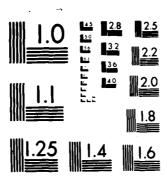


Fig. B-2





MICROCOPY RESOLUTION TEST CHART NATIONAL BUREAU OF STANDARDS-1963-A

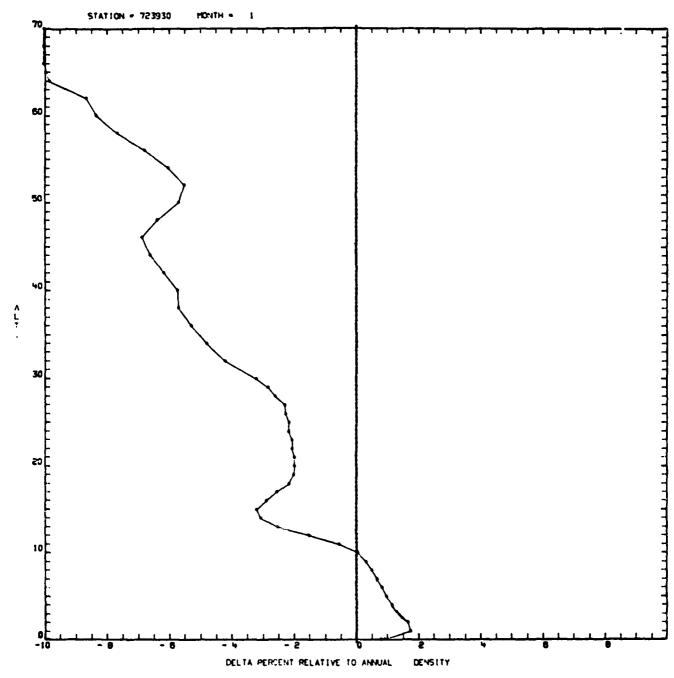


Fig. B-2

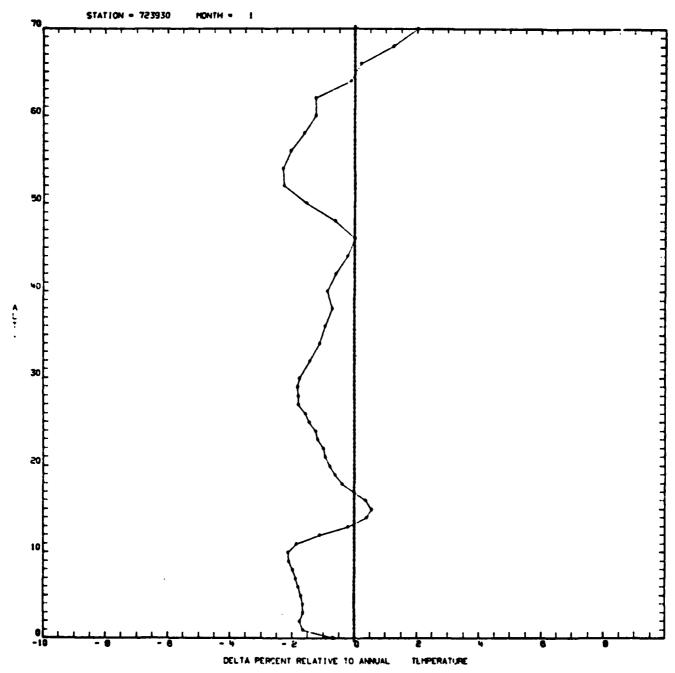


Fig. B-3

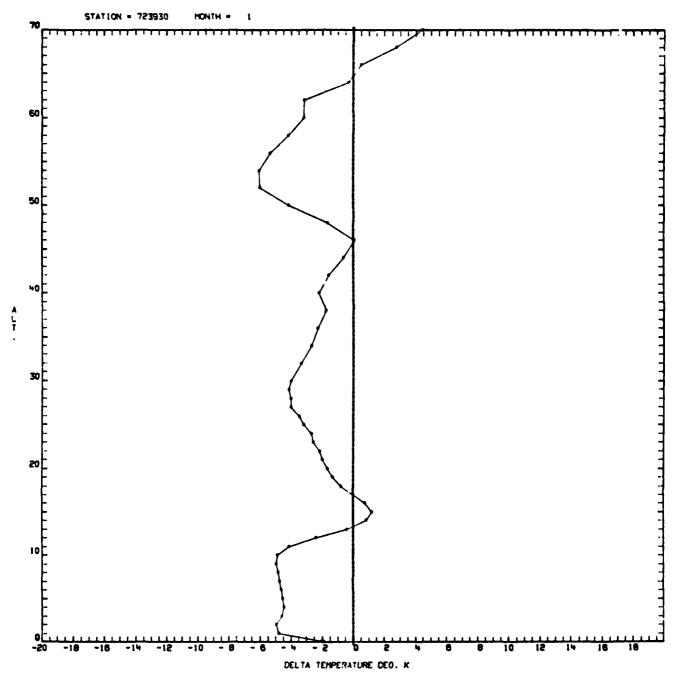


Fig. B-4

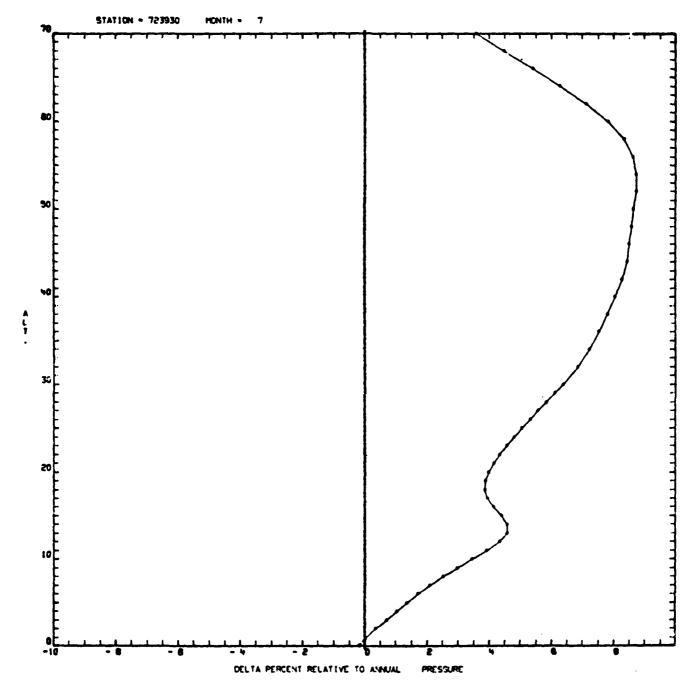


Fig. B-5

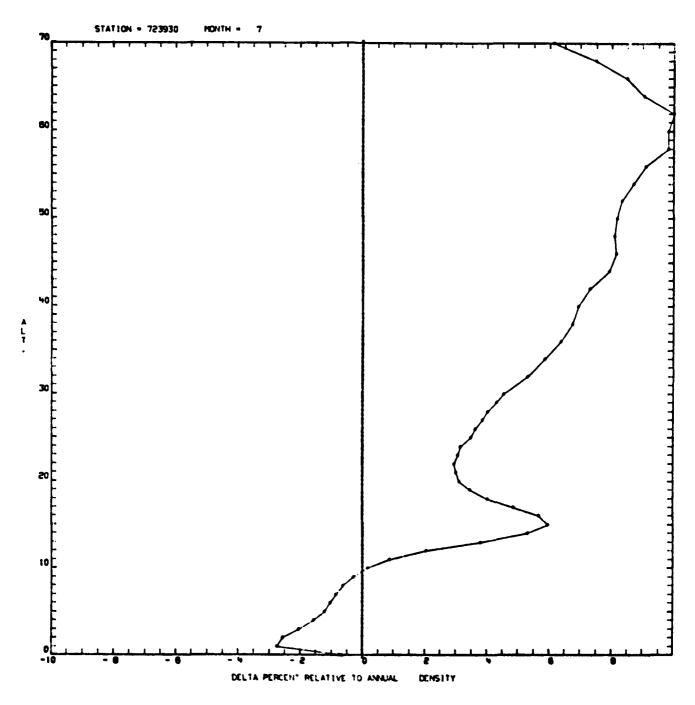


Fig. B-6

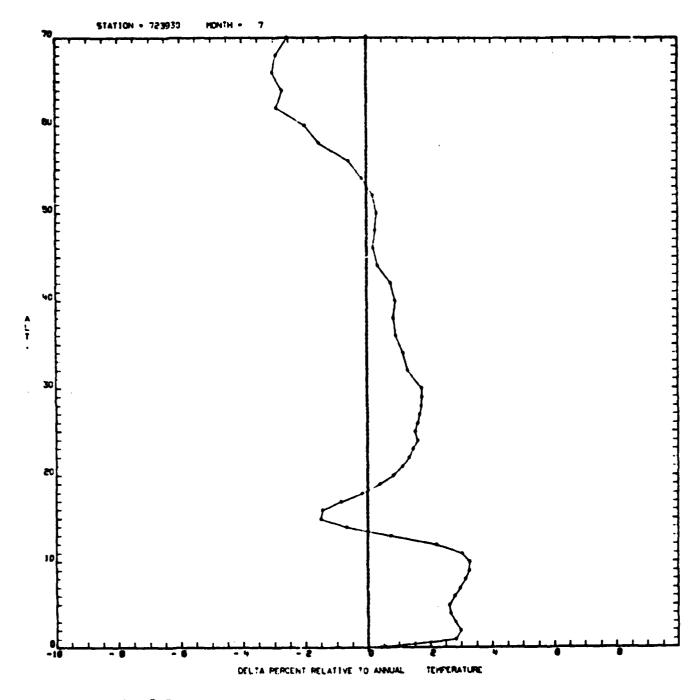


Fig. B-7

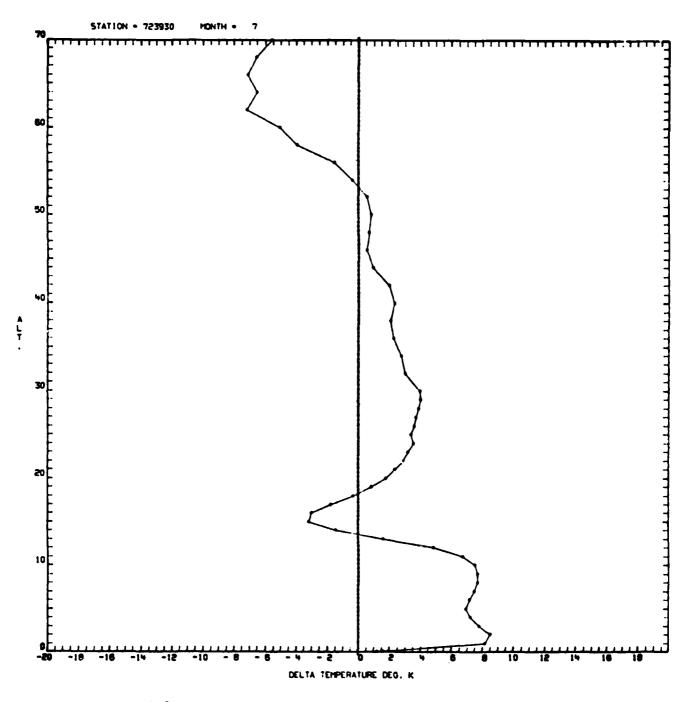


Fig. B-8

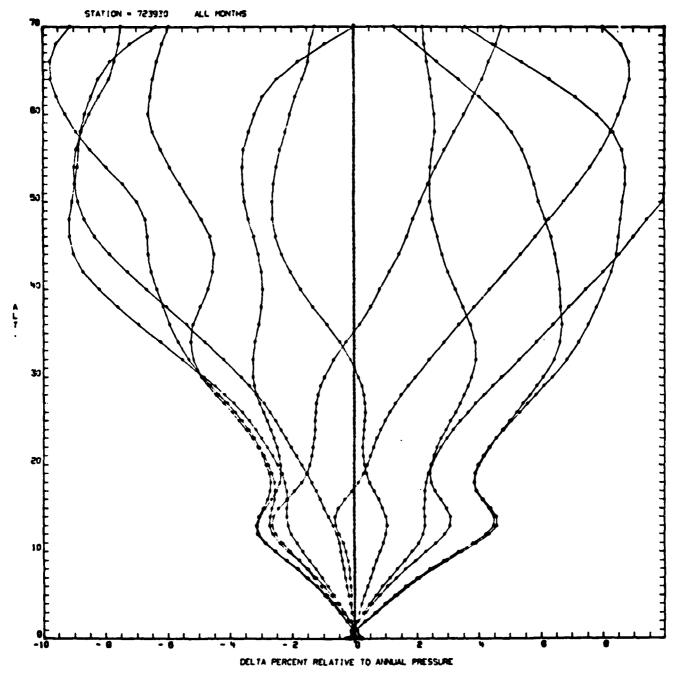


Fig. B-9

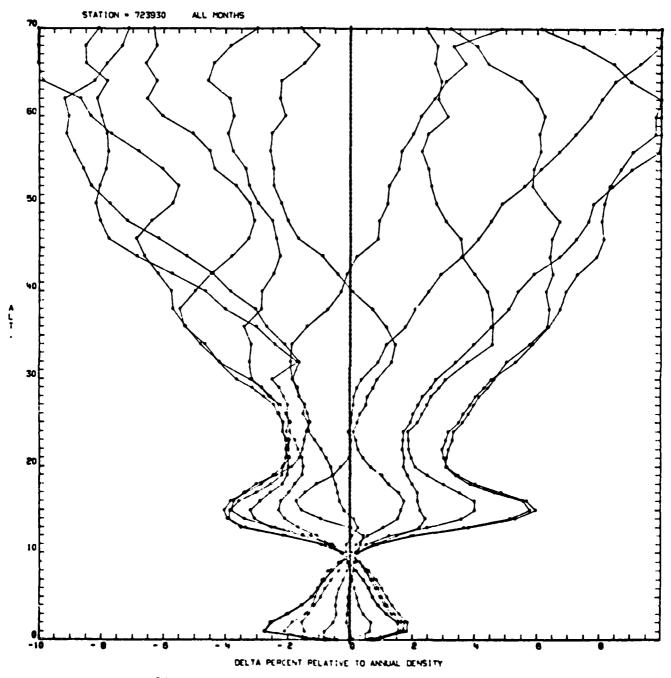


Fig. B-10

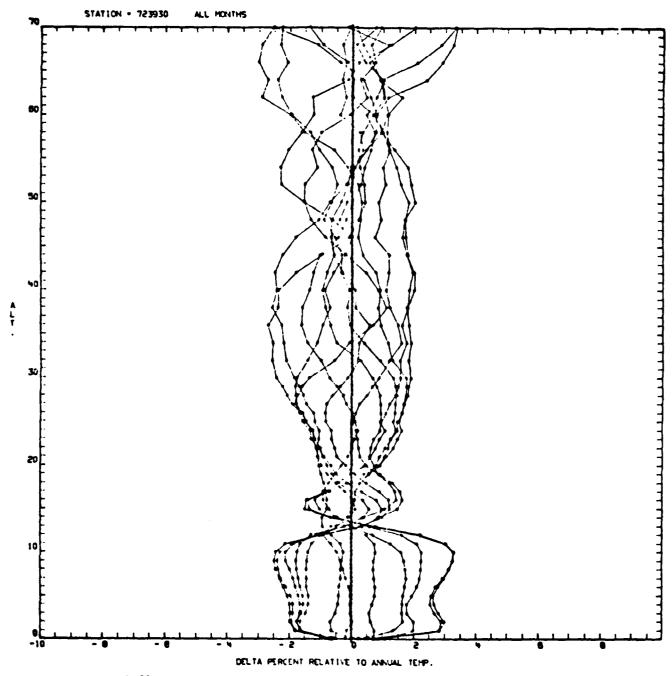


Fig. B-11

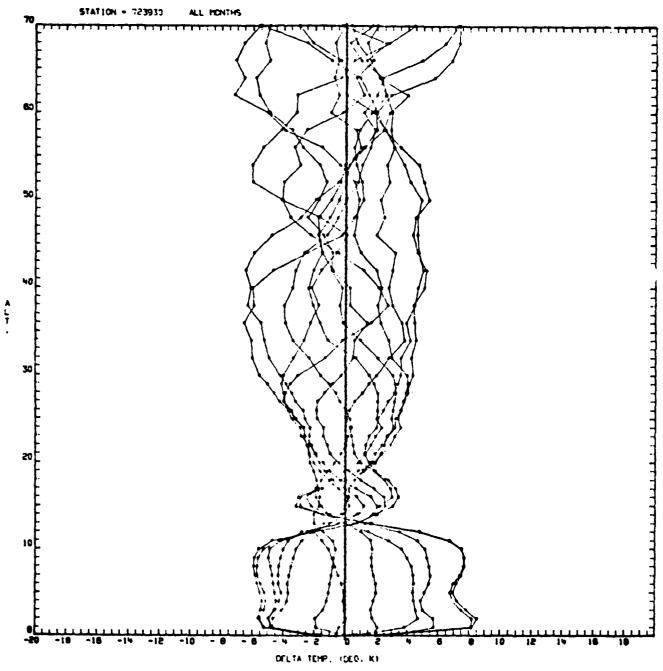


Fig. B-12

Table B-4

STATION	723930 MO	धाम ।							
LEVEL	CVP	CVD	CVT	R(P,T)	R(P.D)	R(T,D)	DCVP	DCVD	DC"17
			•••	••••		A(1,5)	DC VP	DC VU	DC :
.000	. 0045	.0162	.0169	1772	.4107	9701	0306	0032	0058
. 100	. 00→5	.0175	.0164	1089	. 3575	~.9673	0294	0034	0055
1.000	.0051	.0164	.0183	.4890	2338	9624	0296	0070	0032
2.000	.0065	.0145	.0198	.7517	5222	9550	0267	0108	0023
3.000	.0384	.0123	.0182	. 8241	5414	9224	0221	0143	0024
4.000	.0:04	.0102	.0179	.8745	5203	0692	0177	0!81	- 0026
5.000	.0:25	. 0035	.0184	.0802	~.3920	7817	0154	0214	0036
6.000	.0:47	. 0090	.0188	.86+3	2074	6401	0130	0245	0349
7.300	.0169	. 0092	.0190	.8766	.0082	4740	0114	0266	0069
B.000	.0192	.0:00	. 0190	.8528	.2793	2444	0038	02:62	0102
9.000	.0214	.0128	.0182	.8047	. 5286	0784	÷.0096	0209	0159
10.000	. 6232	.0197	.01 <i>6</i> 8	.6052	. 6988	1466	0123	0213	0251
1:.000	.0242	.0297	.0185	.1138	.7681	5487	0231	0140	0344
12.000	0.739	. 0390	, 0∂53	2627	.7798	8088	0406	0101	0375
13.000	.0224	. 0402	. 0055	4058	.8150	8603	04 32	0077	÷.0371
14300	.0208	.035+	.0202	4911	. 8675	8594	0349	0056	0360
15 000	.0193	.0338	.0188	6011	.8961	8933	0335	0040	÷.03¥0
15.000	.0172	.0333	.0199	6196	. 8939	9147	0360	0037	0306
17.000	.0153	.0316	.0202	5812	. 6539	9198	0368	0039	C267
18,000	.0134	. D293	.0195	4582	. 7894	9074	0344	0046	¢221
19,000	4510.	, p. 734	.0176	1952	.6767	8542	0286	0066	~.0182
20.000	.0122	.0198	.0167	. Cui45	. 5436	-,7881	0242	0001	~.0153
21.200	.0169	.0172	, 0165	.3315	. ษ. หกุ	-,7101	0008	0121	0136
22,000	.0143	.0151	.0155	.5192	. 3602	-,6102	0175	D154	01c6
23.000	.0154	.0140	.0165	.6!83	. 3746	4974	0151	0179	0129
24.000	.0167	.0137	.0163	-659+	. 4 <i>3</i> 67	\$695	0133	0194	0140
25.000	.0197	.0139	.0162	.6965	.5381	2533	0113	0515	~.0163
26.000	.0234	.0151	.១រគរ	.6793	.6214	-, 1533	0109	0214	0193
21.000 28.000	. ช. ' ถ่าว	.0163	.0162	6732	.6735	0851	0105	.0719	~. C≥.}}
29,000	.0735	.0184	.0161	.6249	.7302	0783	0110	→. つ ∂12	CJ 5 0
39.000 39.000	.02%5 .0253	.0201	.0170	.5849	.7293	-,1299	0125	0214	0277
39.000 32.000	.0227	.0332 .0320	.0177	.4724	.7408	0421	0154	0200	0311
34.000	.0240	.0320	.0246 8850.	.6901	.6+15	7058	0330	- 0154	0301
36.000	.0253	.0320		.1327	.5767	73.62	0398	0173	0301
30.000	.0292	.0395	. 7354 . 8487	.2010 .4313	. 4777	7646	0490	0219	~.0371
40.000	.0346	.0348	.0+03	.9313 .5762	.3017 .3270	7300 5840	0500	0313	0270
42.0C0	.0408	.0379	.0403	.562 5	.4796	5640 4558	0405 0373	0401	0292
44.00D	. 0455	.0420	.0362	.4917	.6609	3285	03/3	0431	03H5 0514
46,300	.0497	.0457	.0335	.4512	פיציד. פיציד.	-, 24 <i>5</i> 2	0327 0236	0398	0514
48.000	.0532	.0447	.037 9	.5430	.8519	.0228	0194	0375	
50.200	.0569	.0491	. 0244	.5117	.9047	.0969	0166	-∞0364 -∞032}	0701 08! 7
52,000	.0503	.0555	.0241	.3996	.9164	0116	0134	0289	09:7
54.000	.0614	.0586	.0217	.305∢	.9354	0500	0189	0246	0907
56 000	.0611	. 0538	.0254	.2573	.9:20	1517	0241	0267	D955
58.000	.0613	. 0586	.0256	.3124	.9098	:100	0229	0283	0943
60.000	.0667	.0595	.0369	.462.?	.8349	1023	0297	0442	0693
62.000	.0592	.0515	,0427	.5290	.7105	2213	0350	0504	0580
64.000	.0638	. 0537	.0458	.5525	.7078	1858	- 6351	0560	0715
66.003	.0092	. 0484	.0590	.7183	.5332	2047	0392	0787	0577
58 .000	.0875	.3519	.0638	.7058	.6947	0317	0387	0894	0856
79.000	.0652	.0617	.0415	.4176	.7916	2247	0370	0460	CB64

Table B-5

STATION 72	73930 MON	ITH 7							
LEVEL	CVI	CVD	CVT	R(P,T)	R(P.01	R(T,D)	OC VP	CVO	DC"T
.000	.0018	.01:2	.0114	. 1465	.0119	9974	0208	0019	0017
. 100	.0013	.0:06	.0108	.2151	0472	9857	0196	0021	0016
1.000	.0072	.C. 33	.0:39	.2759	1195	9871	0249	0027	0018
2,000	.0027	. CC 32	.010	.553!	3276	9663	C:68	0040	0015
3.000	.0035	. COF-B	. 0194	.6195	2476	9139	0116	0051	0019
⇔ ∵000	.00 • ?	.006	.0075	.5320	.0322	8252	0097	00%+	0031
5.000	.¢3∢7	. 0066	. 3077	.5324	. 0895	7954	- . CC 95	5759	CC36
6.000	.0053	. 006%	.0084	.5477	0240	7772	÷.0095	0072	0033
7.000	10001	.0051	.0031	,74 3 4	1187	7464	0391	0032	0031
8.000	. 6371	.0061	. 2100	.79:9	1277	7080	~.0090	0:09	0033
9.000	.0082	.036+	.0178	.8100	0926	6590	0090	0126	0637
10.000	. 0035	.cosa	.0114	.8058	. 0503	5539	~.0096	0142	00-9
1: 000	.0109	. 2777	.0113	.7591	. 3015	3932	~ . 0081	0144	0073
12.000	.0117	.0:07	.0105	.5352	.5657	33 38	009 5	C114	0119
13.000	.0122	.0155	.0:05	.0723	.7385	6191	~.0138	0072	0172
14.000	.5119	.0:95	.0:24	2932	.7931	8088	0199	0048	0190
15.000	.0113	.0213	.0142	38+3	.7864	8725	0242	0042	0183
16.000	.0106	. 2209	.0145	3760	.76E8	89 30	C248	0042	0170
17.000	.0036	.0179	.0129	2634	.7226	8572	0212	0045	0146
19 000	.0093	.0148	.0108	0762	. 6857	7 781	0162	- 0053	0133
19.000	.0032	.0120	.0184	.0705	7157	- 6452	0112	- 0056	0128 -
20.000	.0035	.0:10	.0077	. 1968	.7271	5300	0092	0062	0128
21.000	.028	. 0102	.0073	. 3224	.73+2	4060	0077	0009	0127
22.000	.0102	.0035	.0069	.4335	. 7645	-,2494	0061	- 0075	0130
23.000	.0107	.0094	.0058	.4350	.7815	1552	00%5	0081	0134
24.000	.0!13	.0033	.0069	.5712	.7923	C4B2	0049	0083	0137
25.000	.01:9	.0003	.0070	.6530	. 8035	. 04 38	0044	0095	0142
26.000	.0126	.0038	.0074	.6278	.8123	. 0559	0046	0102	0:51
27.000	.0132	0103	.0079	.6299	. 8035	. 04 37	5049	0108	0156
28.000	.0143	.0107	.0191	.6693	. B204	. 1378	00+5	0117	0170
29.000	.0152	.0118	.0088	.6351	.8155	.0708	0054	0122	~.0:BI
30.000	.0160	.0122	.0085	.6541	.8-61	. 1502	65+9	0124	~.0;96
32.000	.0162	.0:63	.0145	.4369	1508.	4551	0147	0143	0180
34.000	.0176	.0154	.0138	.5+30	.6576	2755	0116	0160	0:92 0:15
₹6.000 39.00J	.0190	.0165	.0149	.5331	.6979	2338	0115	0165	0215 0244
40.000	. 0208 . 0226	.0:92	.0157	.474 7 .5502	.6953	3011	0141 0120	0173 0189	0263
40.000 42.000	. U226 . C.744	.0:91	.0154		.7378	1576	- 0103	0169	0320
99.000	.0251	.021 2 .0230	.01 <i>3</i> 5 .0169	.5017 .435 3	.9330 .7709	0607 1715	0139	0193	0322
46.000	.0293	.0030	.0204	.5422	.7065	1715	0158	- 0243	0320
48.000	.0308	.0249	.0185	.5993	. 7990	0149	0126	-,0244	0371·
52.000	.0300	.0263	.0158	.5993 .5943	.7990	.1167	0033	0217	0428
5c'.000	.0345	.0291	.0160	.5954	. 8888	.1609	0036	0224	0465
54.000	.0372	.0271	.0205	.7022	. 6431	.2092	0104	0306	0-39
55.000	.0430	.0282	. 022 9	.7795	.8621	. 3547	0089	0365	0474
58.000	.0474	.0337	.0287	.7111	.8002	. 1474	- 0150	0425	0524
60.000	.0474	.0372	.0769	.6570	.6253	1631	0269	0510	04 '5
68.000	.0560	. C449	.04:4	.6109	.6833	1637	0304	05/25	- C' Y
69.000	.0566	.0470	.0474	.595 6	.6665	2140	0336	0529	0 . 4
66 000	.0574	.0572	.0415	.36.47	.7374	3593	0414	0416	، د ، ٥ -
68.000	.0572	.0614	. 0501	.3503	.6453	4895	0543	0458	0685
70.000	.0533	. 0559	.0474	.5221	.6899	+.2571	0400	0549	0718
79.003	.00.5	. 4729		. 2001	. 6623	~.6371	0400		

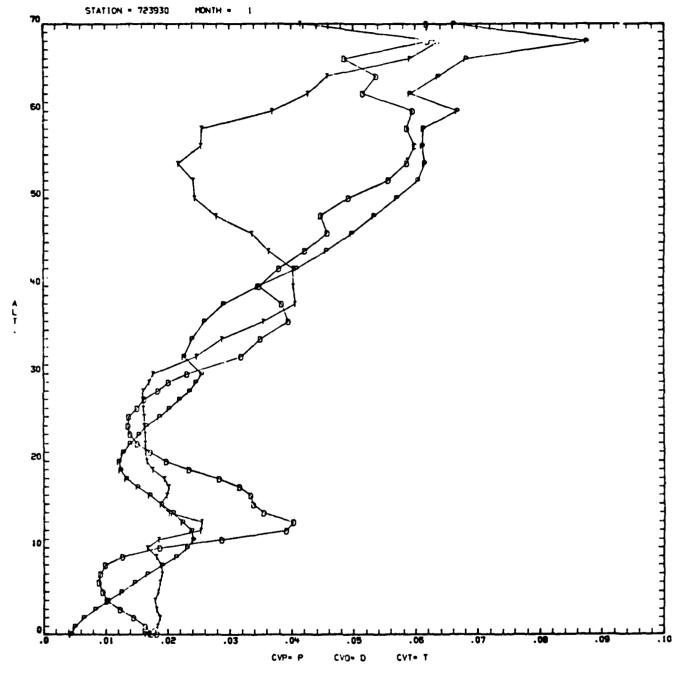


Fig. B-13

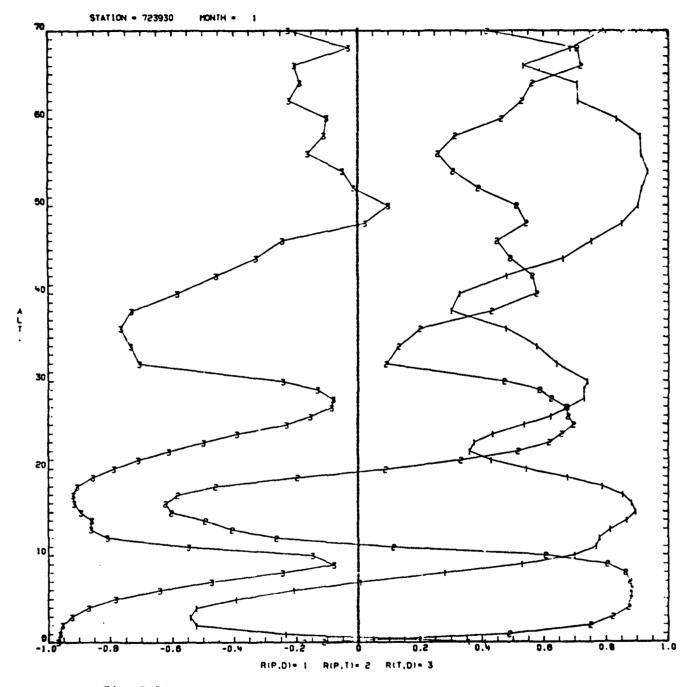


Fig. B-14

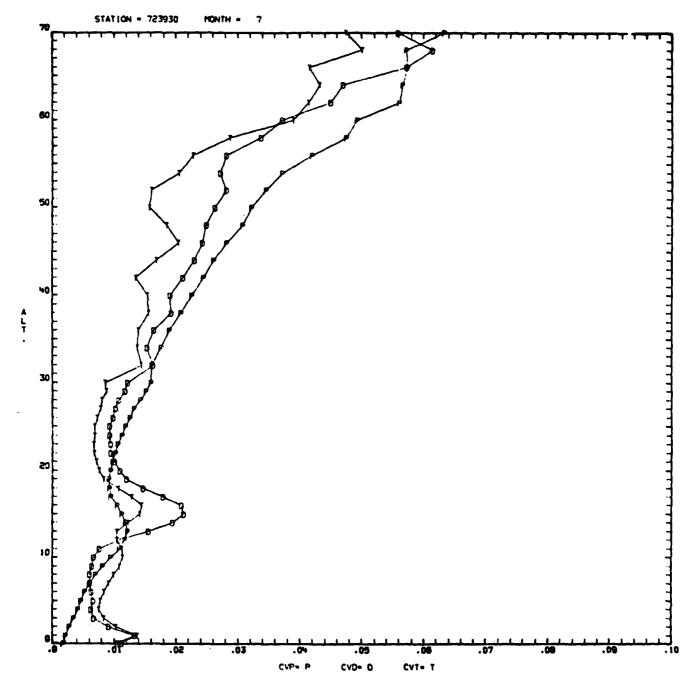


Fig. B-15

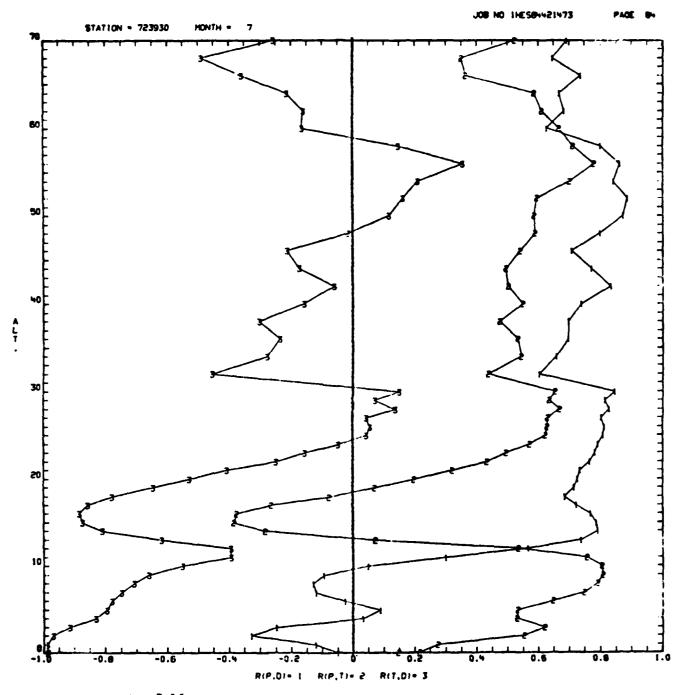


Fig. B-16

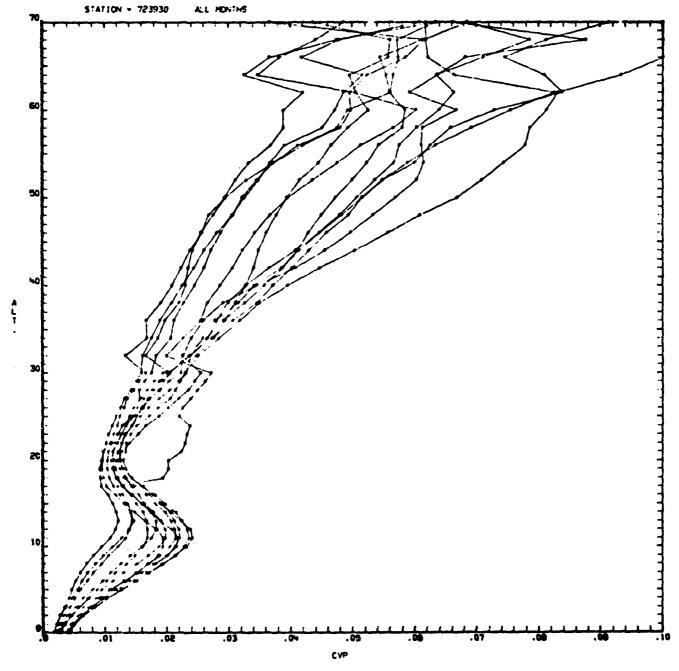
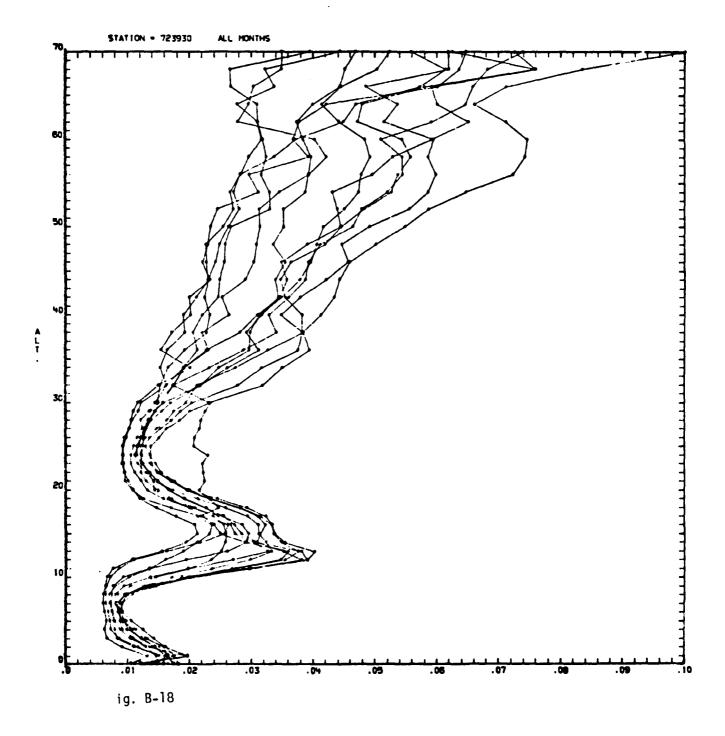


Fig. B-17



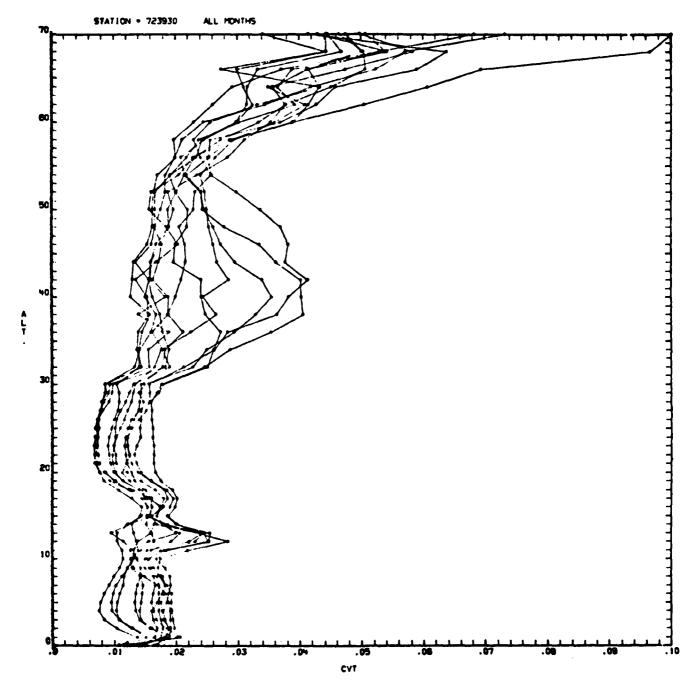


Fig. B-19

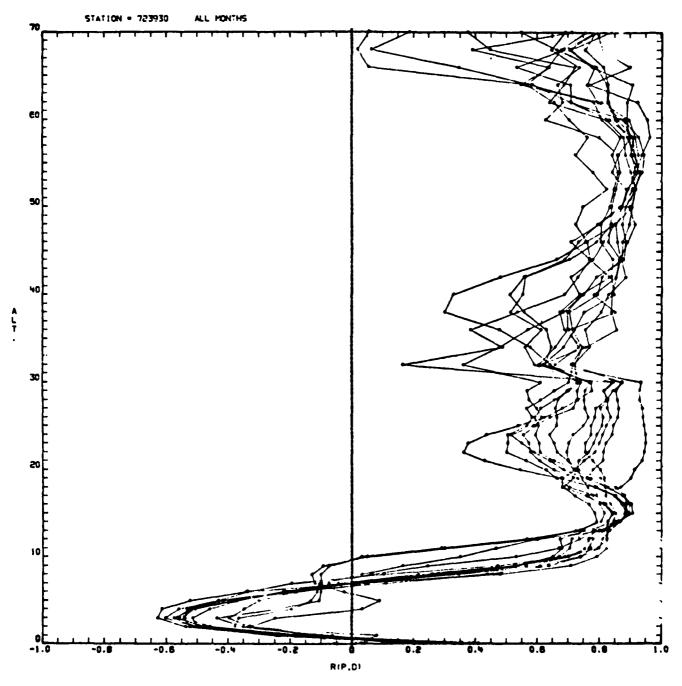


Fig. B-20

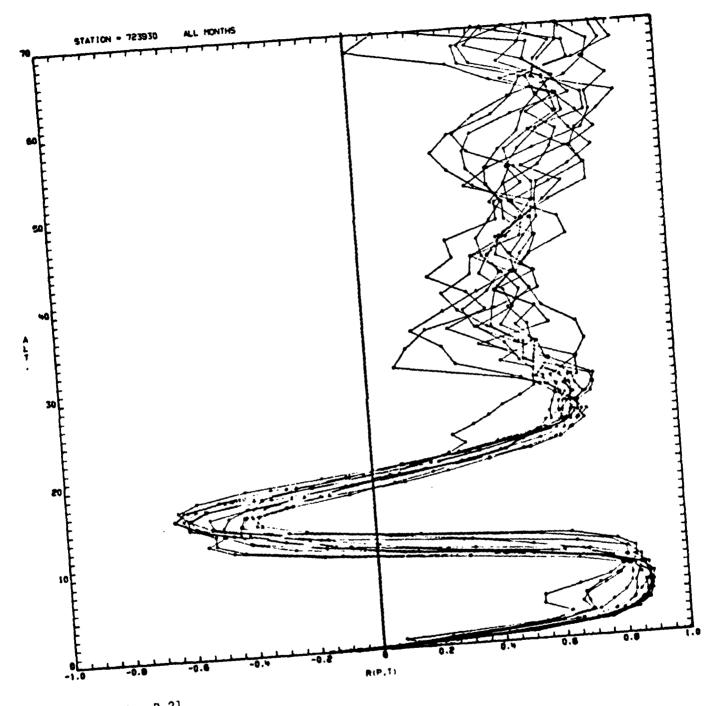


Fig. B-21

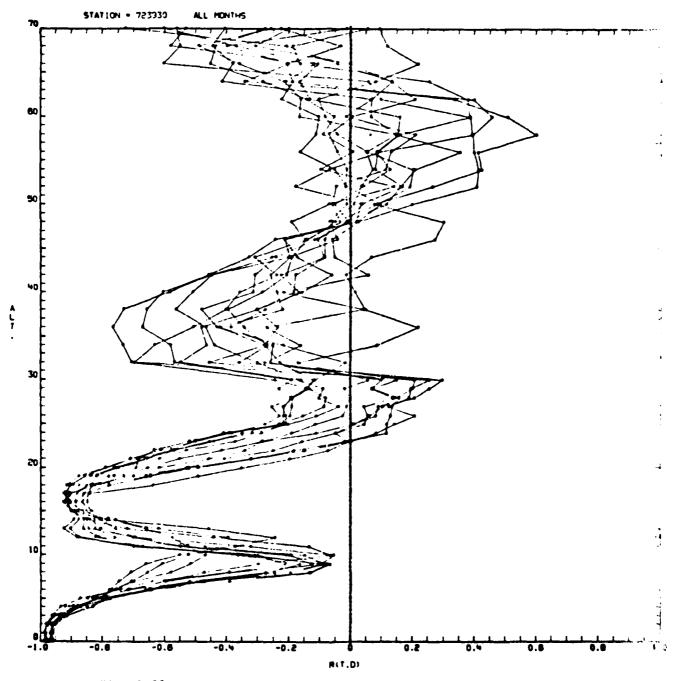


Fig. B-22

